



Laboratory for Timber Constructions

Innovative Timber Constructions

Yves Weinand, Associate Professor

IBOIS | EPFL | Lausanne

Bureau d'Etudes Weinand

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Belgique

Tél: + 32 4 343 39 38
Fax: +32 4 343 01 07
www.weinand.be

2007 Pont pédestre sur l'Our,

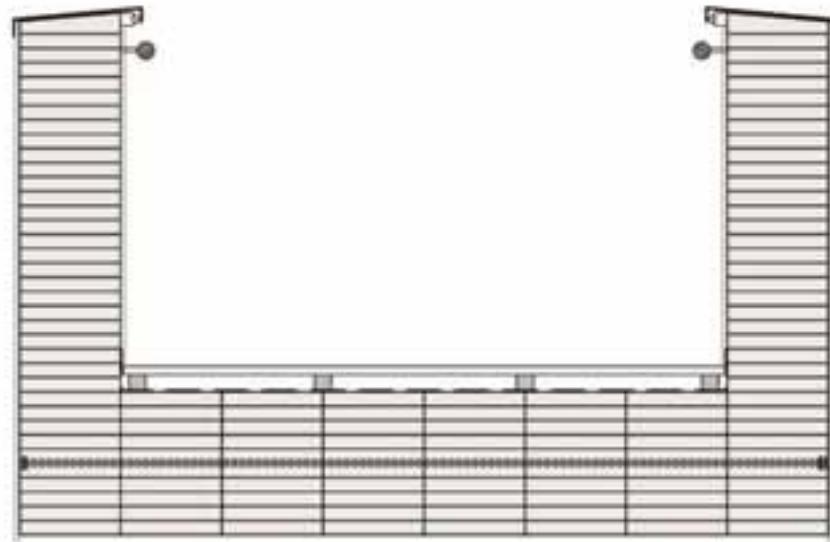
Burg Reuland

Maître d'ouvrage : Commune de Burg-Reuland

Architecte: association momentanée

Michaelis-Weinand, Espeler

Ingénieur: bureau d'études Weinand



2006 Patinoire, Liège

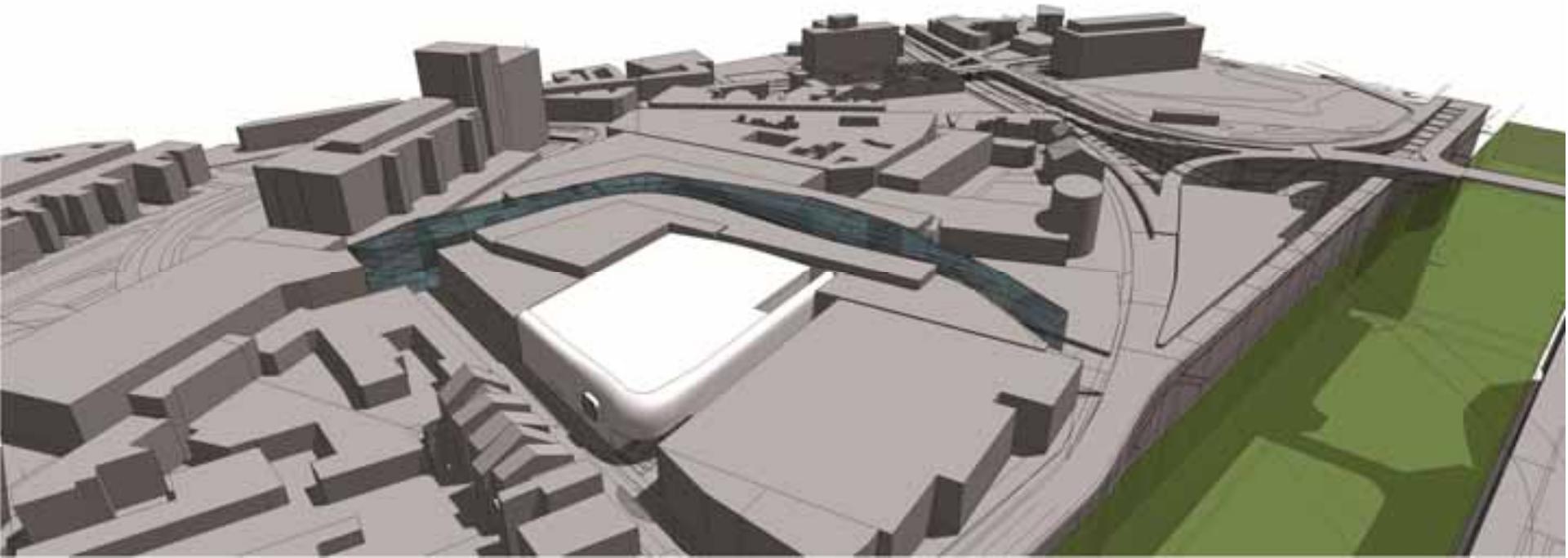
Maître d'ouvrage : Ville de Liège

Architecte: association momentanée Escaut-Weinand

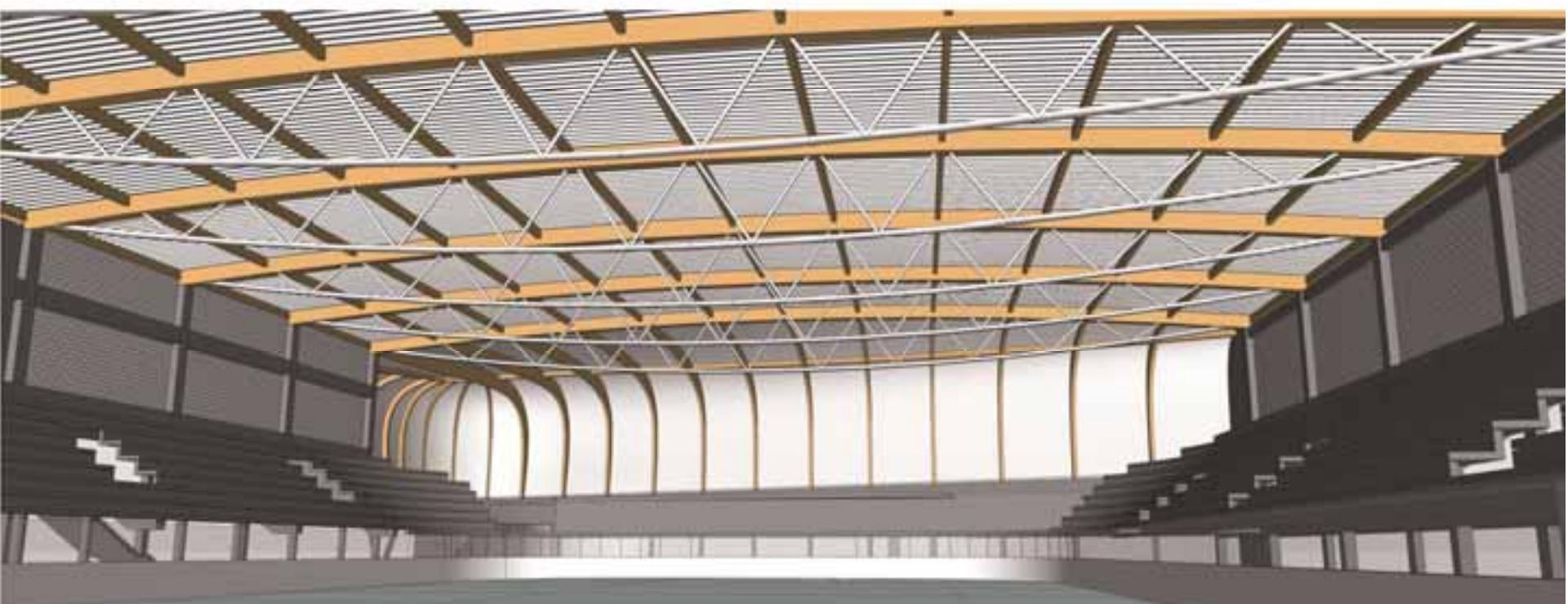
Ingénieur: bureau d'études Weinand

Surface utile : 4700 m²,

Coût estimé : € 7'200'000,-



La charpente principale est composée de 8 poutres treillis en bois lamellé collé soutenues par des tirants métalliques qui confèrent à la structure sa légèreté.



2003 Musée de la photographie, Charleroi

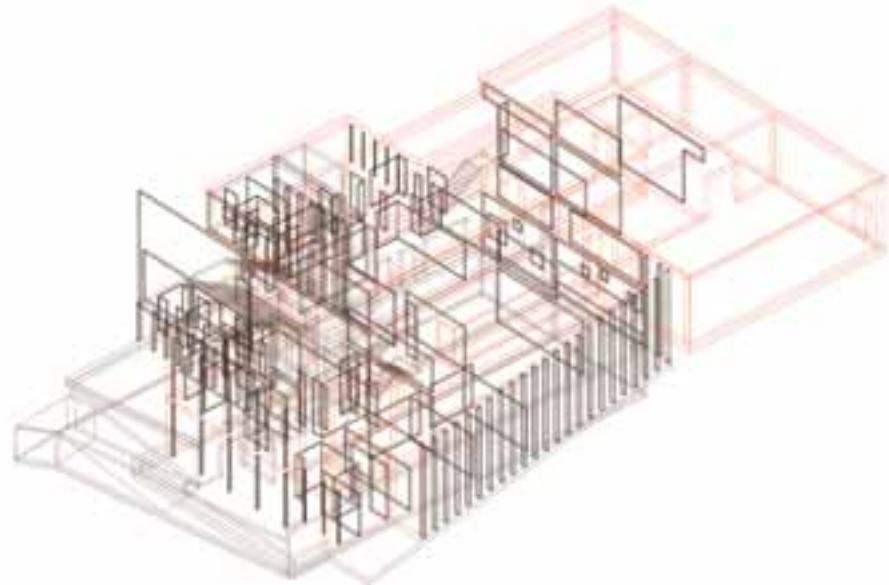
Maître d'ouvrage : Communauté française de Belgique

Architecte: Escaut Architecture, Bruxelles

Ingénieur: Bureau d'études Weinand

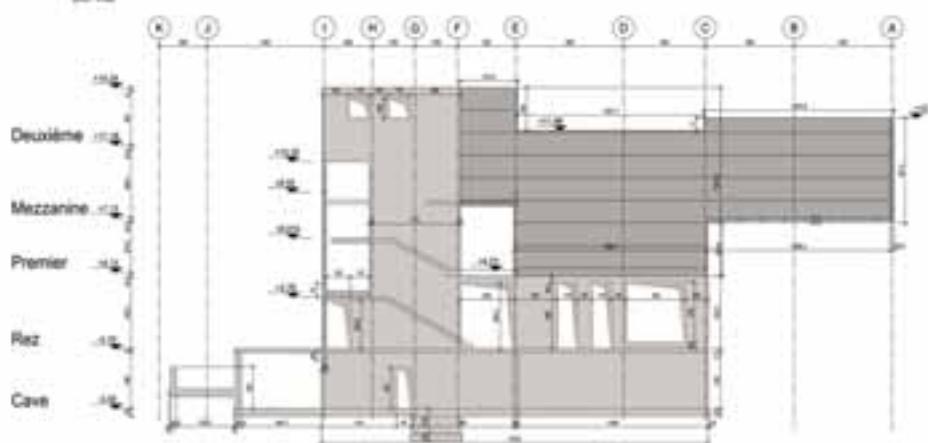
Surface utile : 2450 m²

Coût estimé : € 3'000'000,-



L'architecture de l'extension du musée de la photographie à Charleroi est un exemple d'application innovante d'architecture et d'application du matériau bois. Des panneaux en bois massif et contrecollés sont mis en oeuvre pour réaliser un étage en porte-à-faux. Sur le plan économique la variante bois bat la variante en béton initialement prévu. Il s'agit d'une approche interdisciplinaire qui lie les réflexions d'espace à celle relatives à la structure du bâtiment.

Coupe à l'axe B







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2005, Complexe funéraire, Welkenraedt

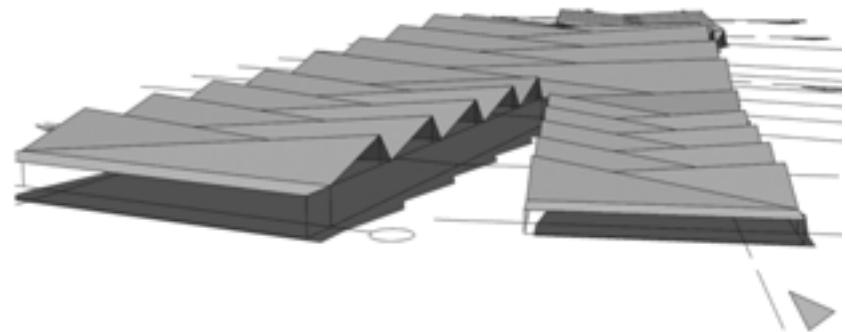
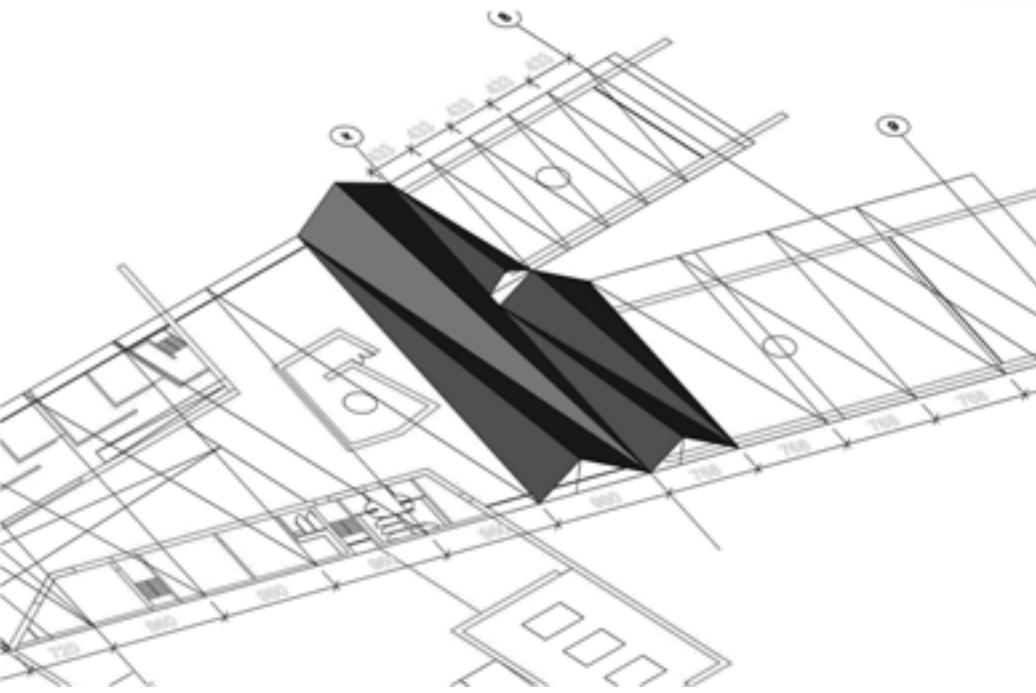
Maître d'ouvrage : Intercommunale du centre funéraire de Liège et environs (CFR)

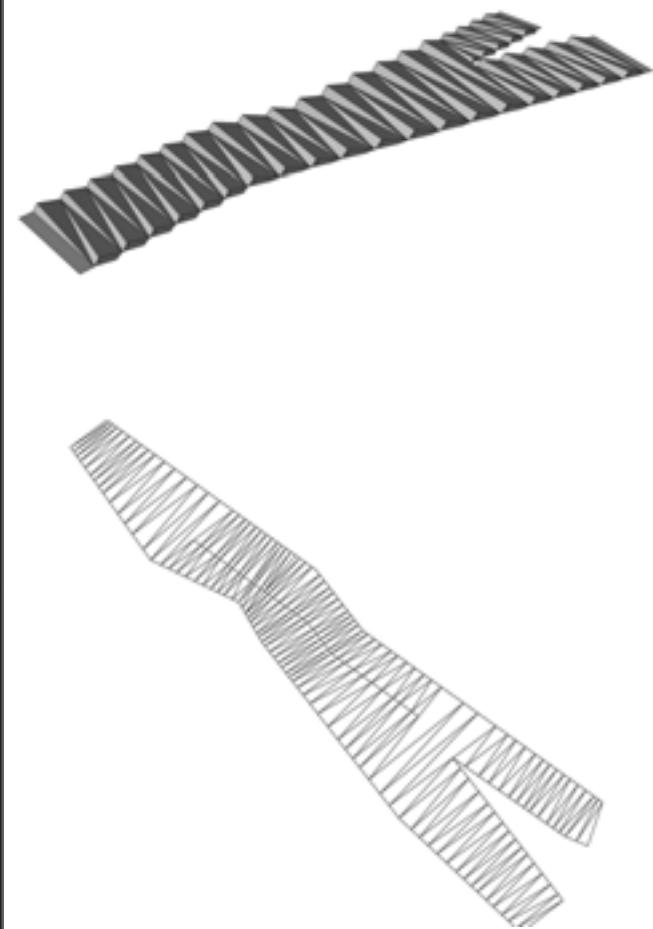
Architecte: Association momentanée Dethier - Weinand

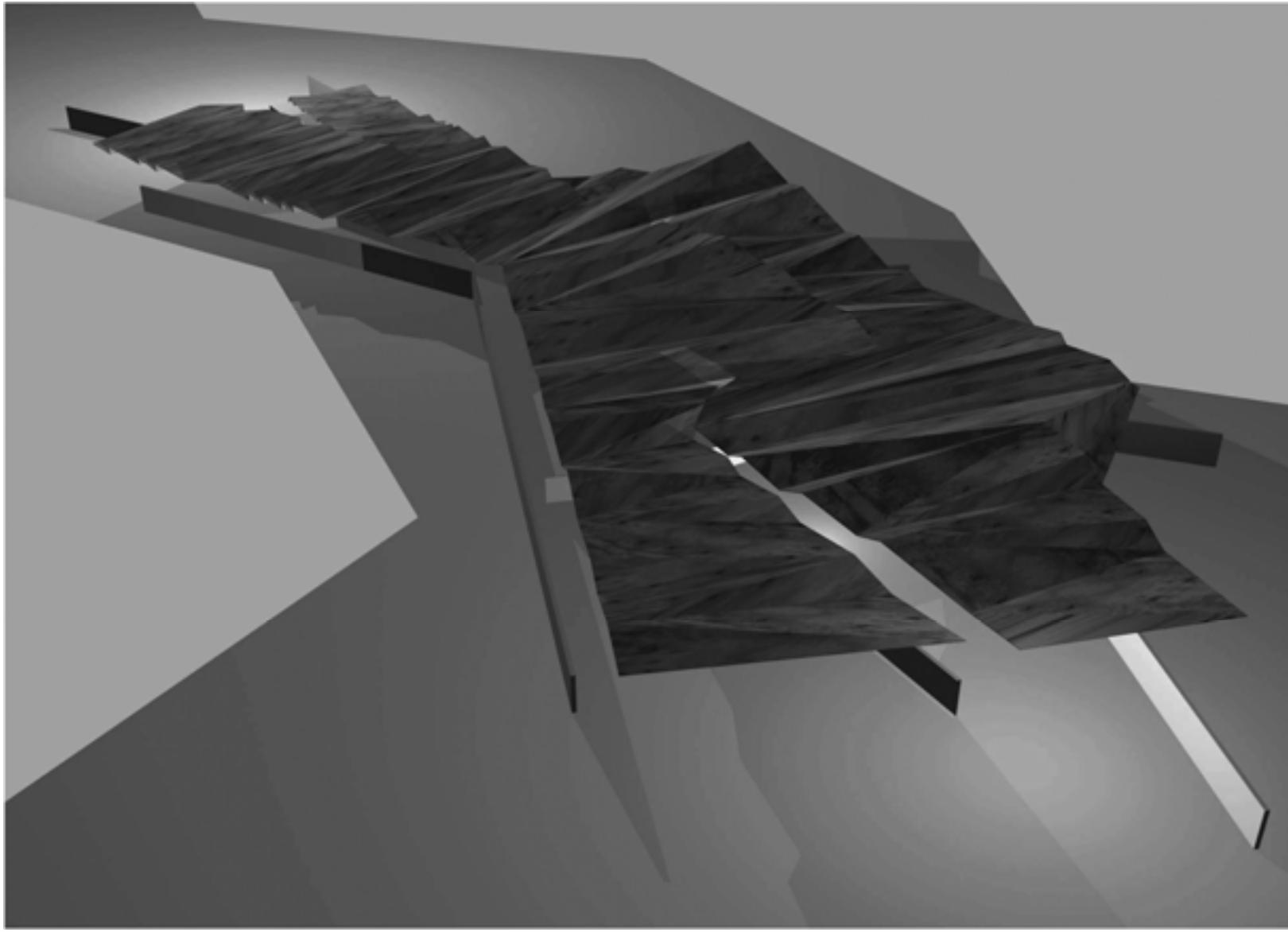
Ingénieur: Bureau d'Etudes Weinand

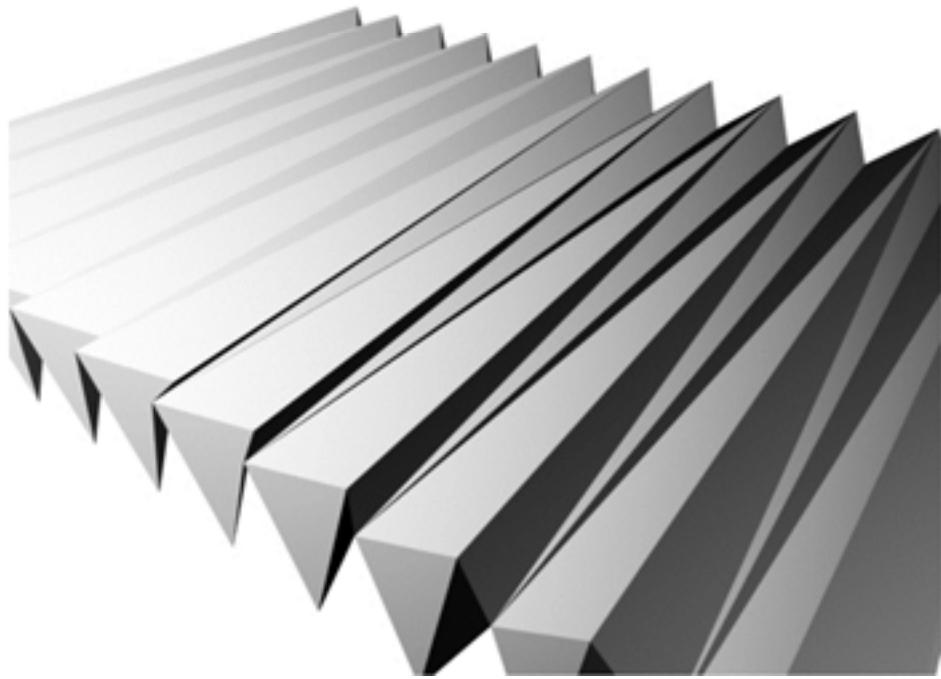
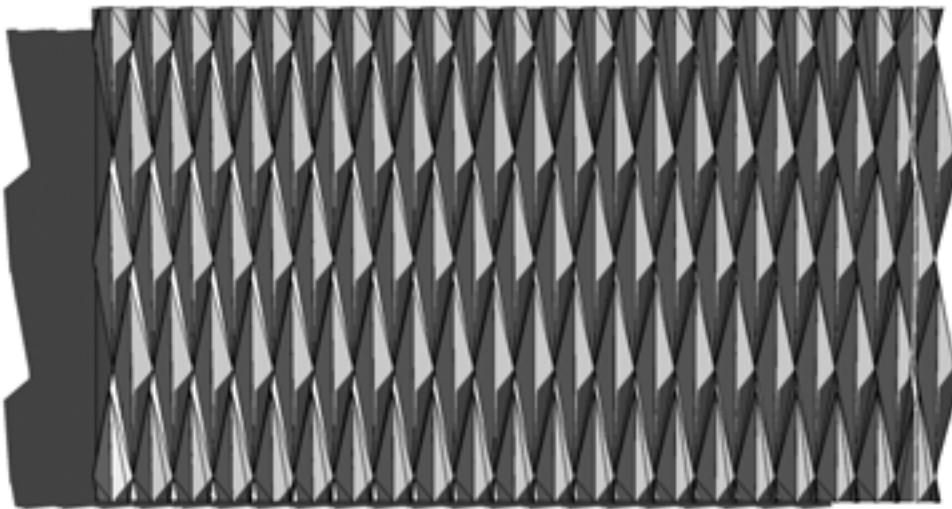
Surface utile : +/- 5000 m²,

Coût estimé € 5'100'00,-

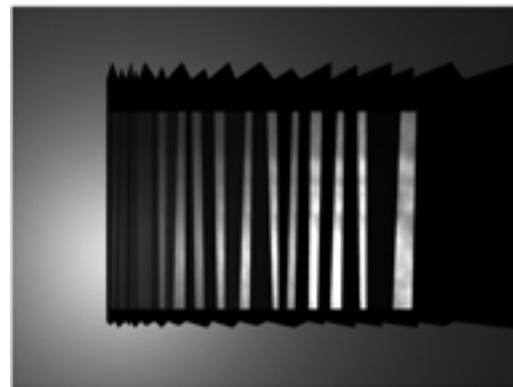
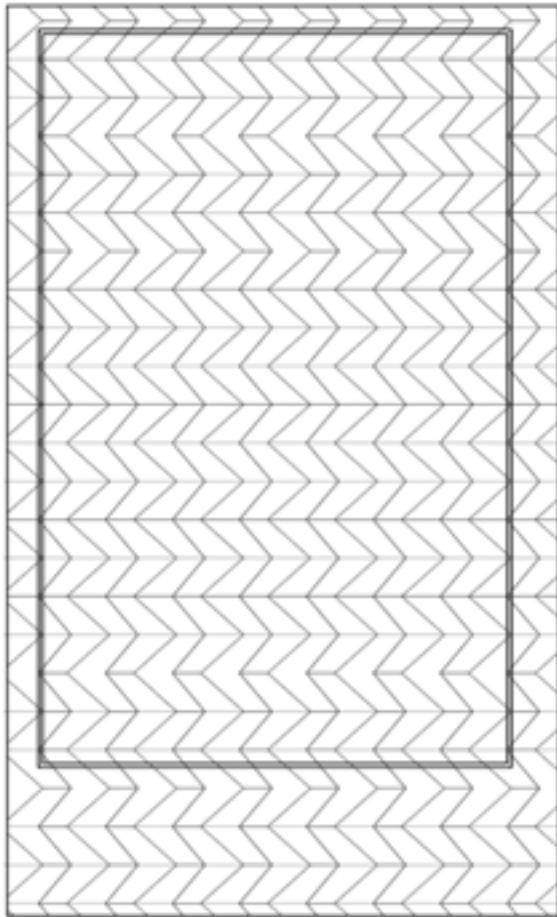




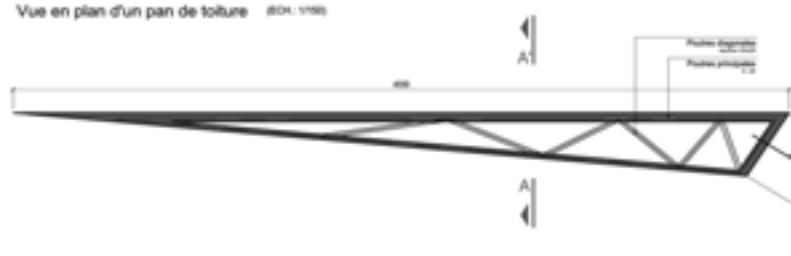
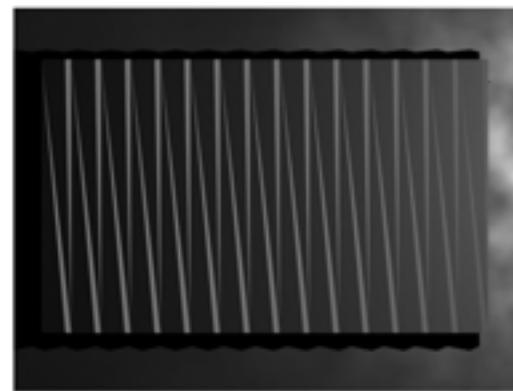
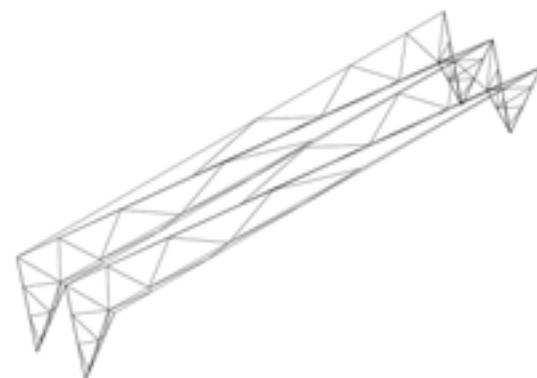




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GÉOMÉTRIE
Modèle tridimensionnel



2006, Salle de sport, Yverdon

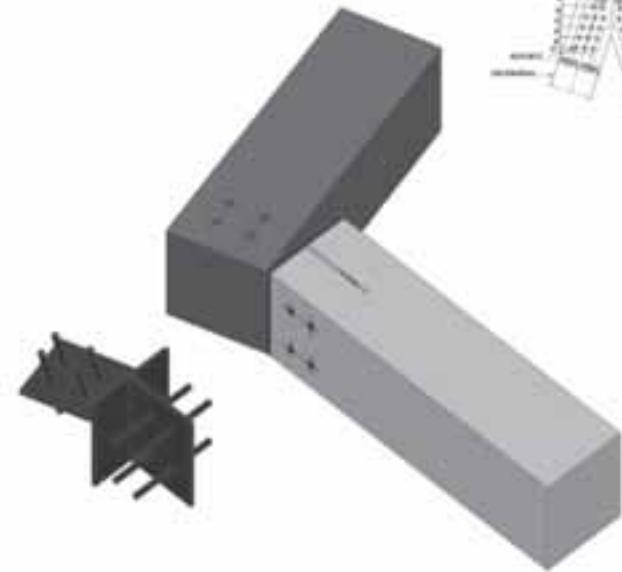
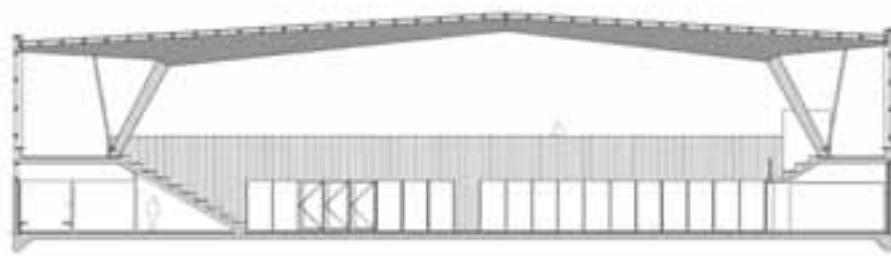
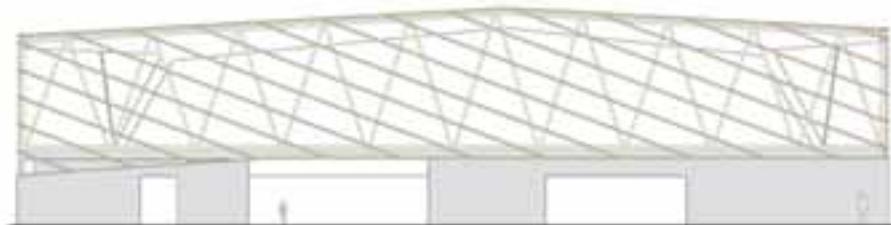
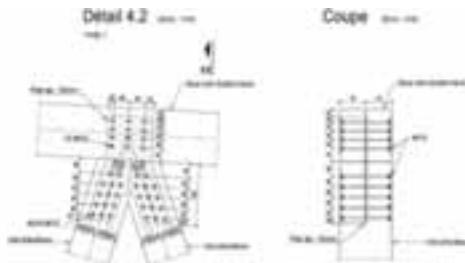
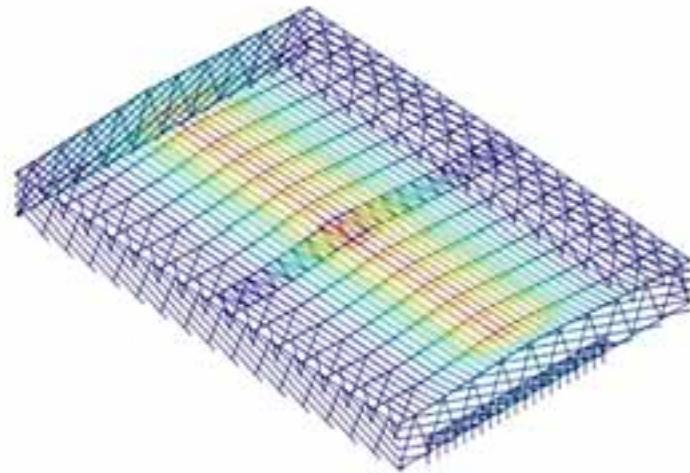
Maître d'ouvrage : Commune d'Yverdon

Architecte: Ueli Brauen & Doris Wälchli avec Yves Weinand

Ingénieur: Bureau d'Etudes Weinand

Surface utile : 2866 m²

Coût estimé : CHF 14'000'000,-

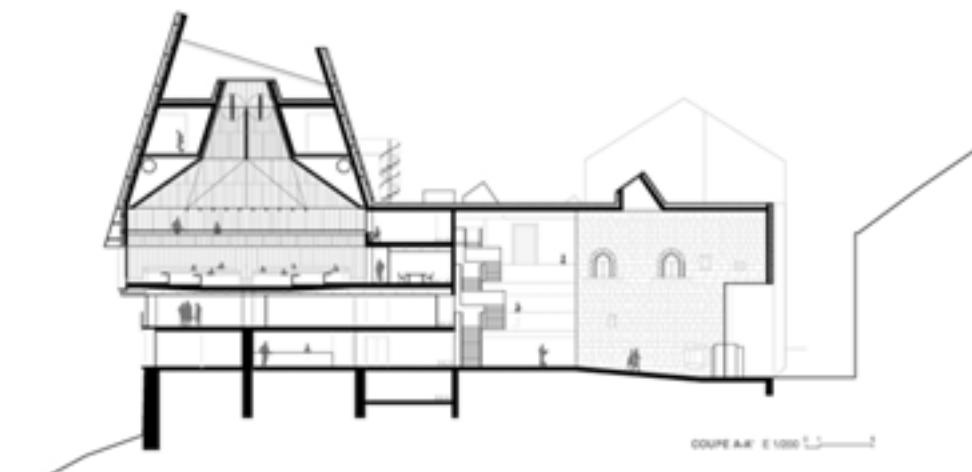


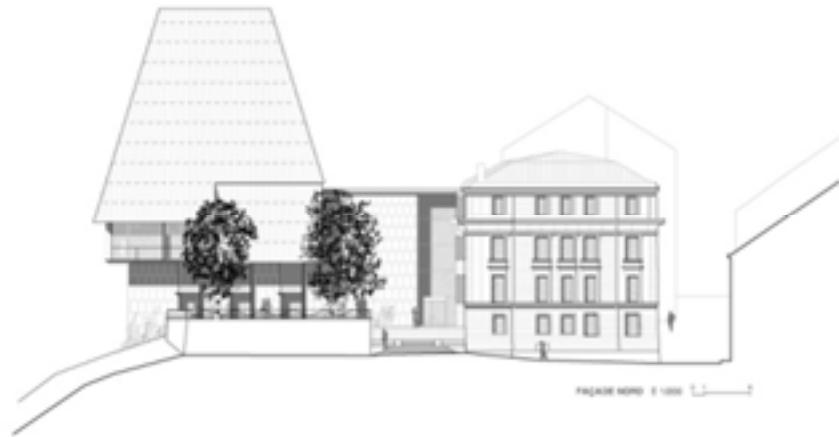
2009, Parlement

Maître d'ouvrage : Canton de Vaud

Architecte: Atelier Cube / Bonell & Gil

Ingénieur: Bureau d'Etudes Weinand





REVÊTEMENT EXTÉRIEUR DE FEUILLES DE CUIVRE AU LORON

LAME D'AIR POMPEÉ PAR TOLE PROFILÉE

ISOLATION

PANNEAUX EN BOIS MASSIF CERTIFIÉS LE

ASPIRATION HAUTE AIR CHAUD

LAMES DE CONTRÔLE DE L'ÉCLAIRAGE NATUREL

ESPACE MACHINES VENTILATION ET CHAUFFAGE

GALERIE TECHNIQUE INFRÉGÉE D'AIR

ASPIRATION BASSE AIR CHAUD

PANNEAUX EN BOIS MASSIF CERTIFIÉS LE
UTILISÉS COMME SURFACE TERRASSE



SALLE DU PARLEMENT 240m²

LA EXISTENCE DE LA DÉMOCRATIE EST DANS LES PERSONNES, LE CADRE PHYSIQUE DOIT LE INSPIRER.



IBOIS

Laboratory for timber constructions

Direction

Prof. Yves Weinand, ISA architect, EPFL civil engineer,
Associate Professor

Administration

Hildegard Bachmann, secretary

Collaborators

Hani Buri, EPFL architect, scientific collaborator
Gilles Gouaty, DEA EDIIS Lyon (F) computer scientist, PhD assistant

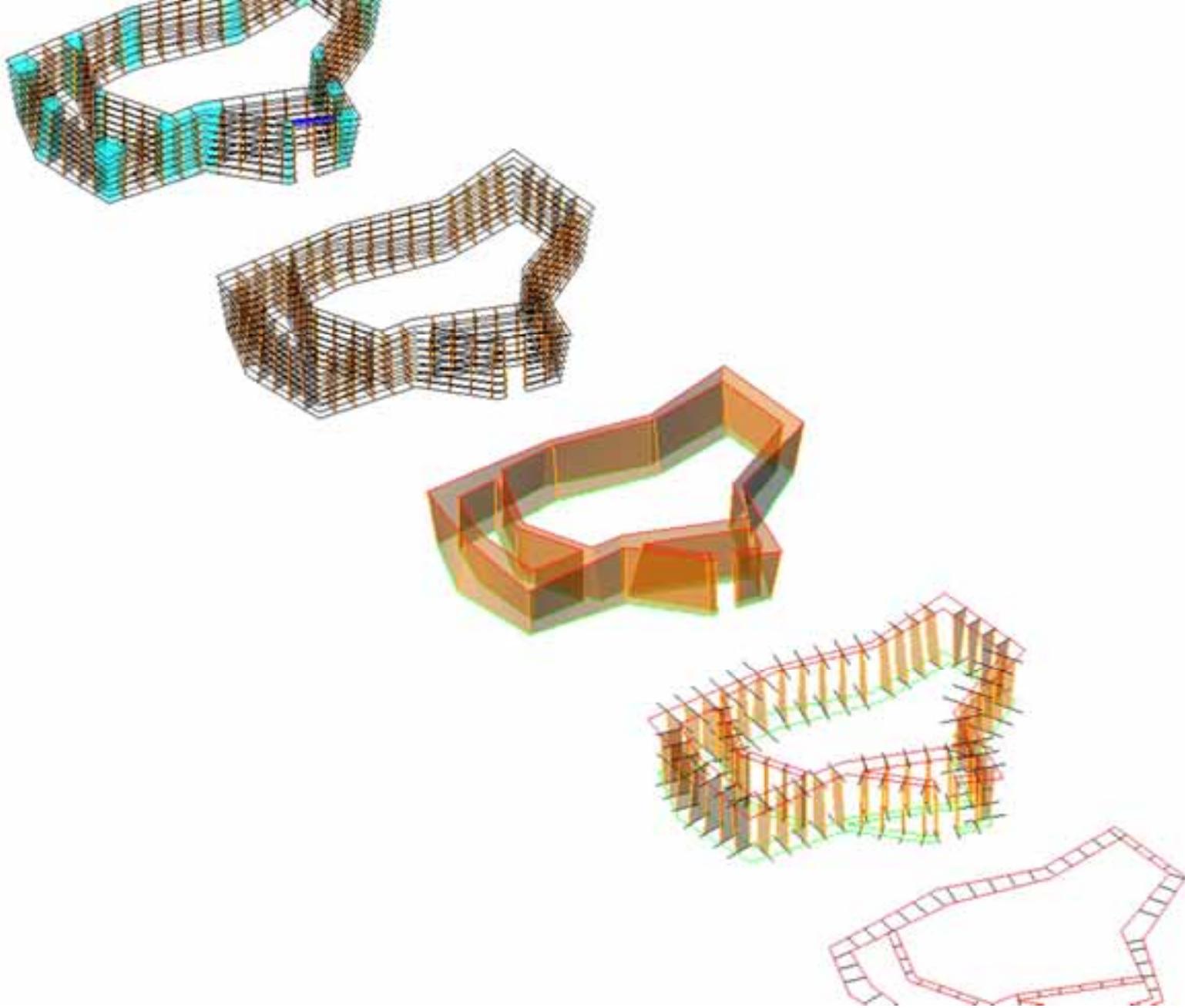
Markus Hudert, Städelschule Frankfurt (D) architect, PhD assistant

Johannes Natterer, EPFL SIA civil engineer, PhD assistant

Ivo Stotz, EPFL architect, PhD assistant

François Demoures, EPFL, mathematician, PHD assistant

Masoud Sistaninia, Iran University of Science and Technology, Teheran
mechanical engineer, PHD assistant





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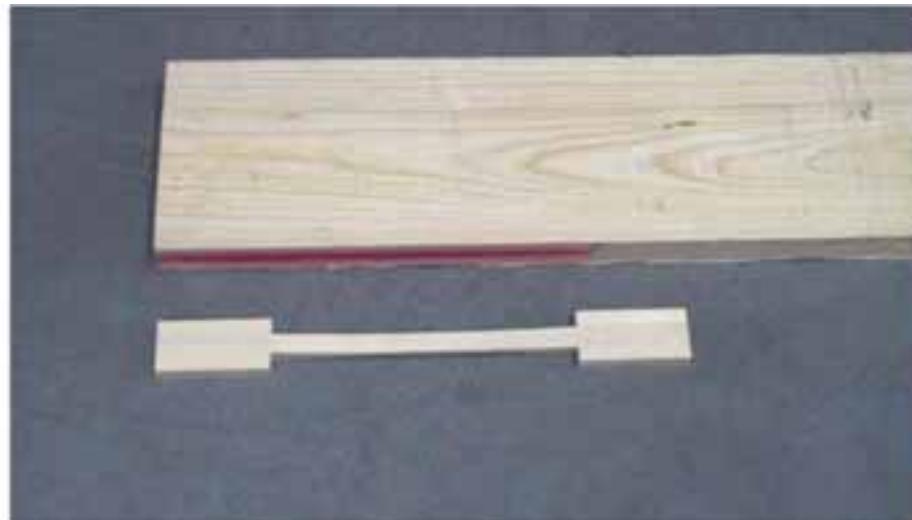


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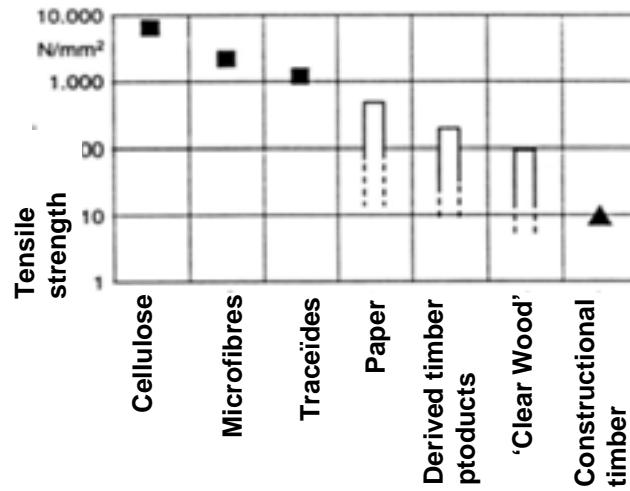
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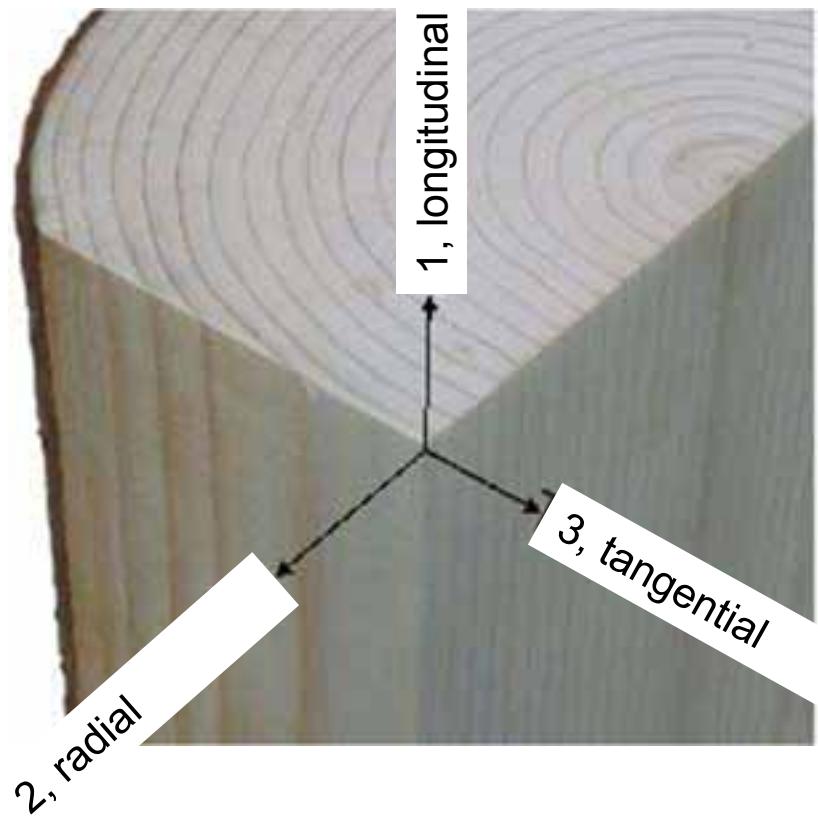
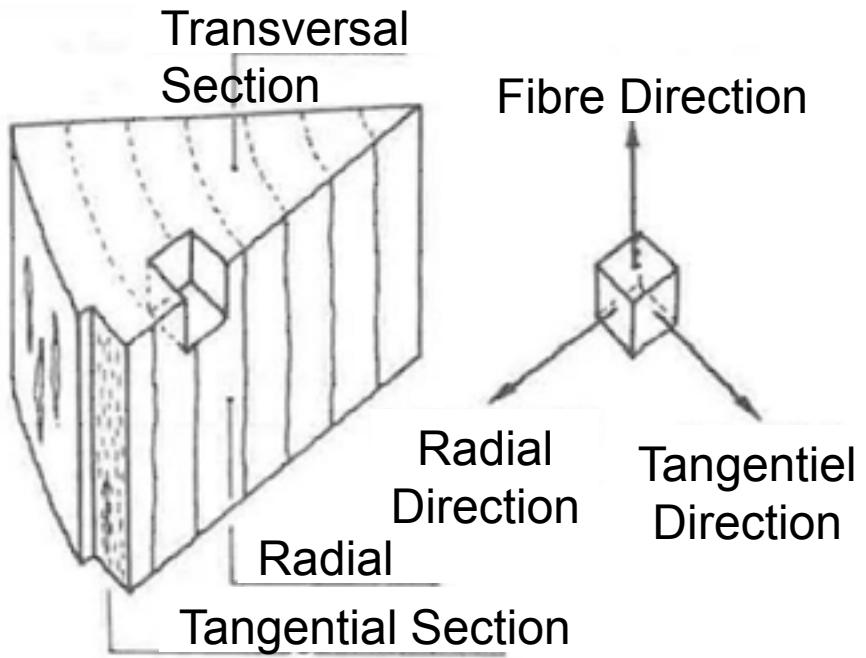
Characteristic values of spruce [P. Niemz, 1993 and P. Glos, 1981)

Characteristic properties	Small Specimen	Constructional Element	Difference to the small specimen
Bending Strength (mean value [N/mm ²])	68	37	46%
Tensile Strength parallel to fibers (mean value [N/mm ²])	80	30	63%
Compression Strength parallel to fibers (mean value [N/mm ²])	40	32	20%



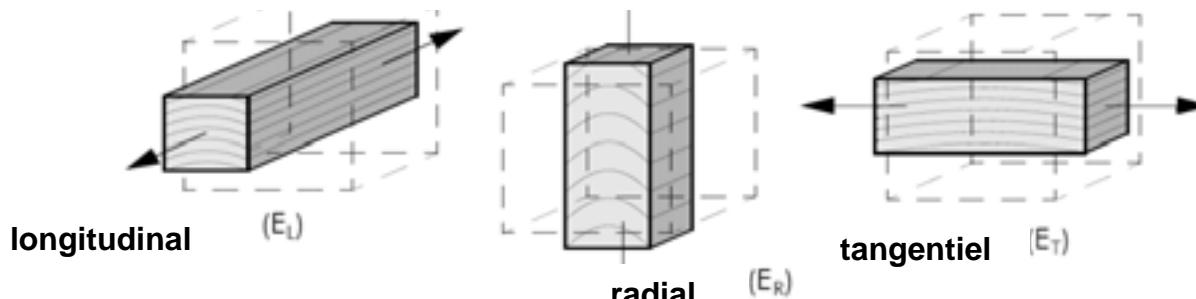
Mecanical Properties [Glos 1999]



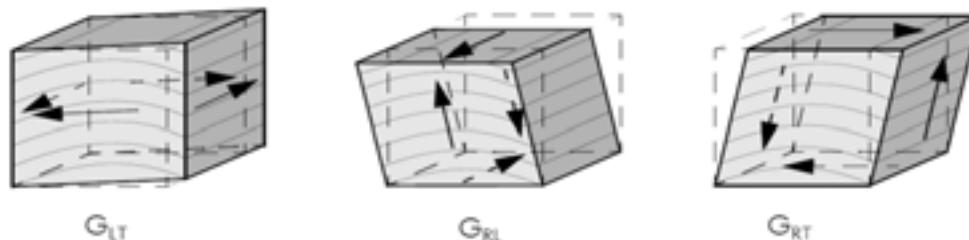


Definition of the circular orthotropic coordinate system [Schickhofer 2005]

Elasticity modulus ***E*** – normal deflection:



Shear modulus ***G*** – shear deflection:



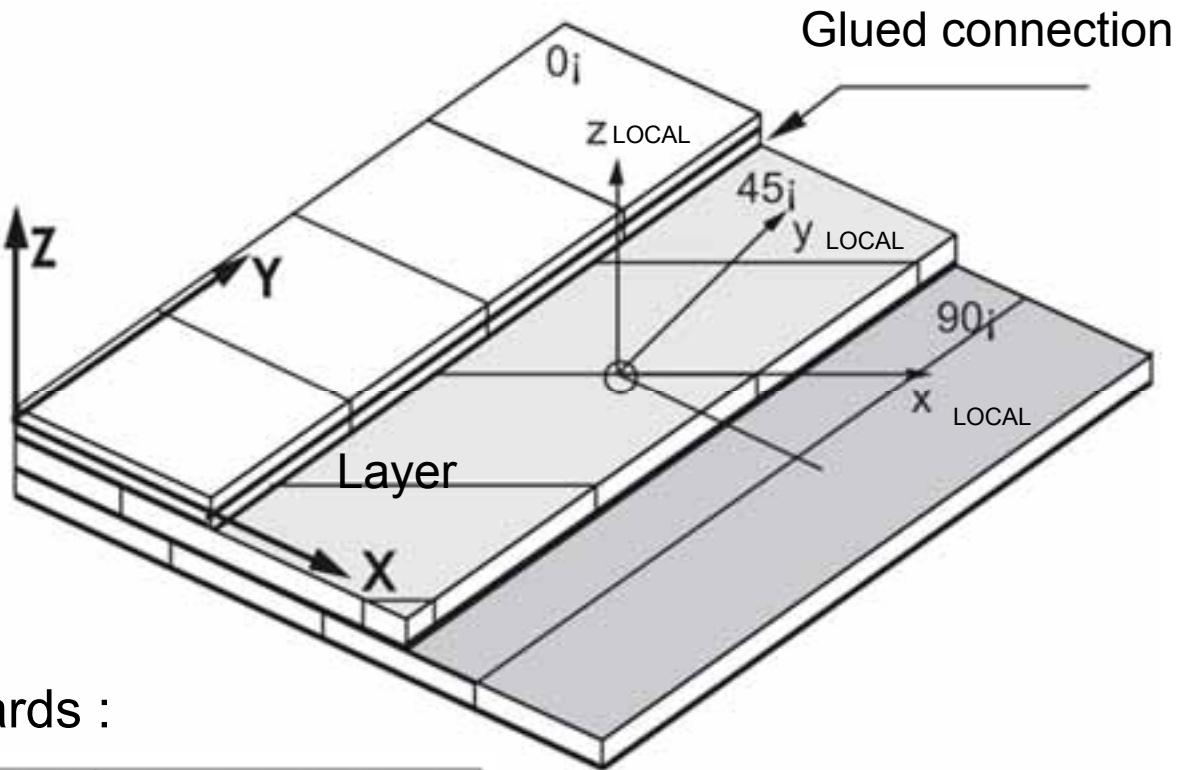
Elasticity Modulus ***E*** (in Tangential, Longitudinal and Radial direction)

$$E_T \div E_R \div E_L = 1 \div 1,7 \div 20 \quad (\text{Soft Wood})$$

$$E_T \div E_R \div E_L = 1 \div 1,7 \div 13 \quad (\text{Hard Wood})$$

Shear Modulus ***G*** (in Tangential, Longitudinal and
Radial) $G_{LR} \div G_{LT} = 1 \div 1$
 (Soft Wood)

$$G_{LR} \div G_{LT} = 1,3 \div 1 \quad (\text{Hard Wood})$$



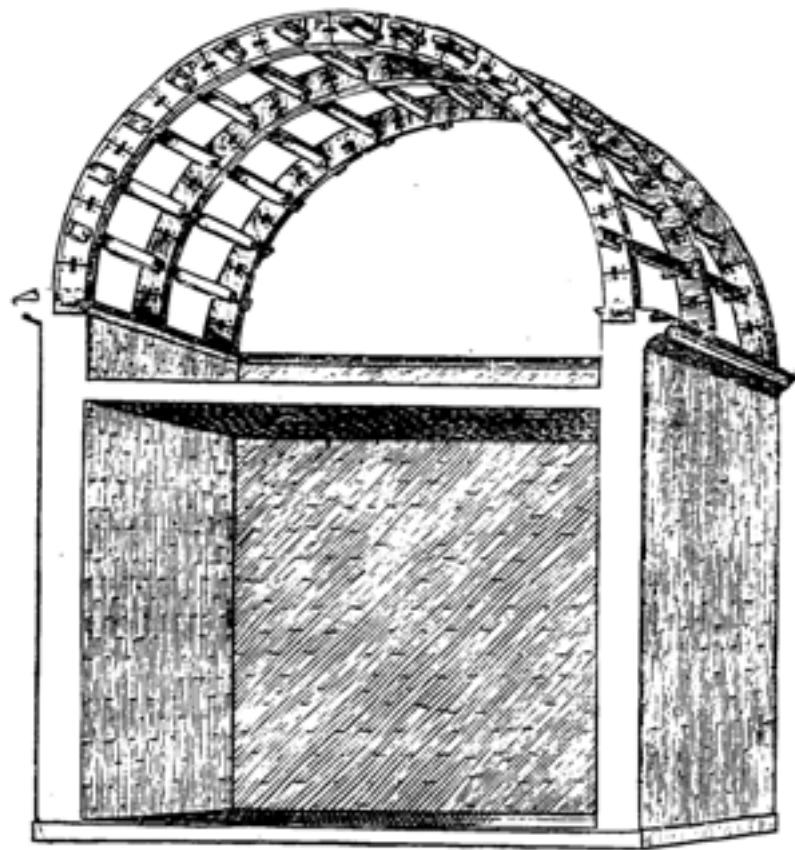
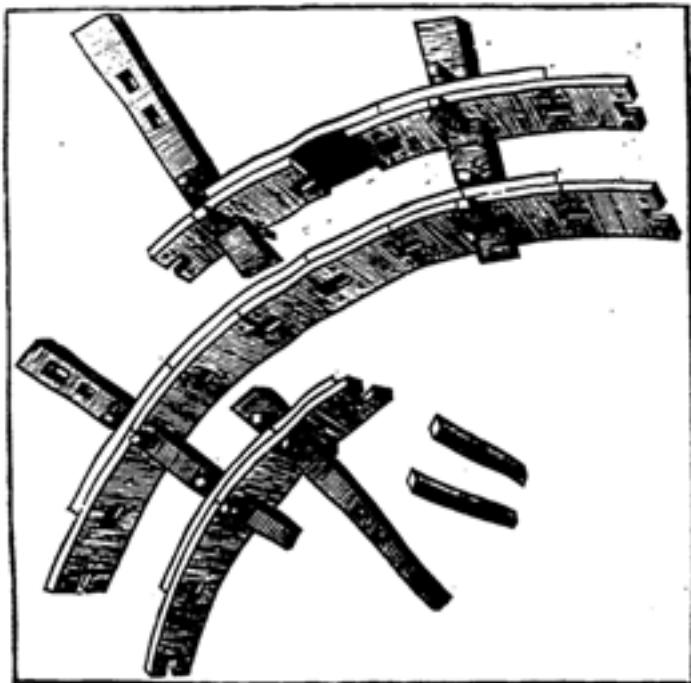
Three-layered timber boards :

E Modulus [N/mm ²]	Thickness [mm]	Fiber Orientation [deg]
$E_1 = 12000$	$t_2 = 24$	$\alpha_1 = 0$
$E_2 = 10000$	$t_2 = 15$	$\alpha_2 = 45$
$E_3 = 12000$	$t_3 = 24$	$\alpha_3 = 90$

[Schickhofer 2005]

Philibert de l'Orme

Construction detail



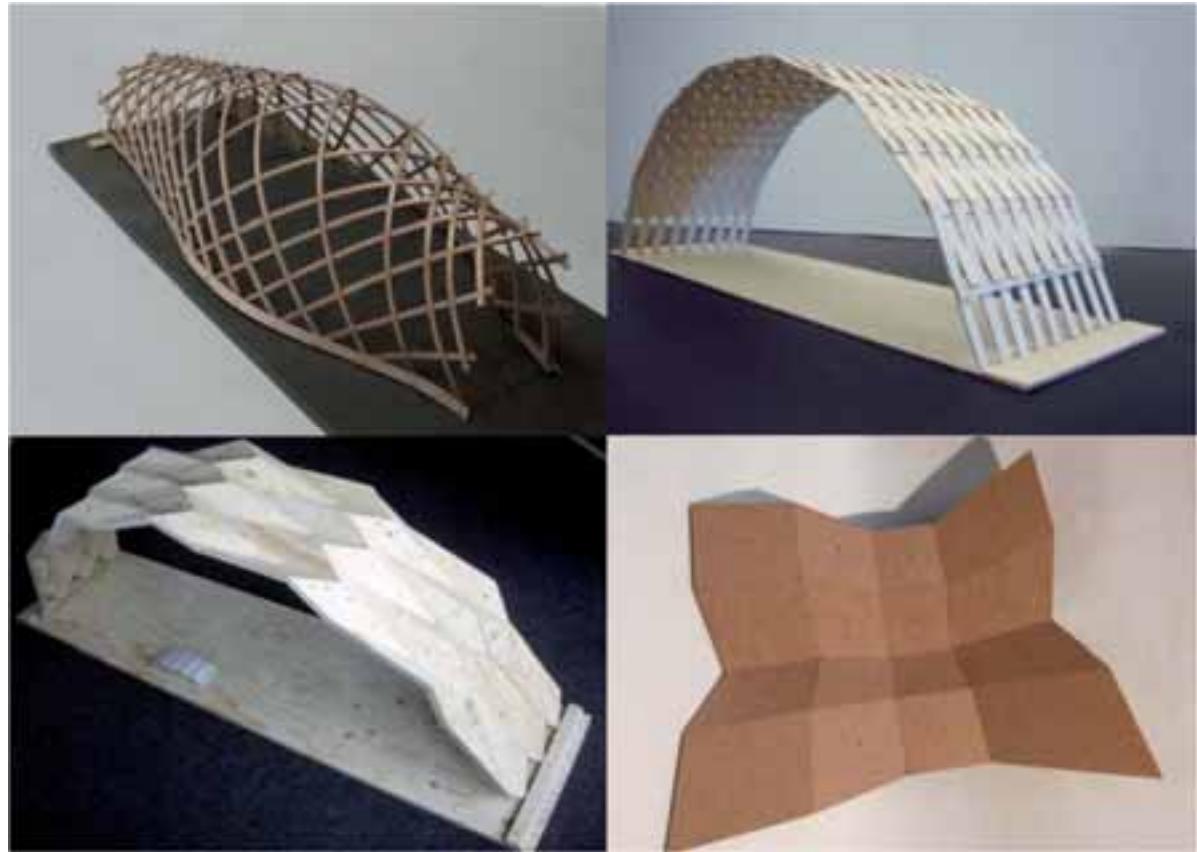


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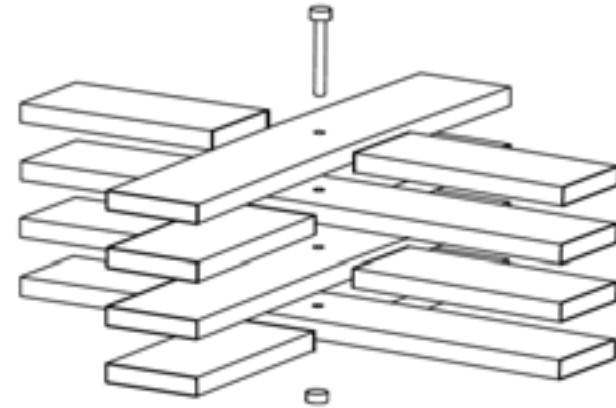
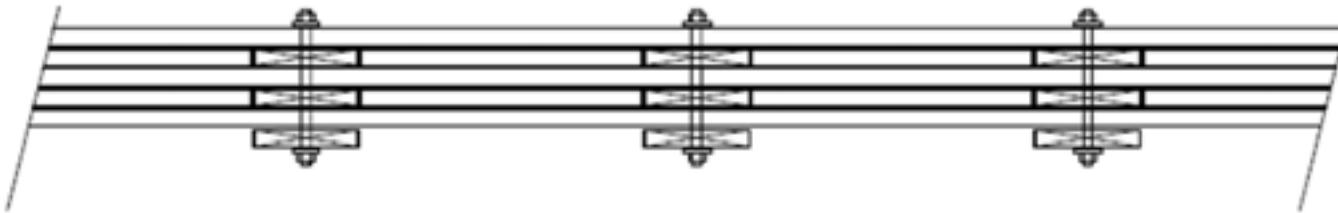
Research at Ibois

Free form shell structures



Structural behavior of rib shells

Construction detail



Johannes Natterer

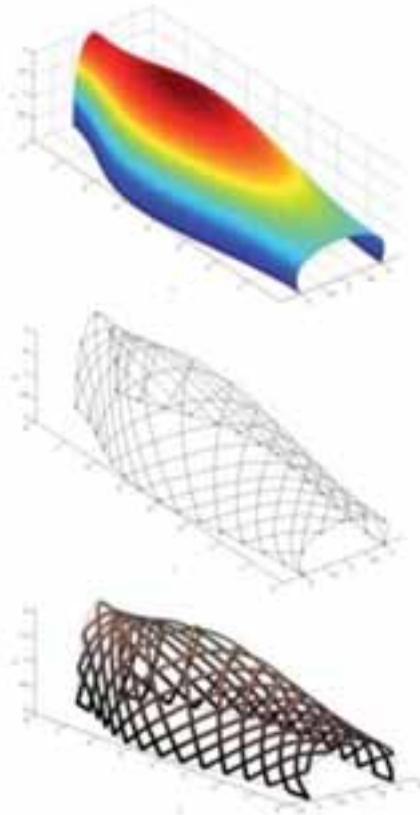
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GEOS

Build rib shells on free-form surfaces



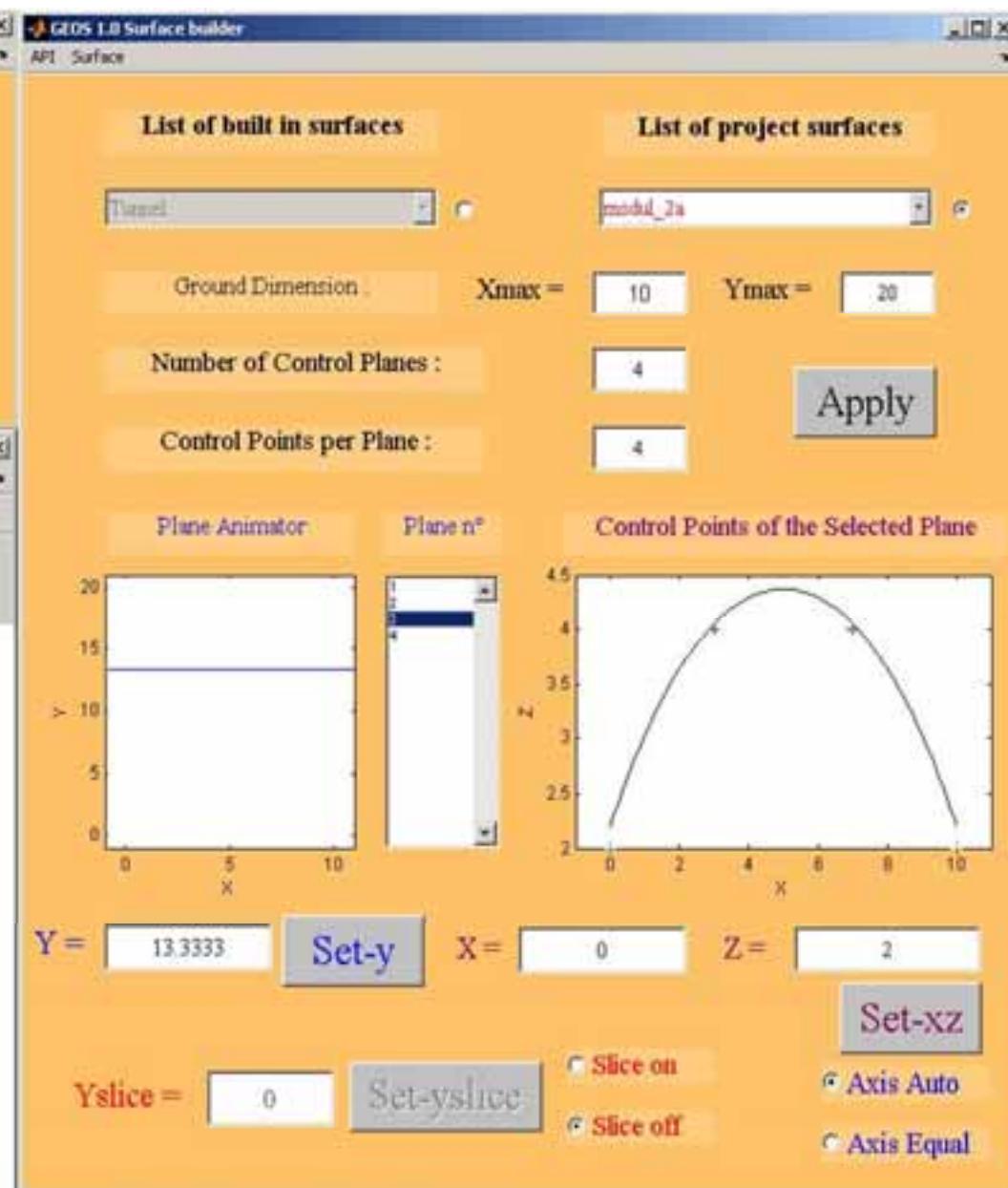
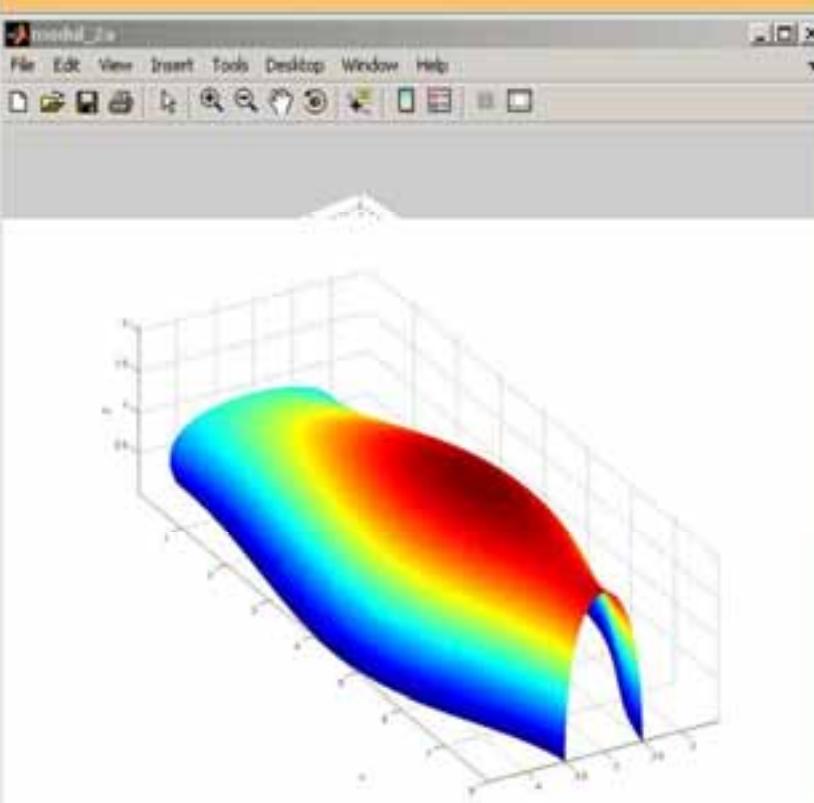
Claudio Pirazzi

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GEOS 1.0

List of Projects

model_2a_neal





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Multi-Layer beams with inter-layer-slip theories

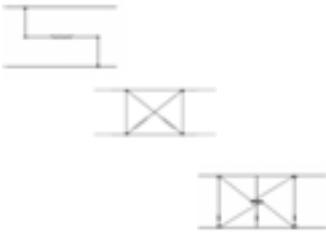
Method gamma

$$I_{ef} = \sum_i^m I_i + \sum_i^m \gamma_i A_i a_i^2$$

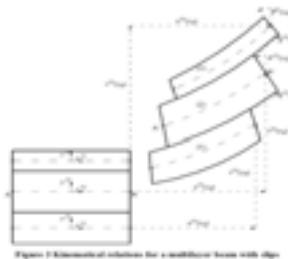
Appendice-G de la DIN 1052

$$\begin{aligned} \text{Trager A} \quad B_A &= \sum E_i \frac{d_i^3}{12} \cdot b_i; S = \infty \\ \text{Trager B} \quad B_B &= \sum E_i \cdot d_i \cdot z_i^2 \cdot b_i; S \end{aligned}$$

Truss



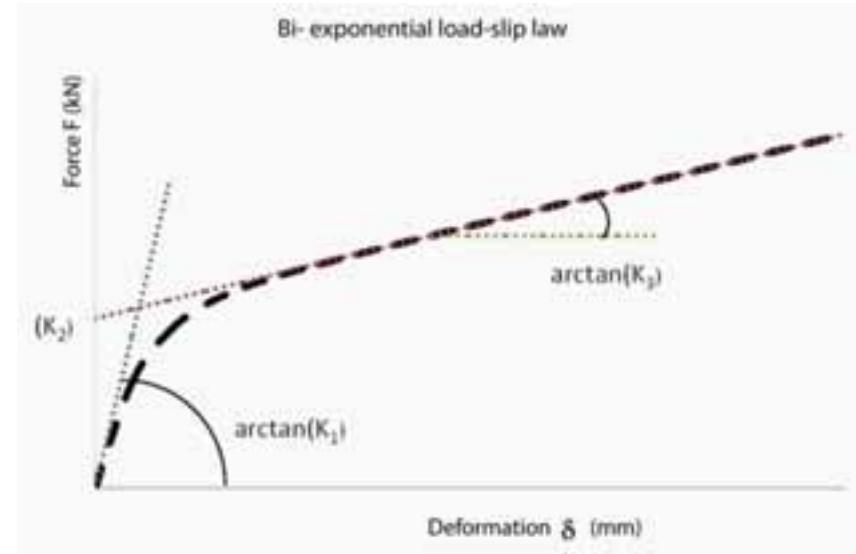
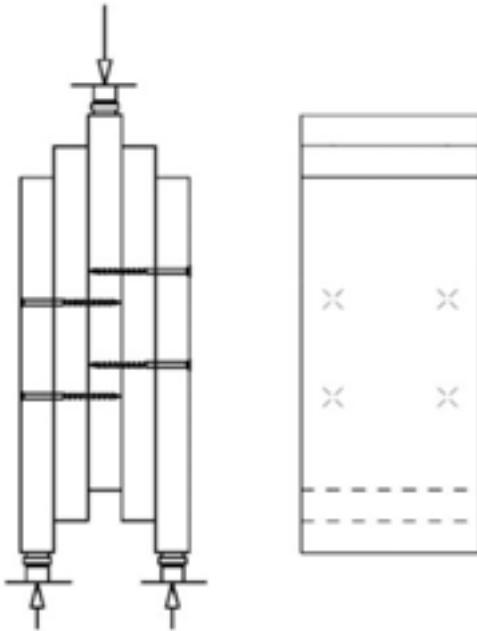
Finite element
2n+1 degrees of freedom



Johannes Natterer

Test

Stiffness of the joints



Johannes Natterer

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Structural behavior of rib shells

Develop a finite element

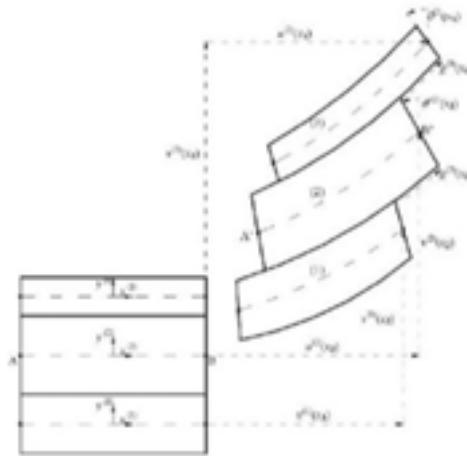
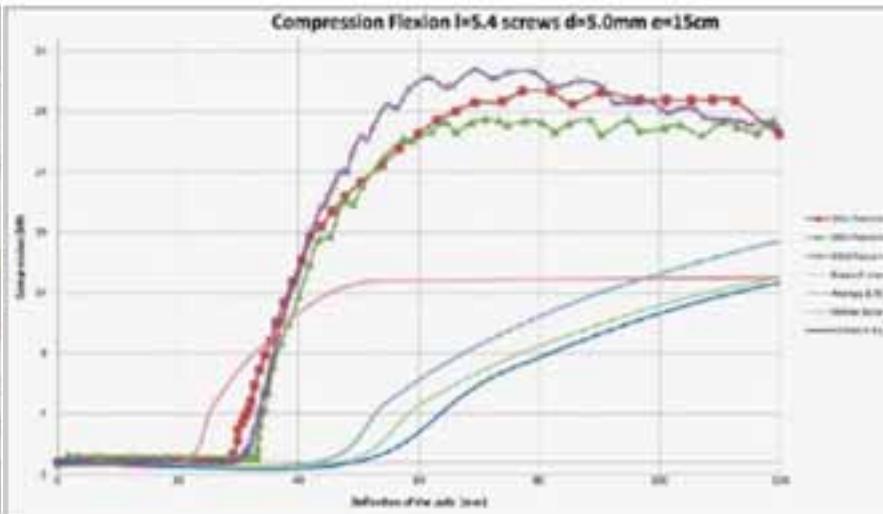


Figure 3 Kinematical relations for a multilayer beam with slips



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Prototype

Final validation of the finite element

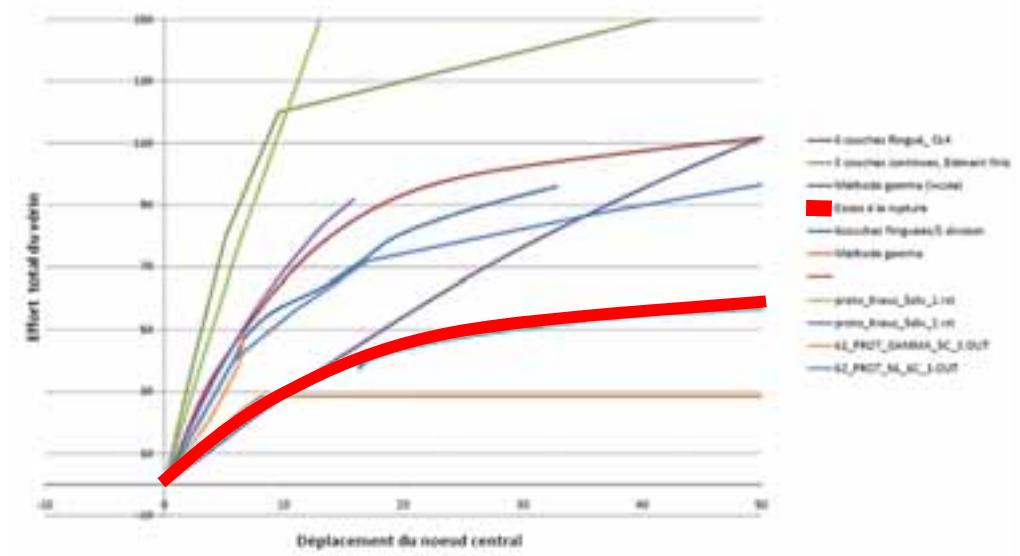
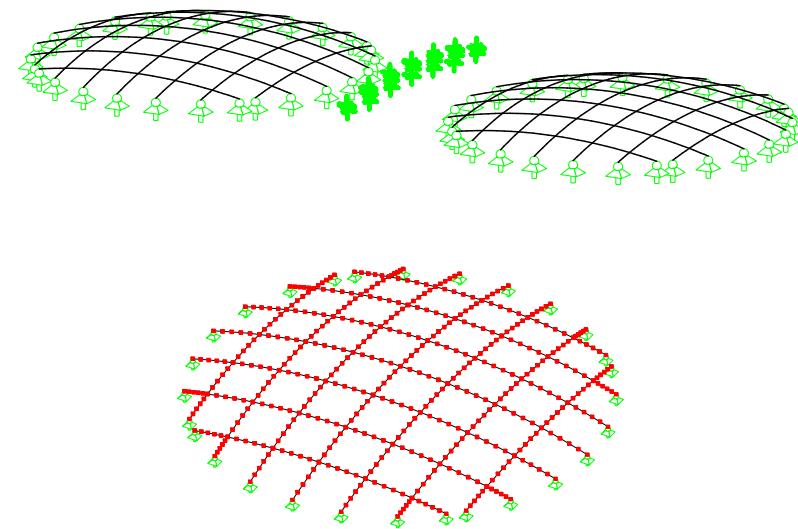


Johannes Natterer

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Modélisation du prototype

Résultats



Johannes Natterer

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Structural timber fabric

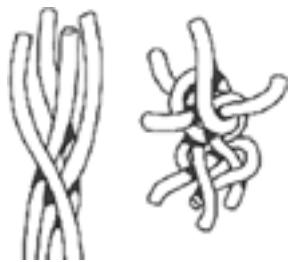
Applying textile principles to building scale



Markus Hudert

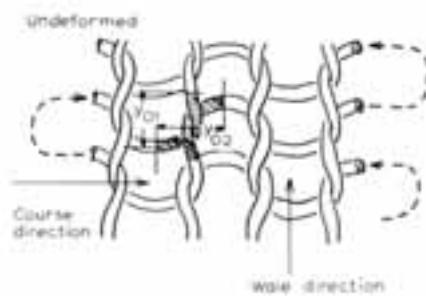
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Felted Fibers



Example Exemple
.Felt Feutre
.Paper Papier

Primary Textile Techniques



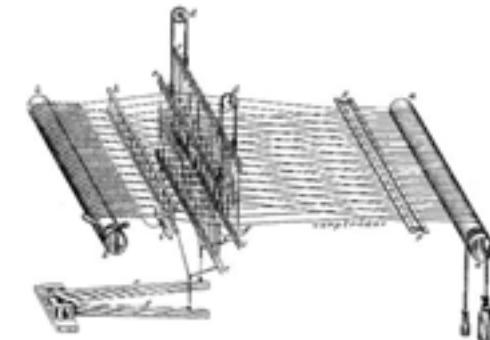
Example Exemple
.Mesh Fabrics Tissus à mailles

Transitional Techniques



Example Exemple
.Braiding Tresser
.Plaiting with active systems
natter avec systems active

Advanced Textile Techniques



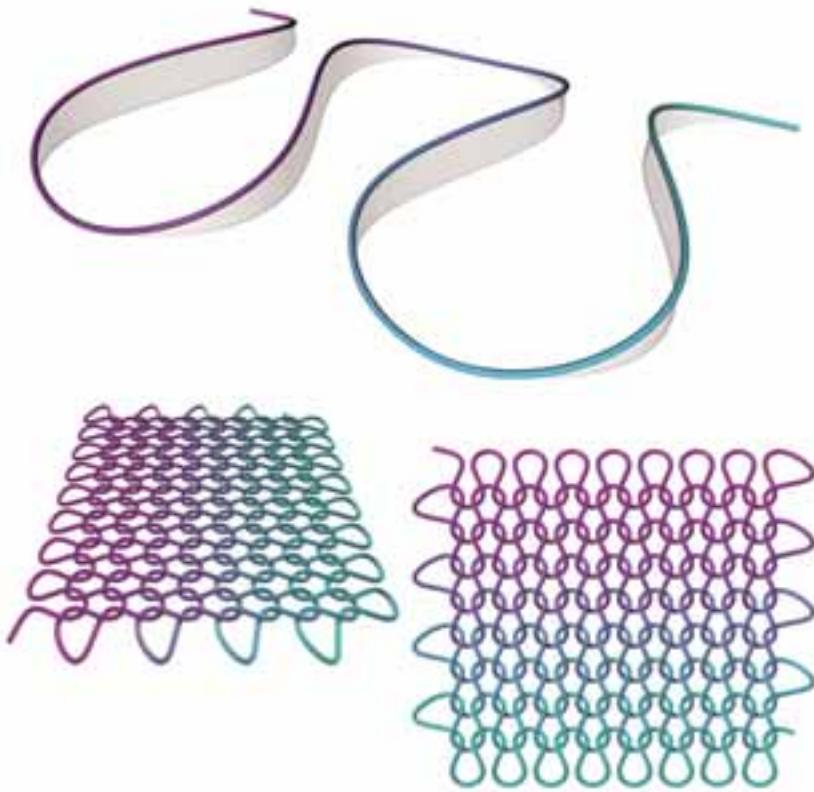
Example Exemple
.Weaving Tisser

Markus Hudert

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Basic Textile Techniques

Felting, meshing, plaiting, weaving

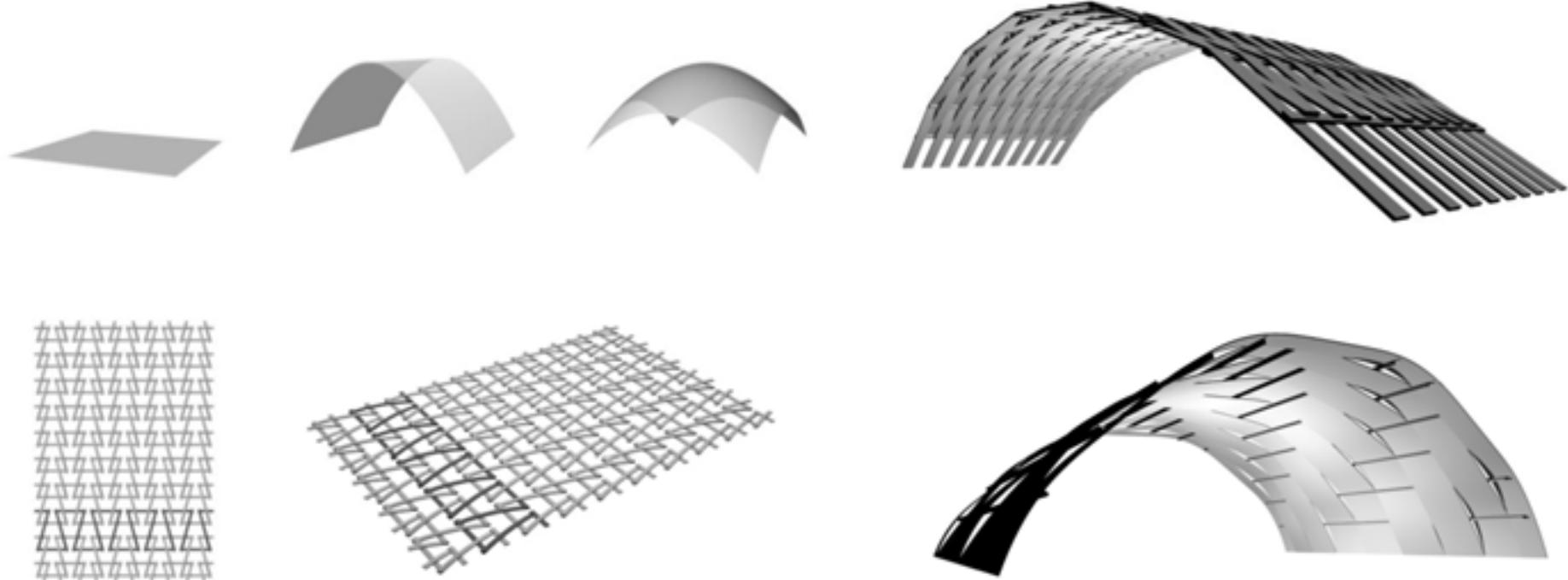


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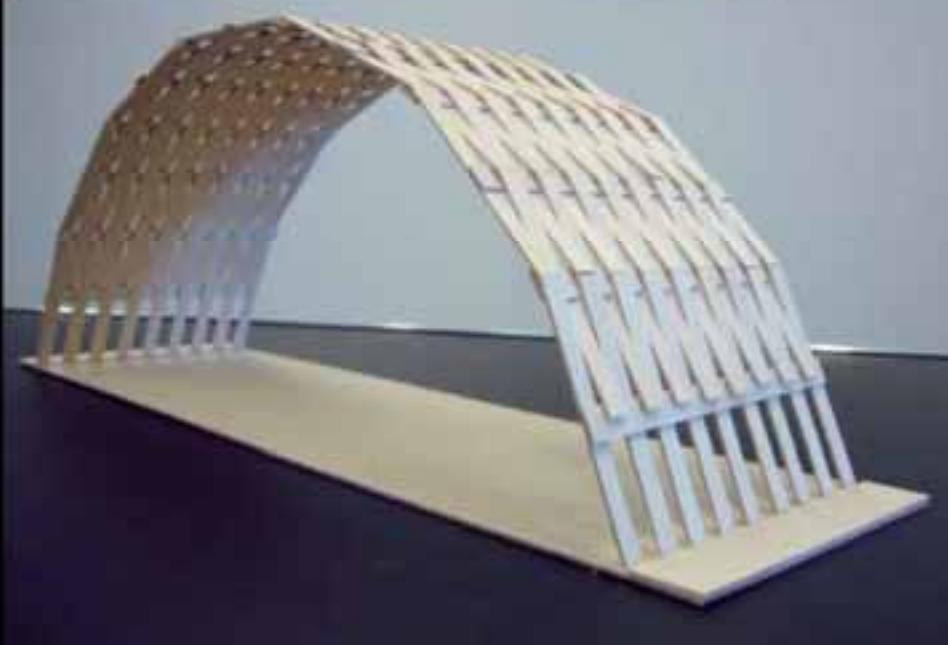
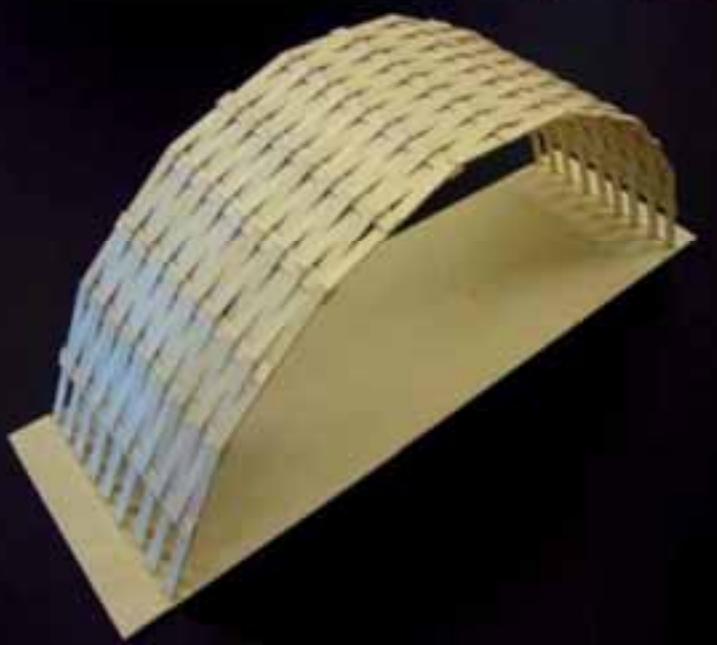
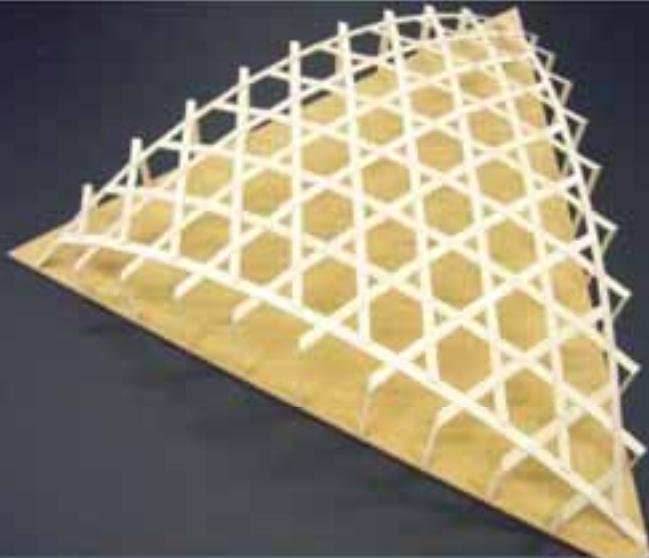
A matter of scale

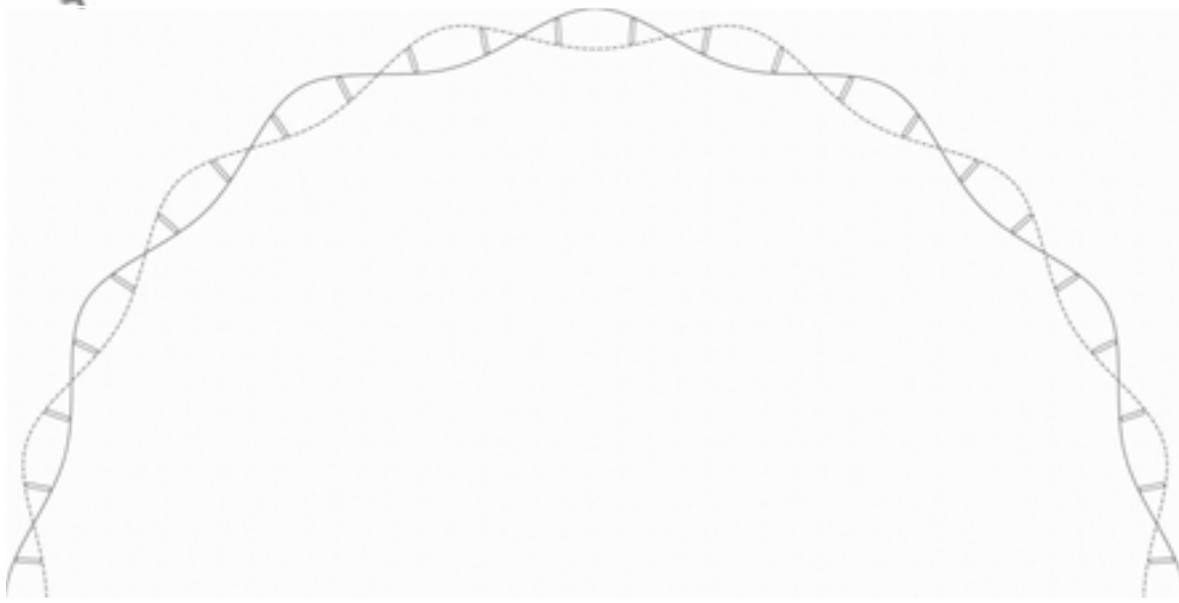
Changes in material, geometry and behaviour



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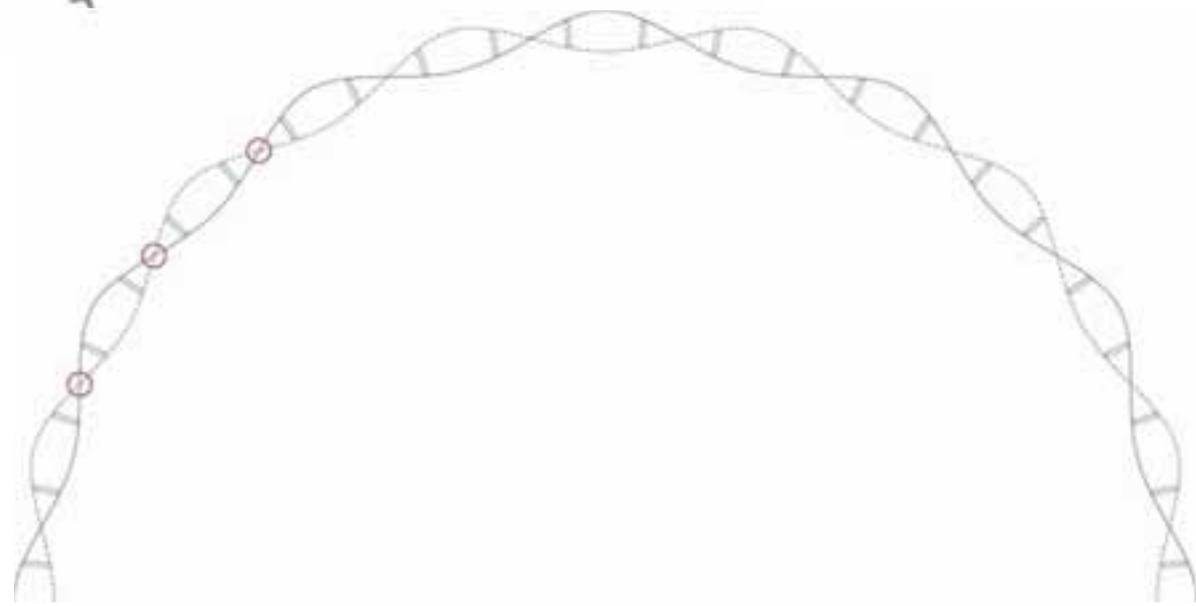
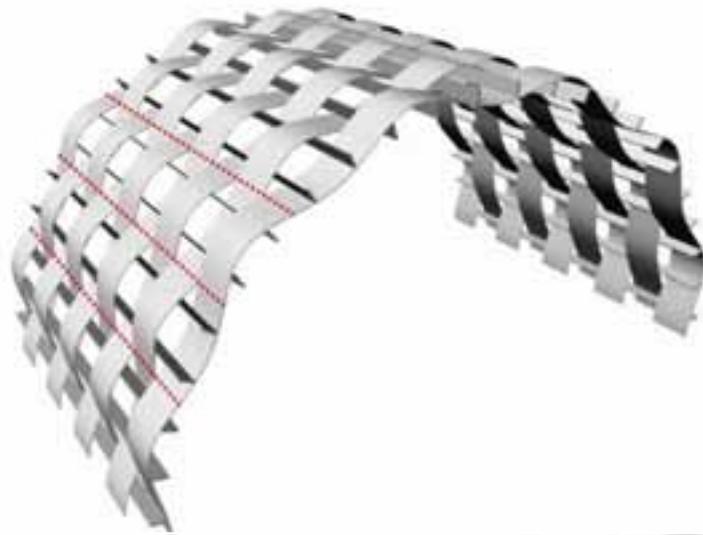




Markus Hudert

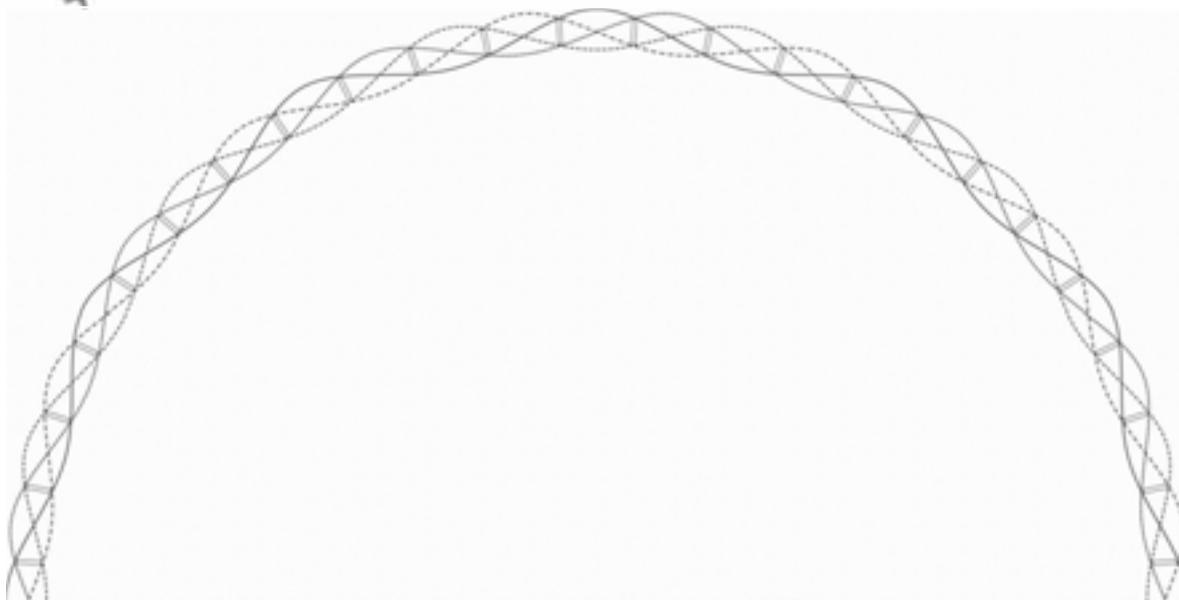
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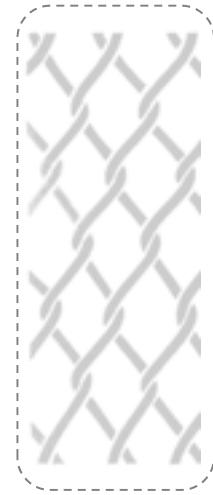
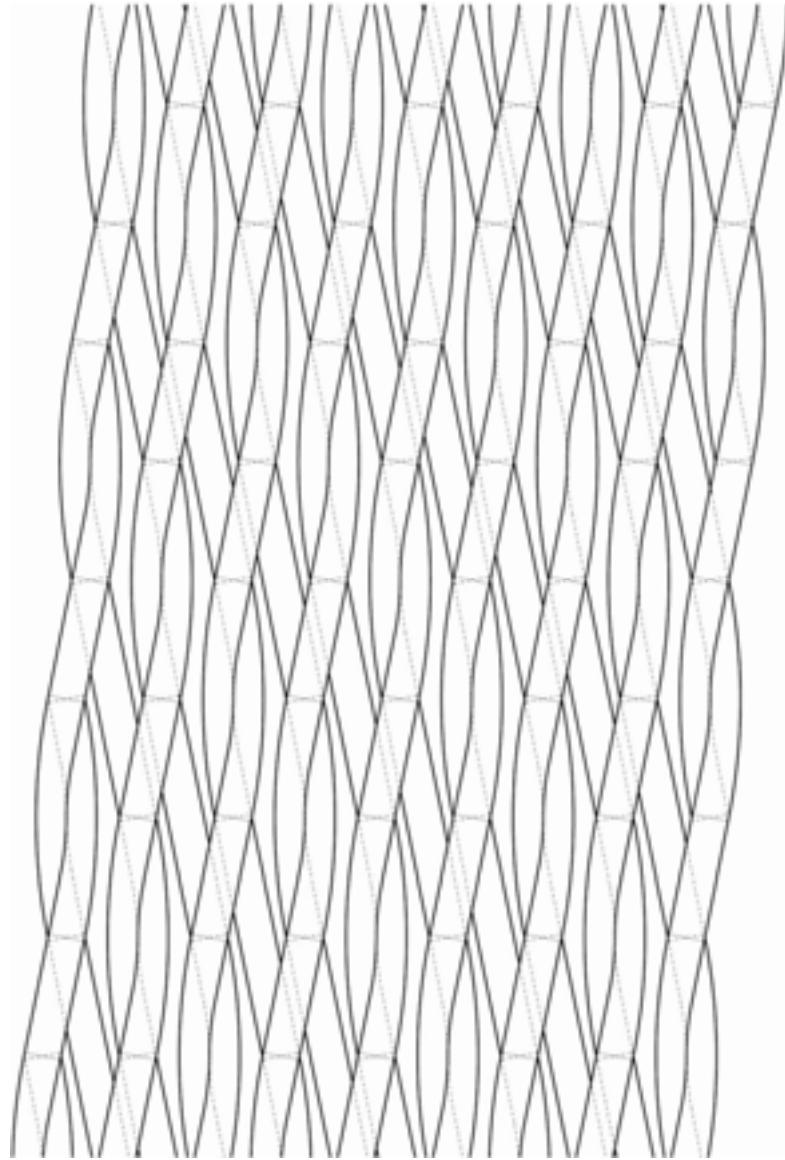


Markus Hudert

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Yves Weinand

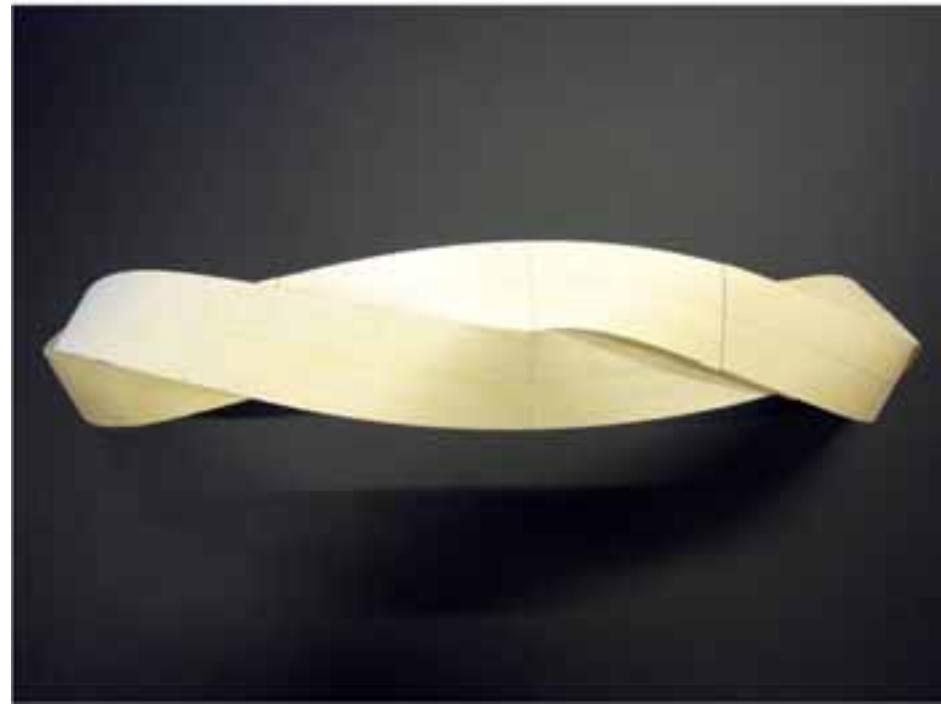
iBOIS EPFL
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,Sprang' Structure



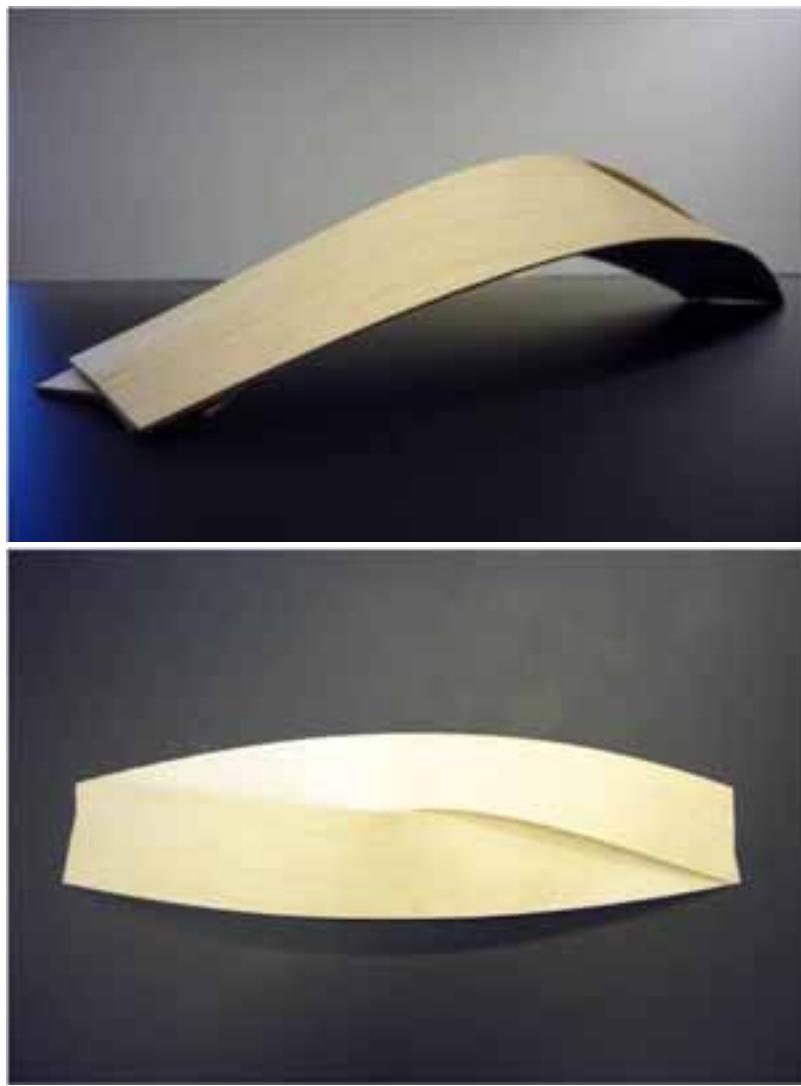
Markus Hudert

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Yves Weinand



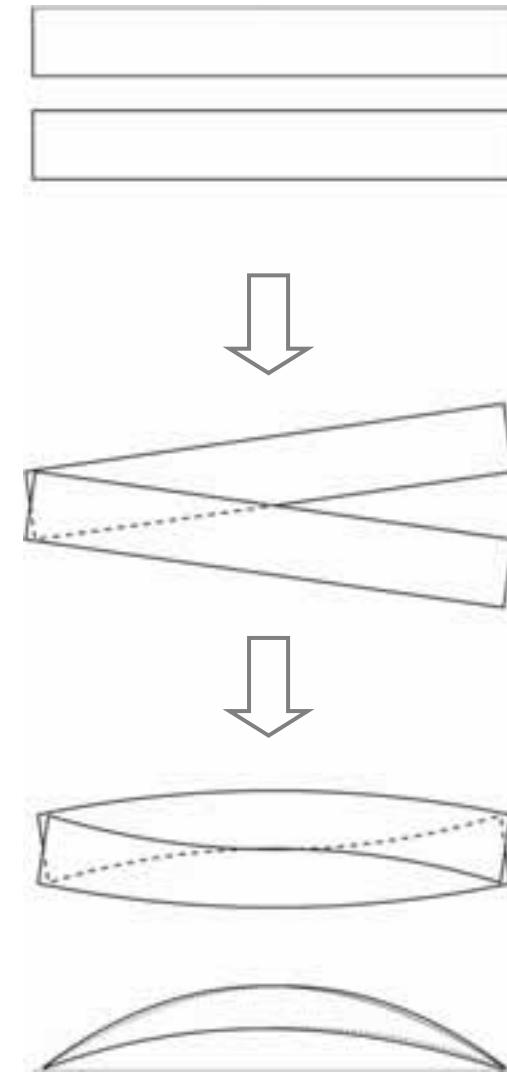
Markus Hudert, Masoud Sistaninia

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Yves Weinand



Markus Hudert

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Yves Weinand





Markus Hudert

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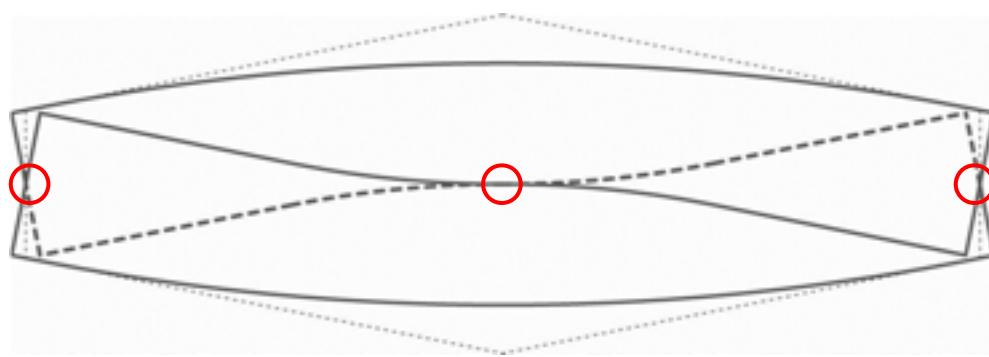
Markus Hudert

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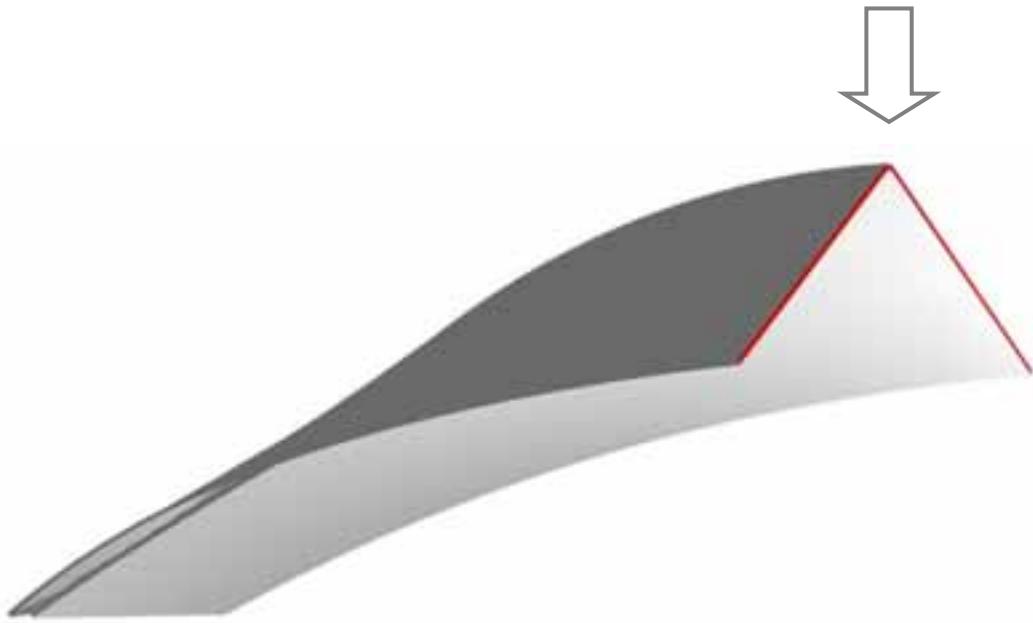


Fixpoints



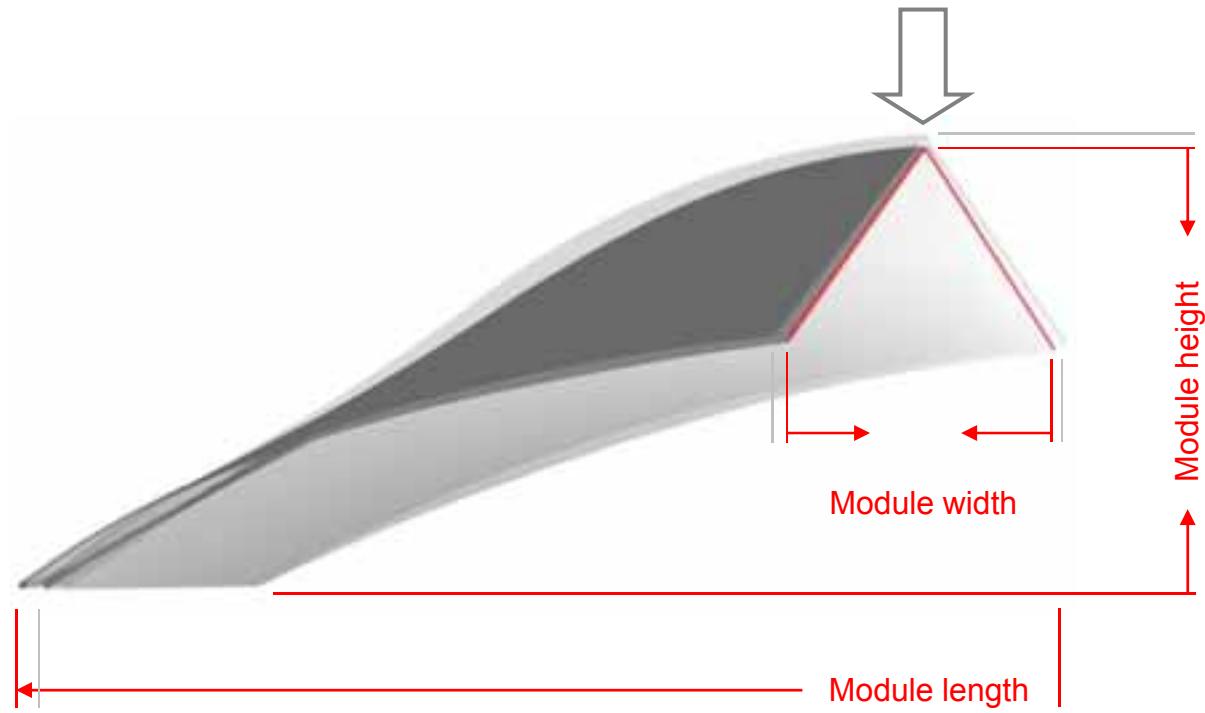
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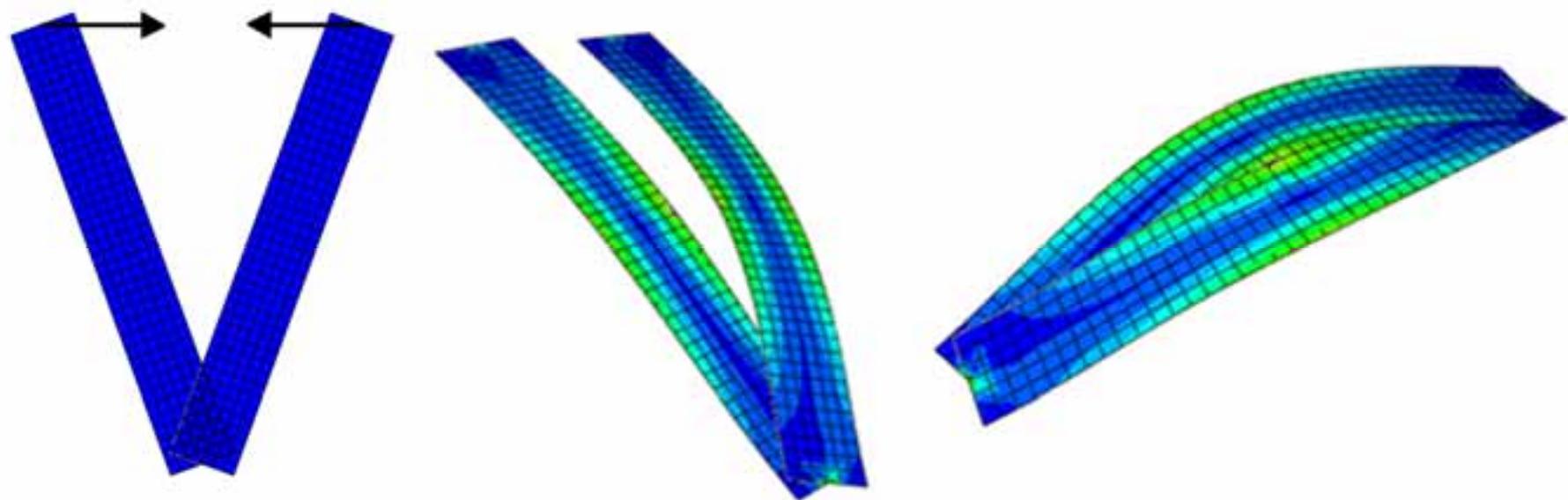
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Calculation of internal stresses in textile modulus

Finite Element software (ABAQUS 6.7-1) was used for this analysis

Simulated by FEM software:



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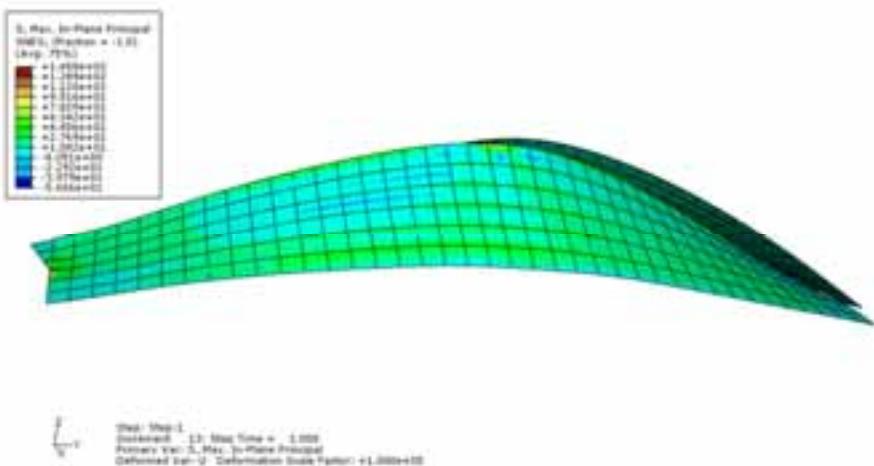
Maximum principal internal stresses for two proportion

Proportion (length/width)= 7

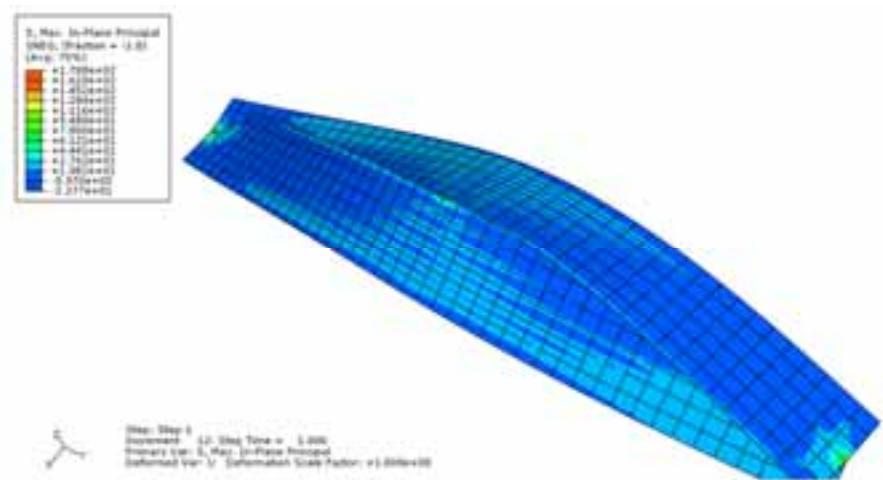
Length= 11.55 m, Width= 1.65 m

Proportion (length/width)= 8.7

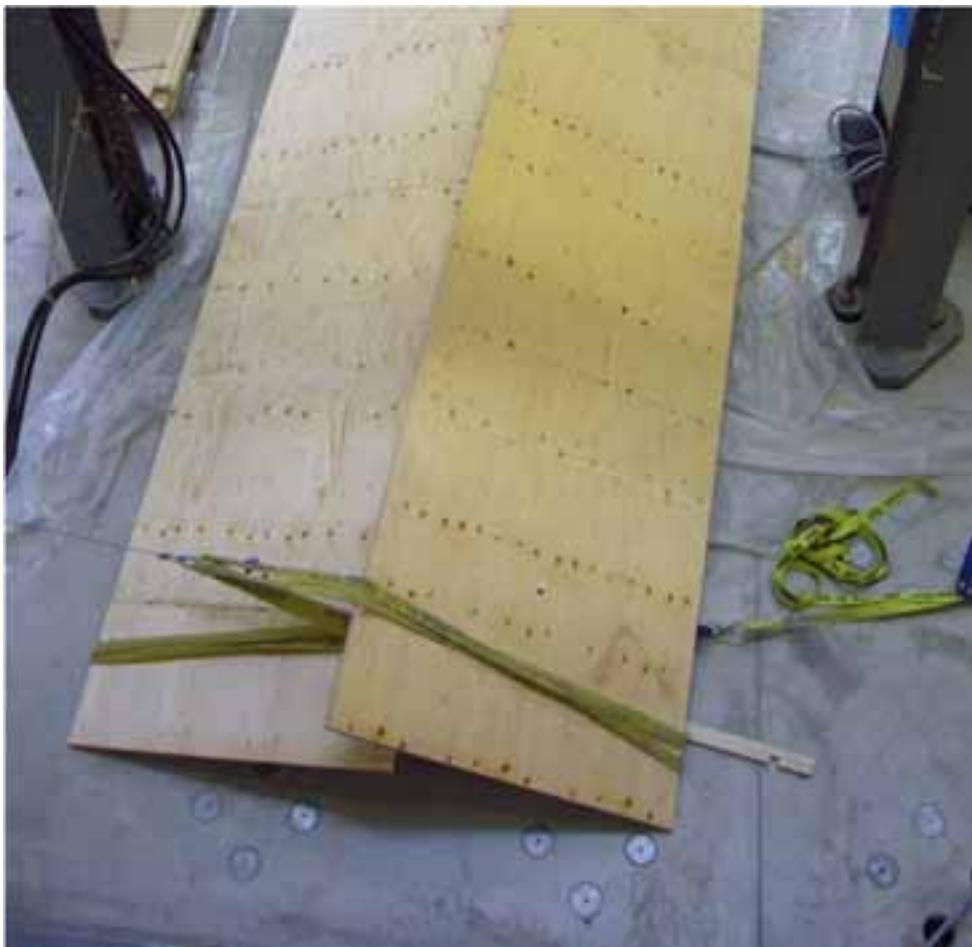
Length= 11.55 m, Width= 1.32 m



Maximum Principal stress= 46 MPa



Maximum Principal stress= 29 MPa



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Conclusion of this analysis

According to ABAQUS results, proportion ≥ 8.7 is safe for Plywood material with $E=8800$ Mpa, tensile strength= 26 MPa

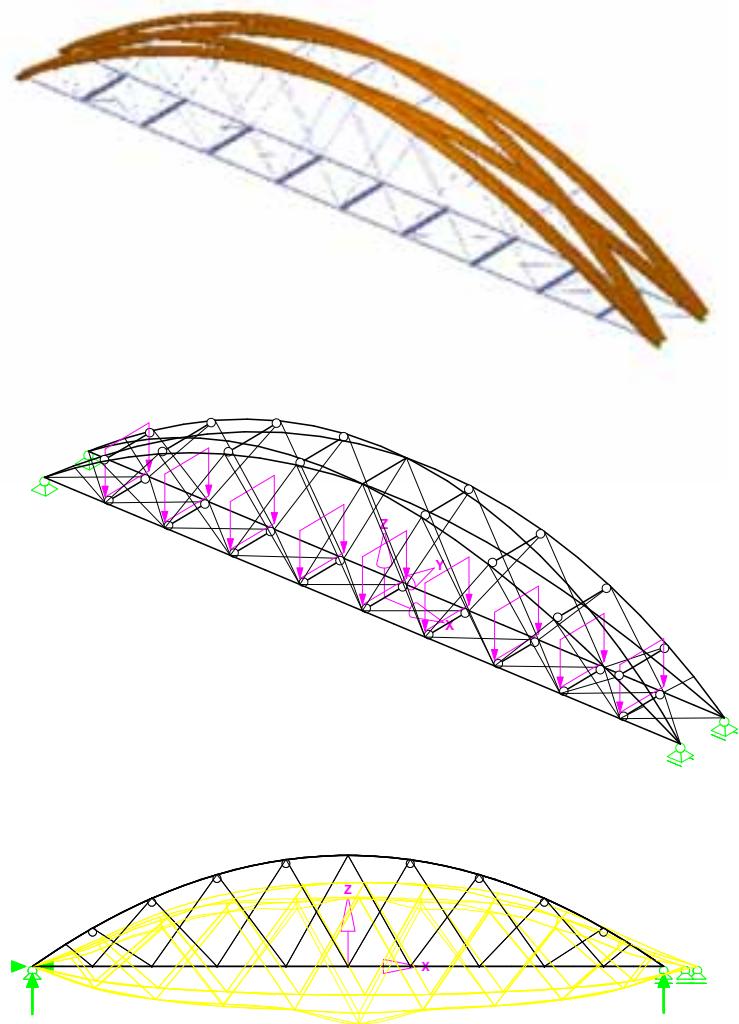
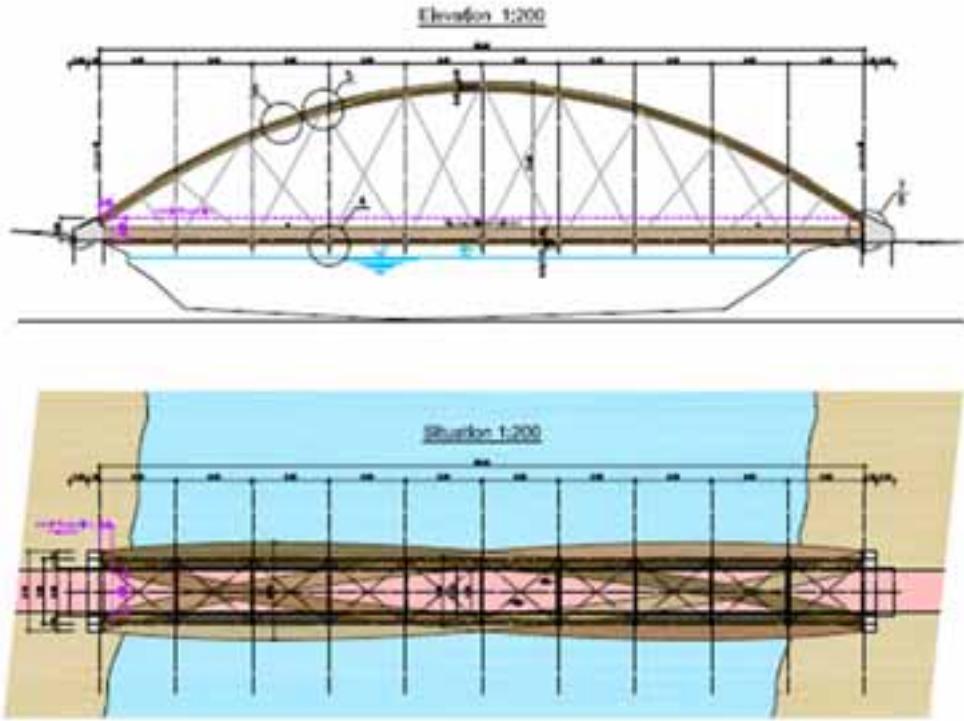
Prototype

The modulus with proportion of 8.7 was built in the laboratory



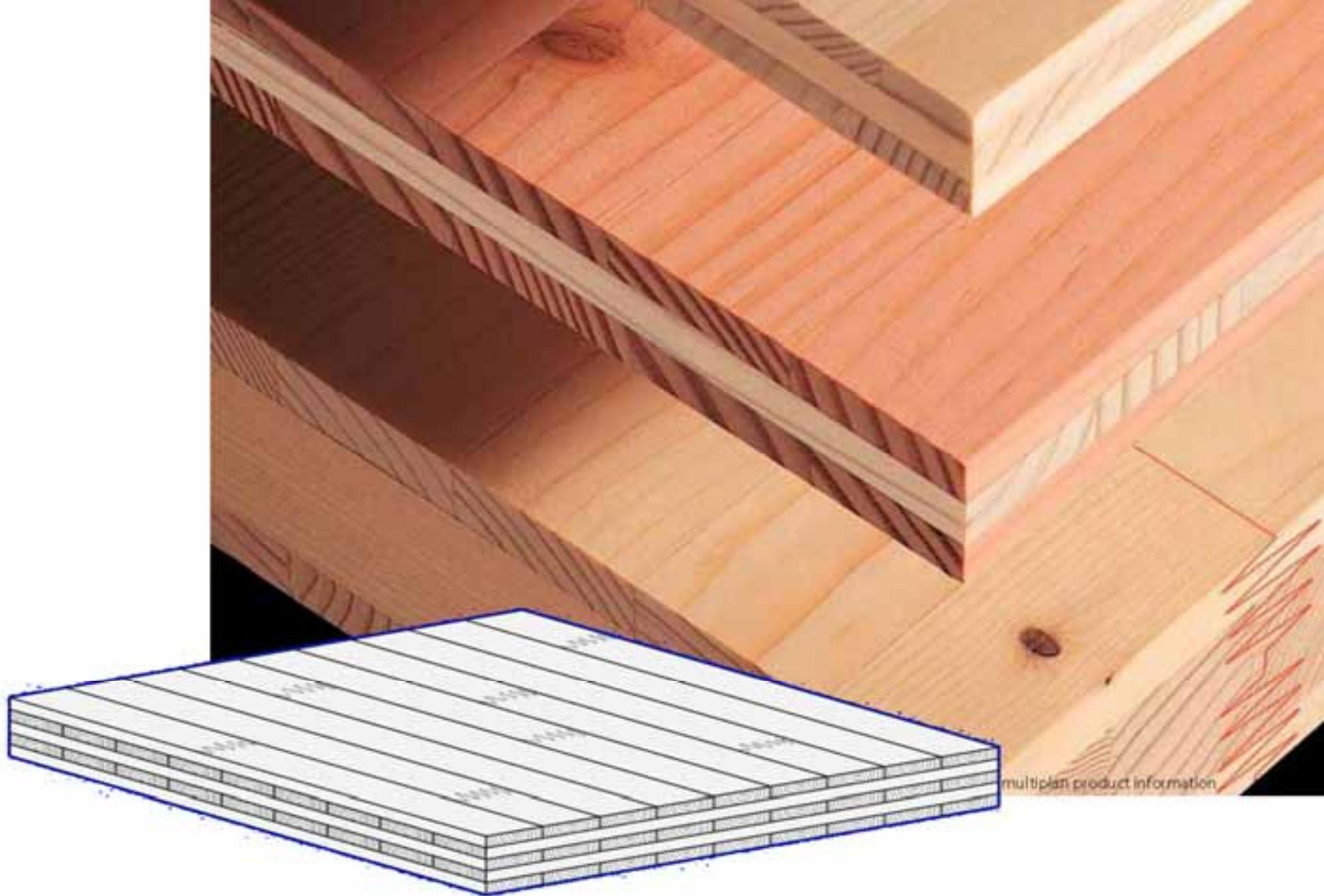
Masoud Sistaninia

Passerelle tressée



Student Richard Thürler

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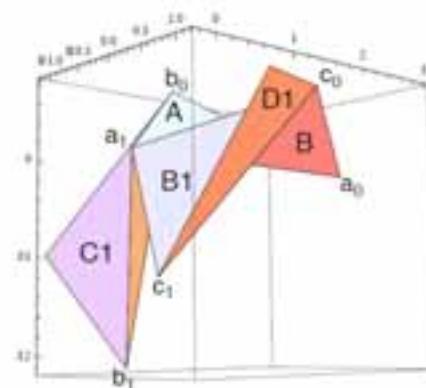
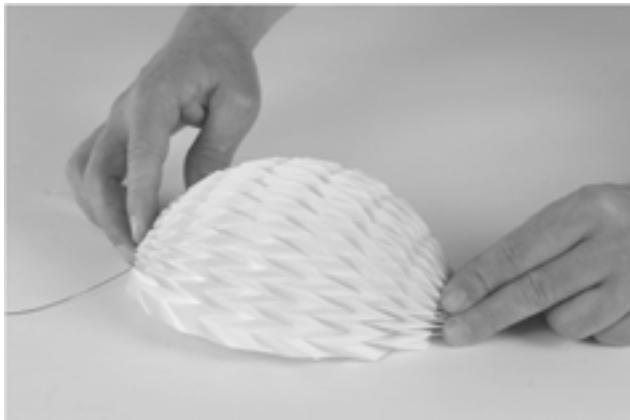
multiplan product information



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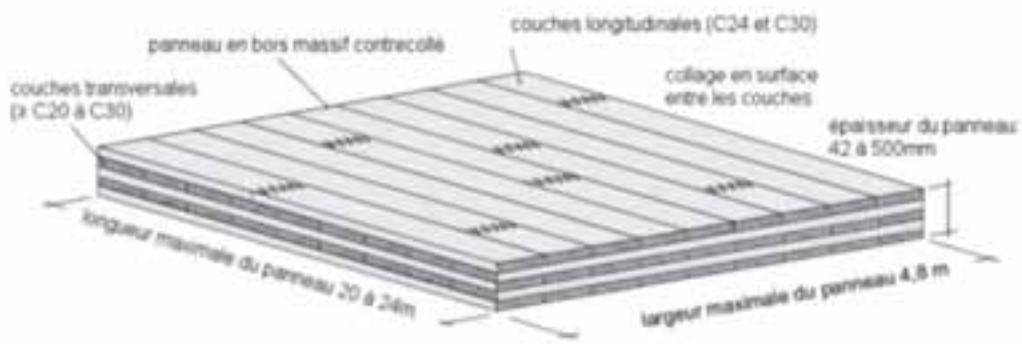
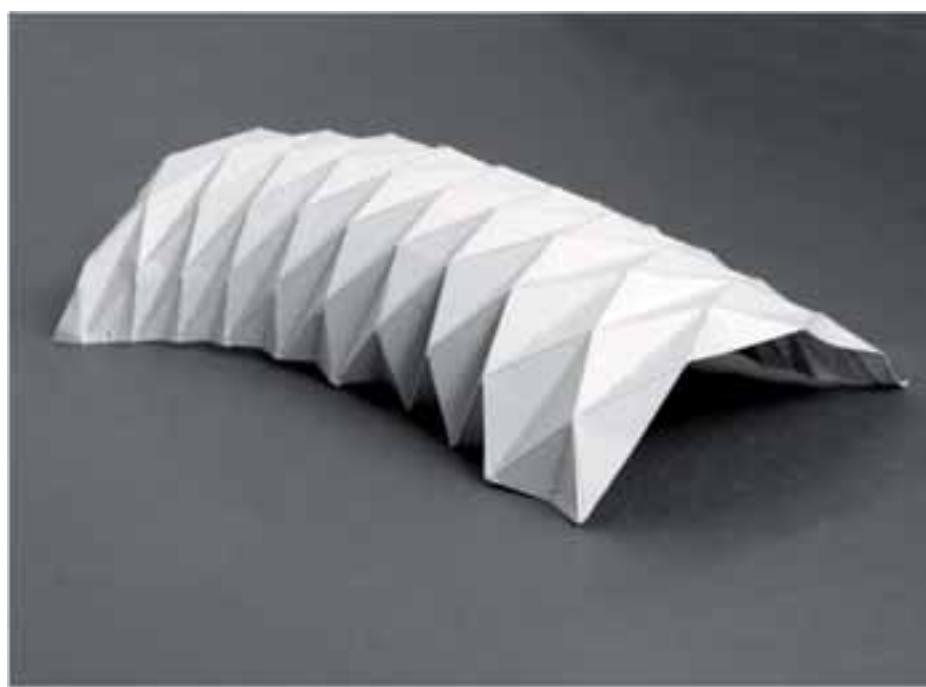
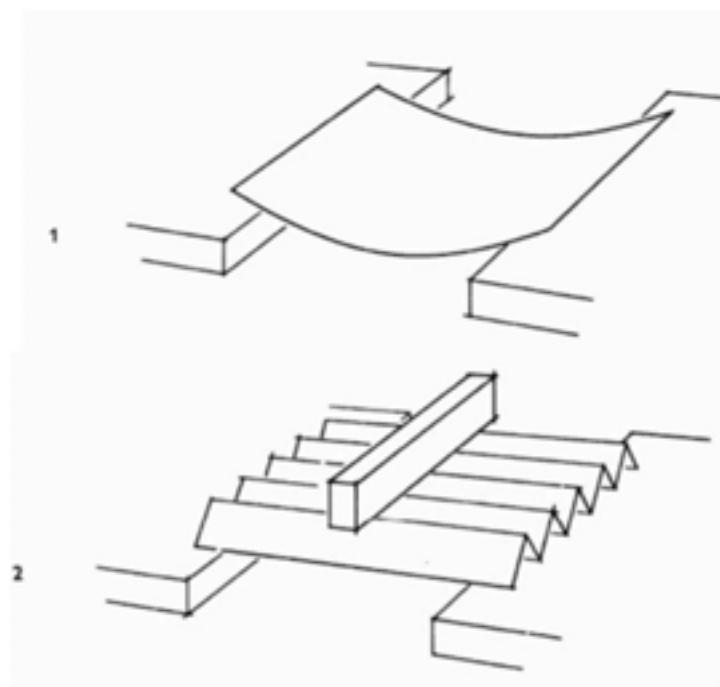
Origami – Folded Plate

An interdisciplinary research between architects, engineers and mathematicians



Hani Buri, François Demoures

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Yves Weinand

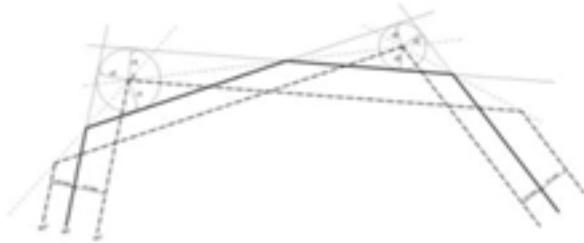


Hani Buri

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Method

- Form-finding
- Analysis of the geometry
- Prototypes

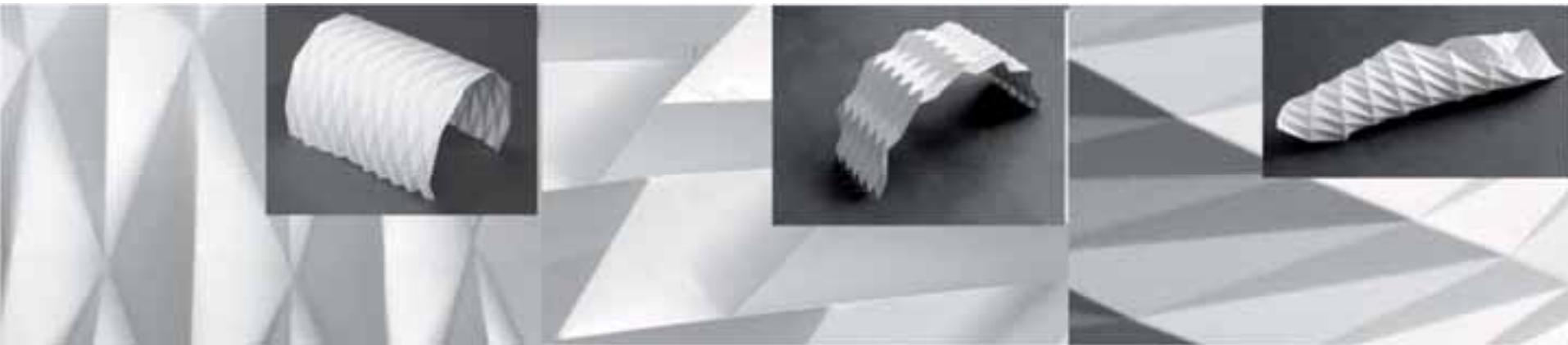


Hani Buri

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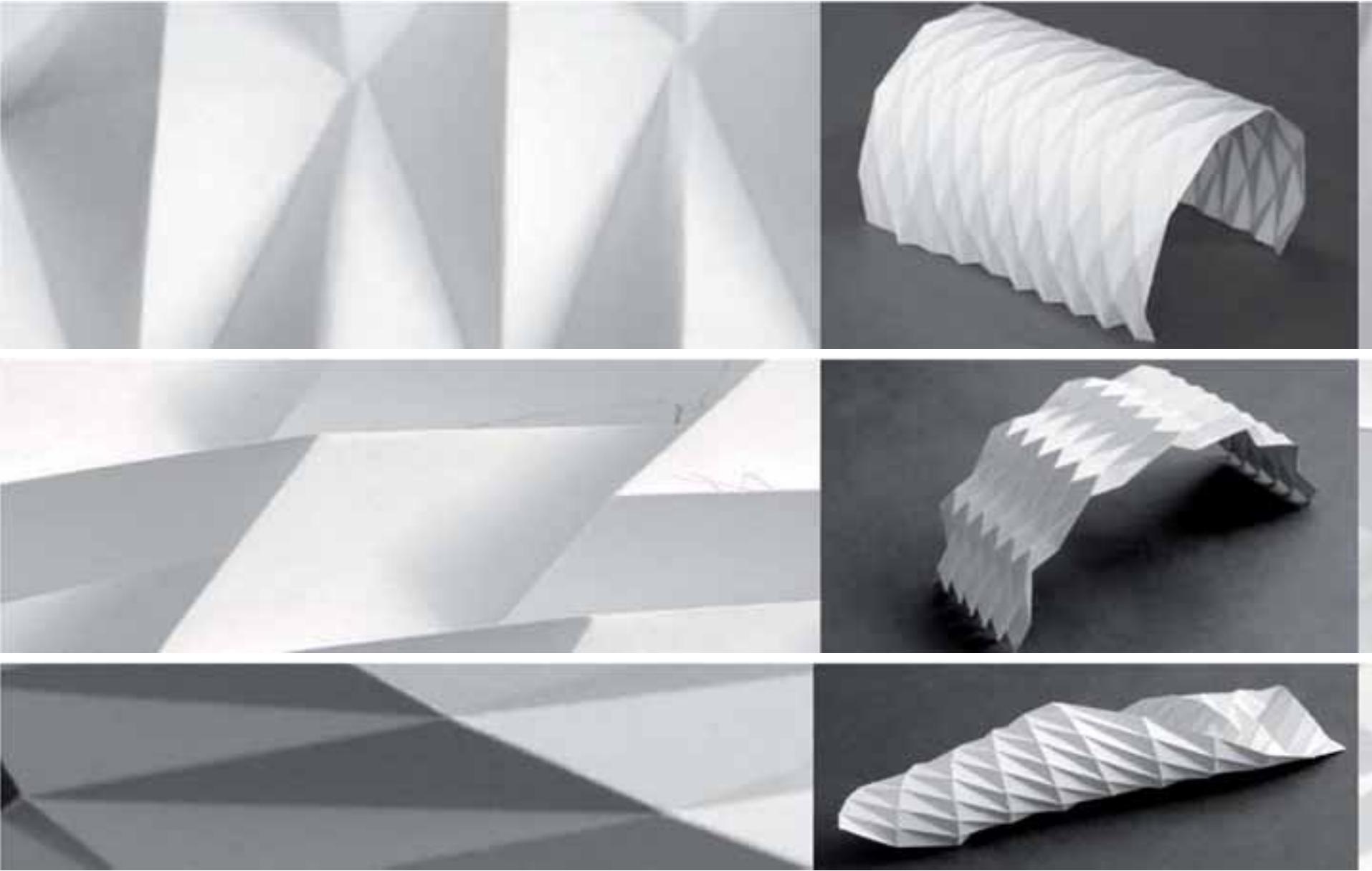
Patterns

- Diamond
- Herringbone
- Diagonal



Hani Buri

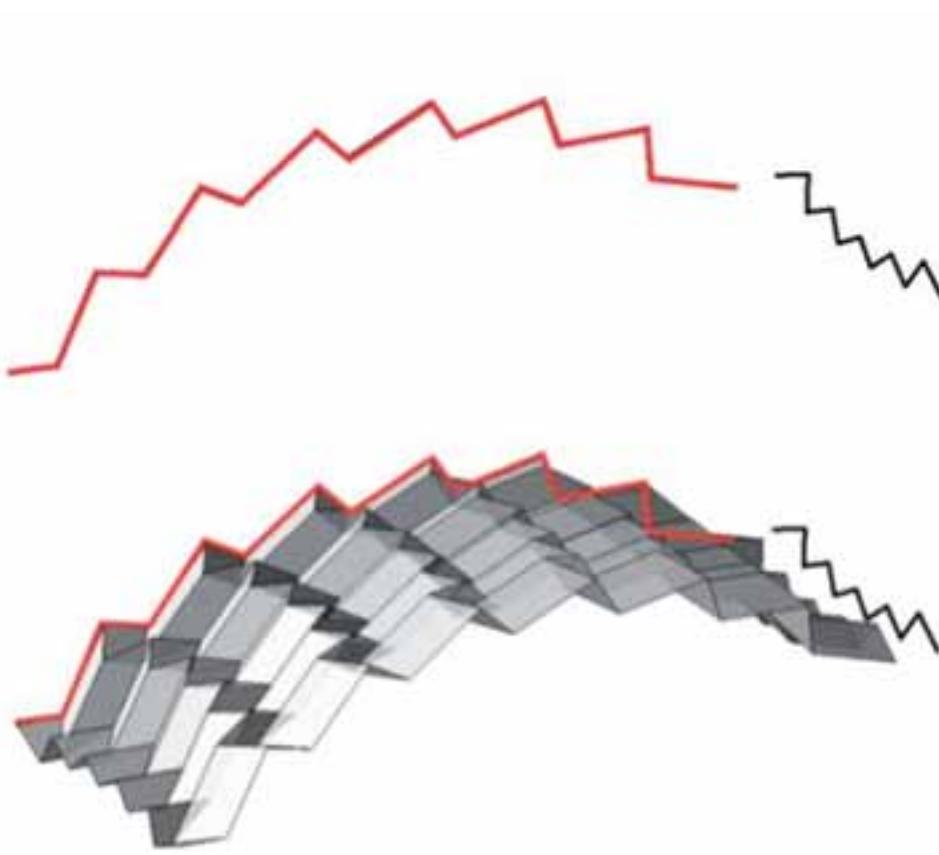
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Numerical pattern generation

Two profiles generate a folding pattern



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Prototype



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Origami, engineering Goal

Provide tools that allow an economic and easy realisation of folded constructions made from cross glued timber panels

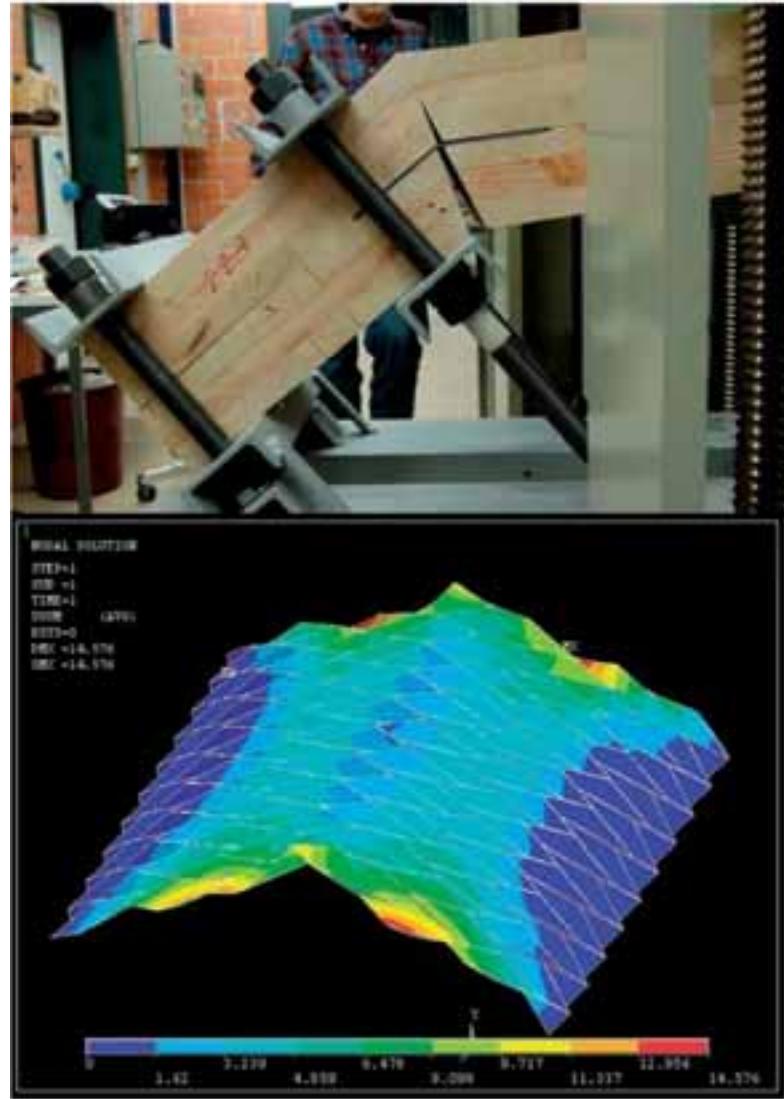


Hani Buri

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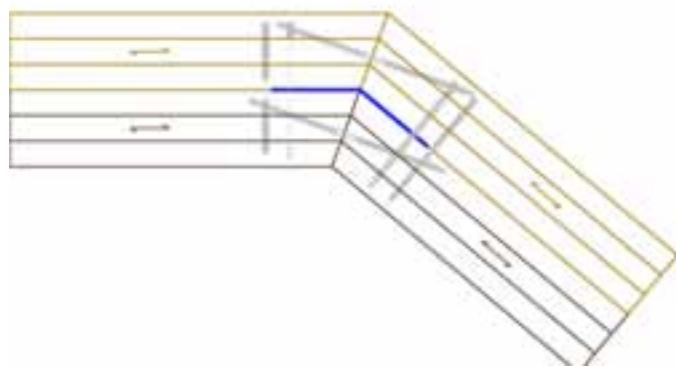
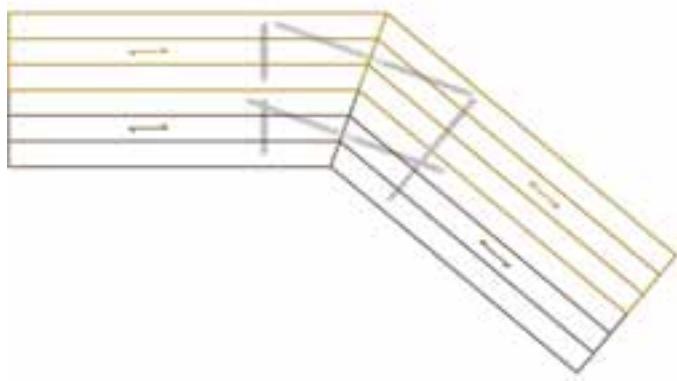
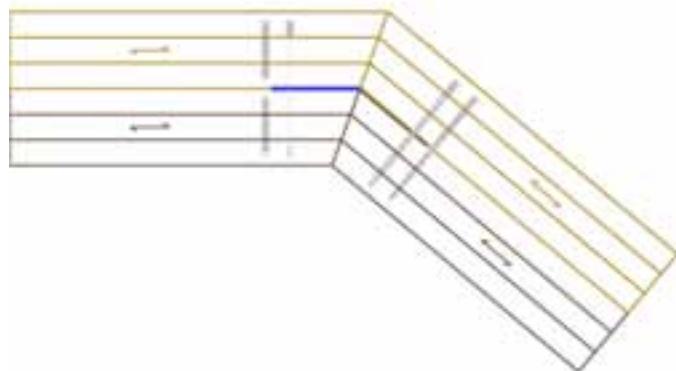
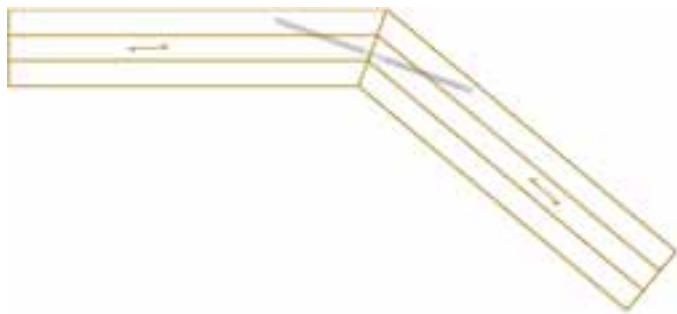
Methods

Both numerical simulation and laboratory testing contribute important information



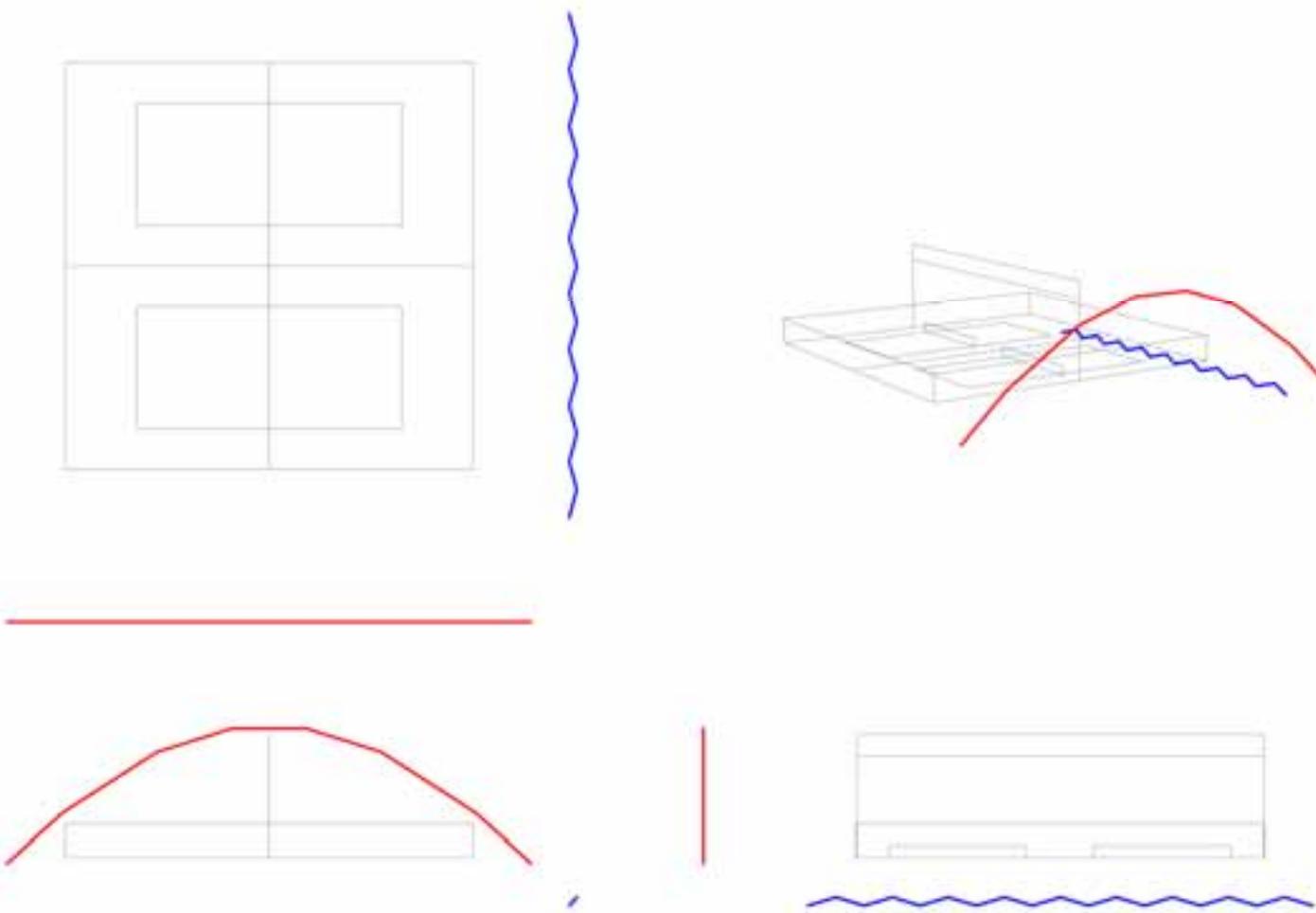
Hani Buri

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Yves Weinand



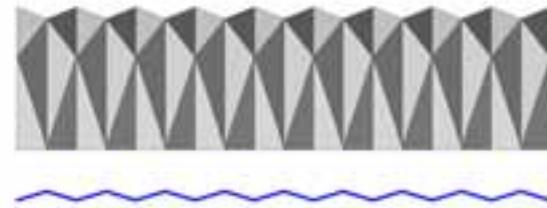
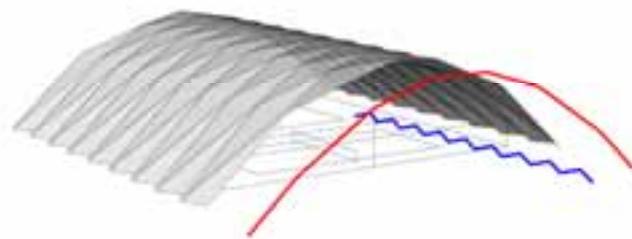
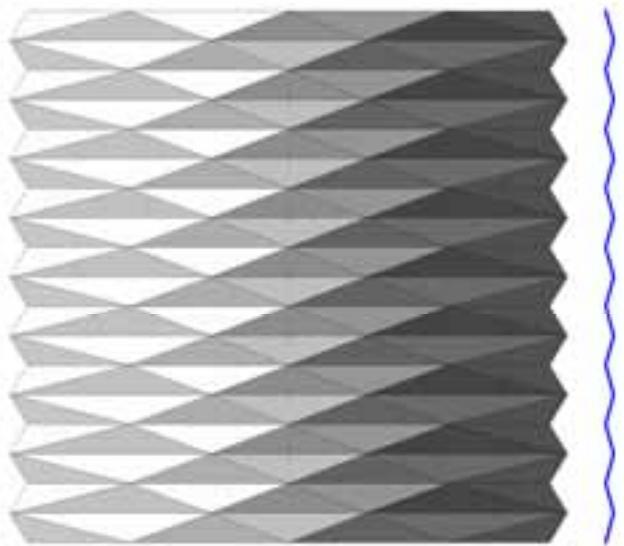
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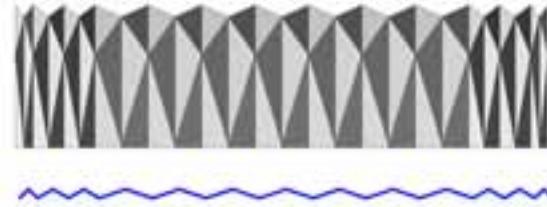
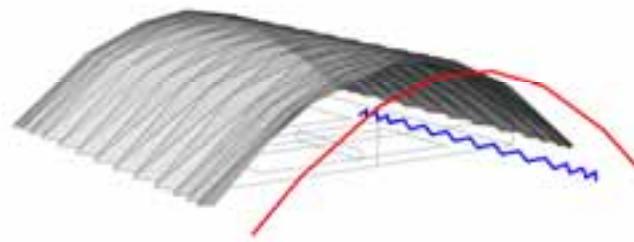
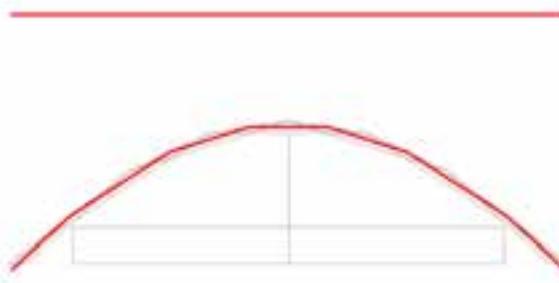
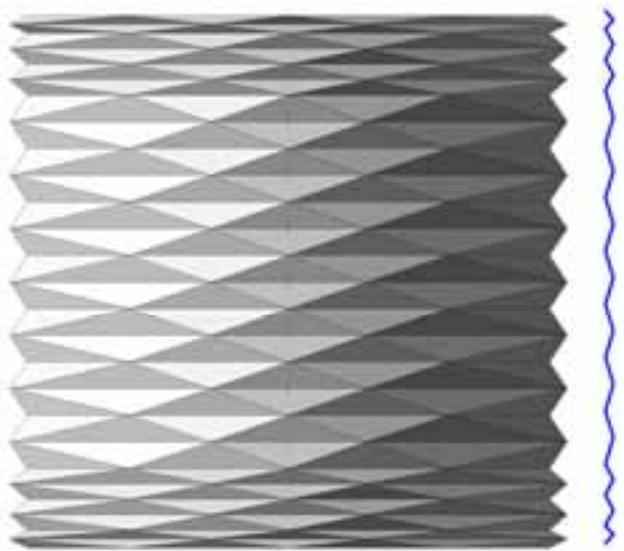
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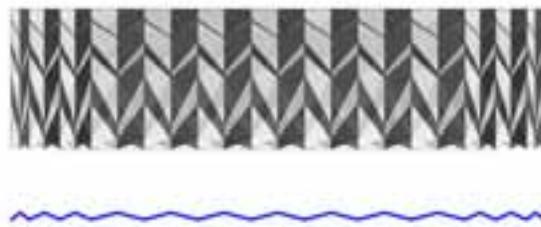
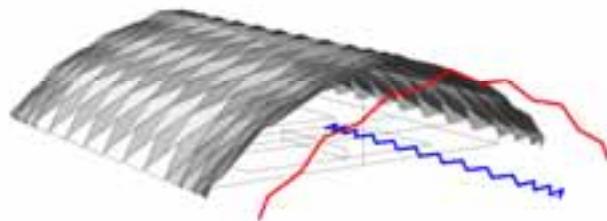
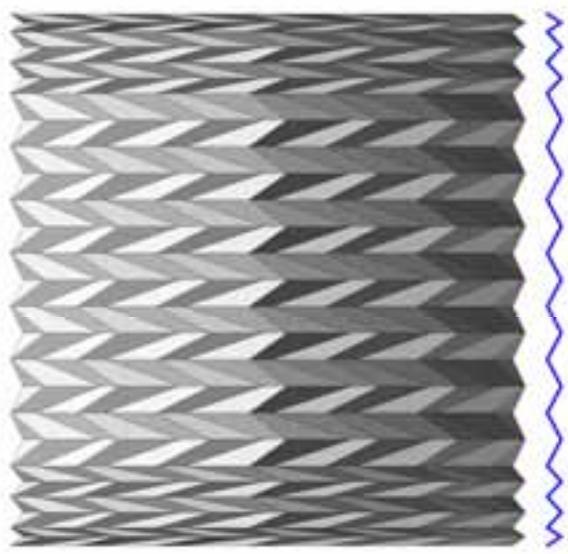
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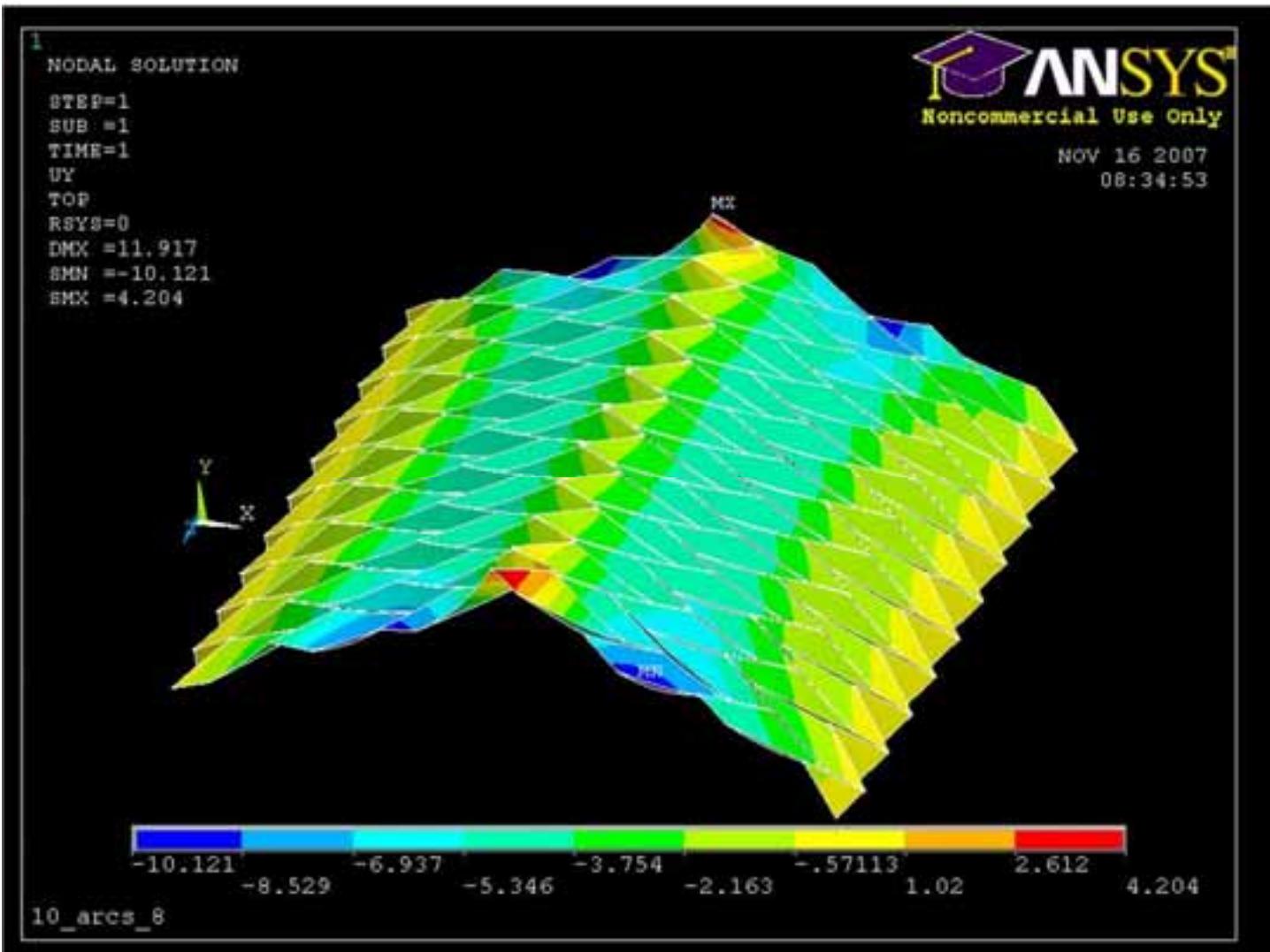
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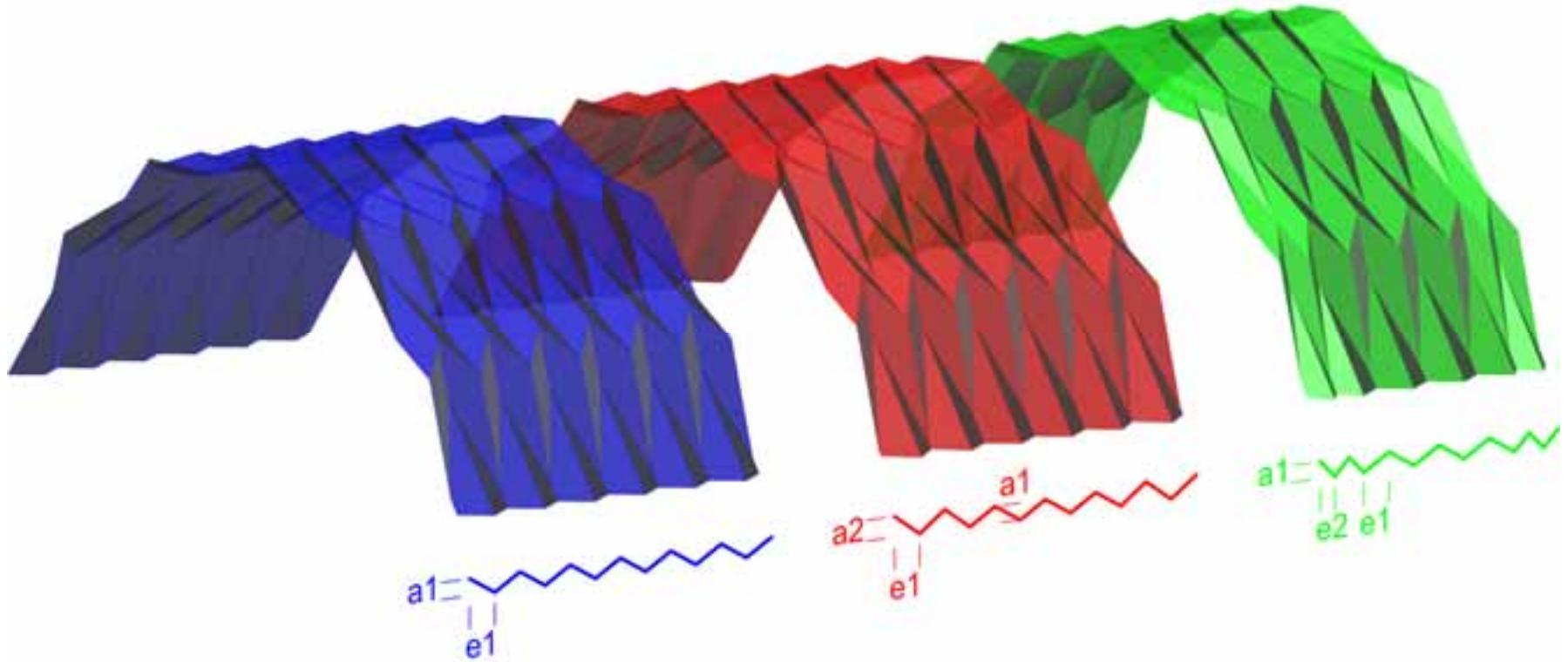
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Variations of amplitude and extension of a folded plate structure:

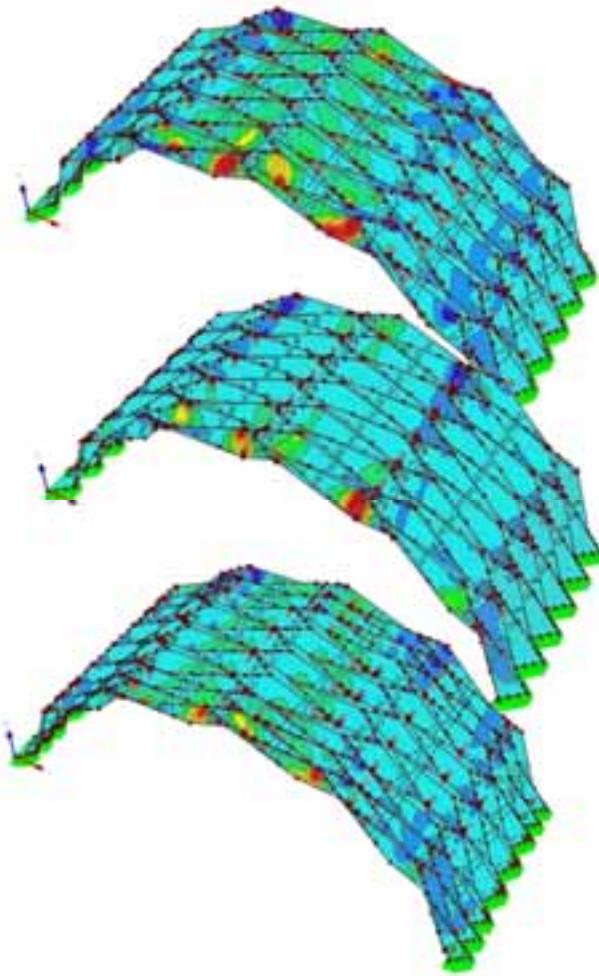


1. amplitude a_1 constant
extension e_1 constant

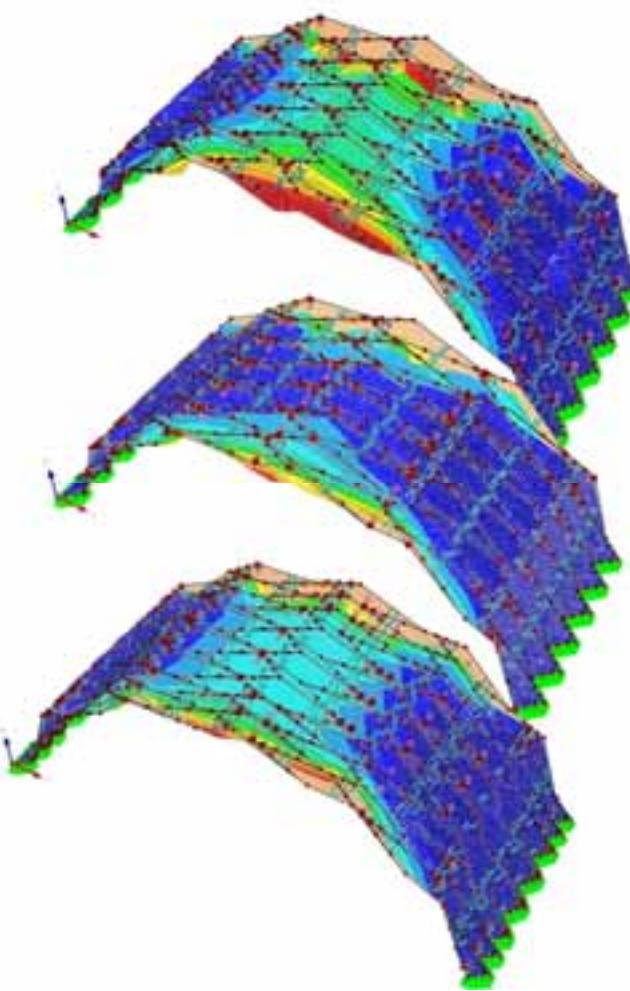
2. amplitude $a_2 > a_1$
extension e_1 constant

3. amplitude a_1 constant
extension $e_2 < e_1$

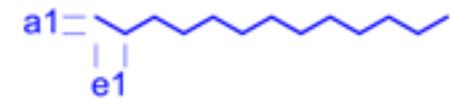
Internal forces



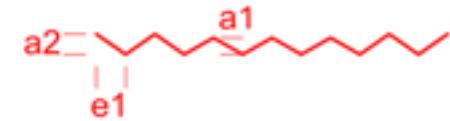
Deformations



1. Max vectorial displacement 3.3 mm



2. Max vectorial displacement 2.2 mm

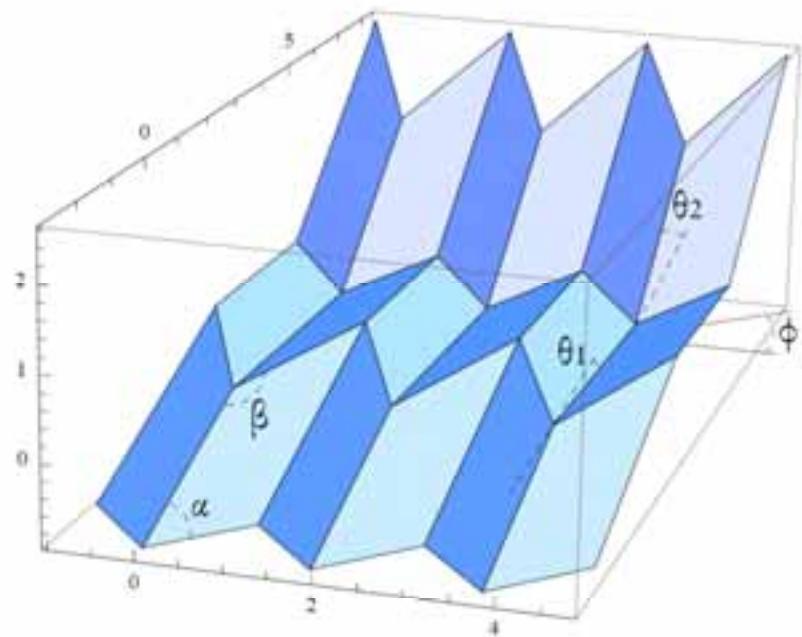
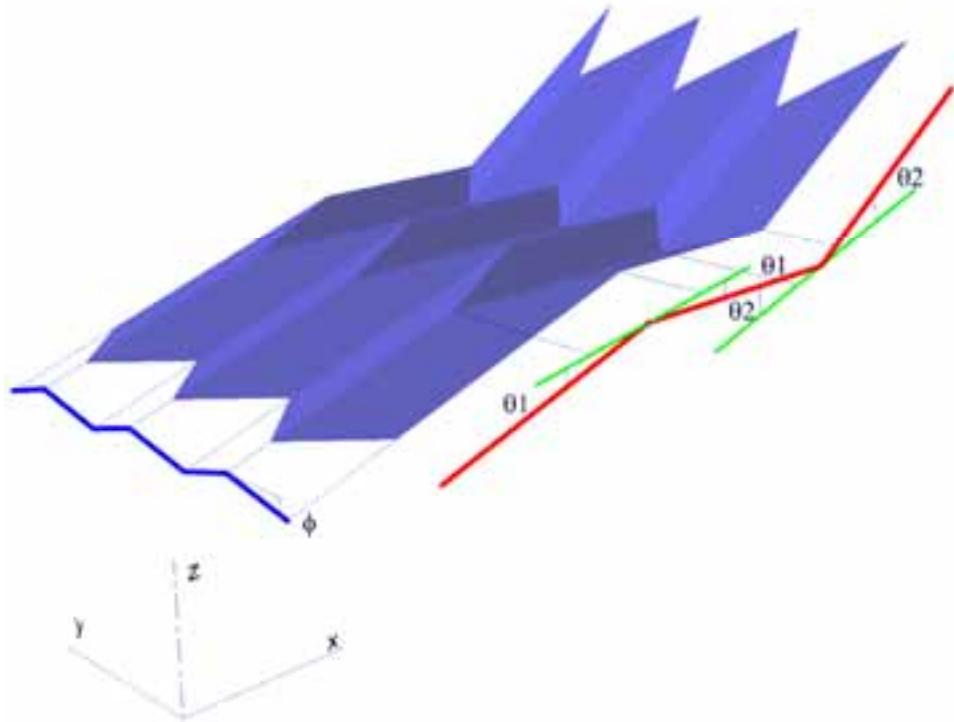


3. Max vectorial displacement 1.9 mm



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$$\theta_1 = \text{ArcTan}(\text{Sin}(\phi) \tan(\alpha))$$

$$\theta_2 = \text{ArcTan}(\text{Sin}(\phi) \tan(\beta))$$

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IFS surface design for timber constructions

An interdisciplinary research between architects,
mathematicians and computer scientists

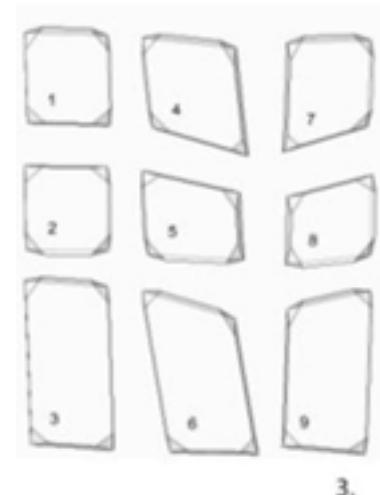
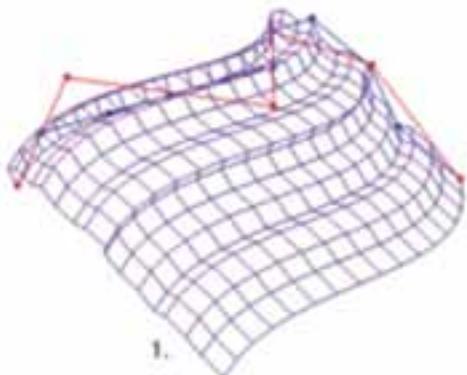


Gilles Gouaty, Ivo Stotz

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Goal

Computer-aided solutions for the production of complex free-form architecture



```
%prog2  
N1 G90  
N2 G71 T1 M6  
N3 GO X93.0203260604704 T62.5742002389265  
N4 G1 Z-3  
N5 G1 X92.5173637881376 T32.3964638989584  
N6 G1 Z6  
N7 GO X108.361877416248 T60.3013778158484  
N8 G1 Z-3  
N9 G1 X107.858915143915 T30.1236414758803  
N10 G1 Z6  
N11 GO X96.8557138994148 T62.005994633157  
N12 G1 Z-3  
N13 G1 X96.352751627082 T31.8282582931889  
N14 G1 Z6  
N15 GO X104.526489577304 T60.8695834216179  
N16 G1 Z-3  
N17 G1 X104.023527304971 T30.6918470816498  
N18 G1 Z6
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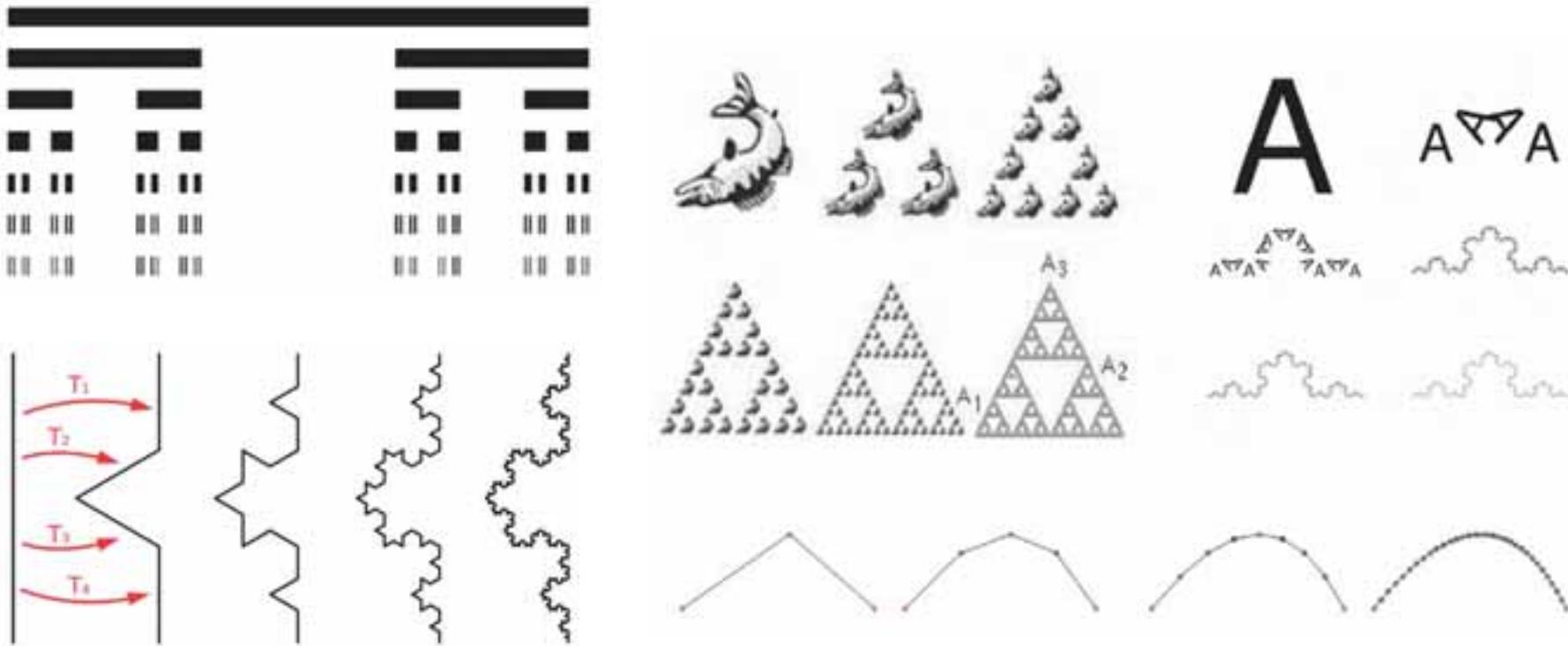


Digital production of free-form architecture

1. Free Surface design
2. Computing the constructional elements
3. Addressing and lay out of the elements
4. Machine code generation
5. Integrated manufacturing

Mathematical Background

Of monster curves and Iterative geometric figures

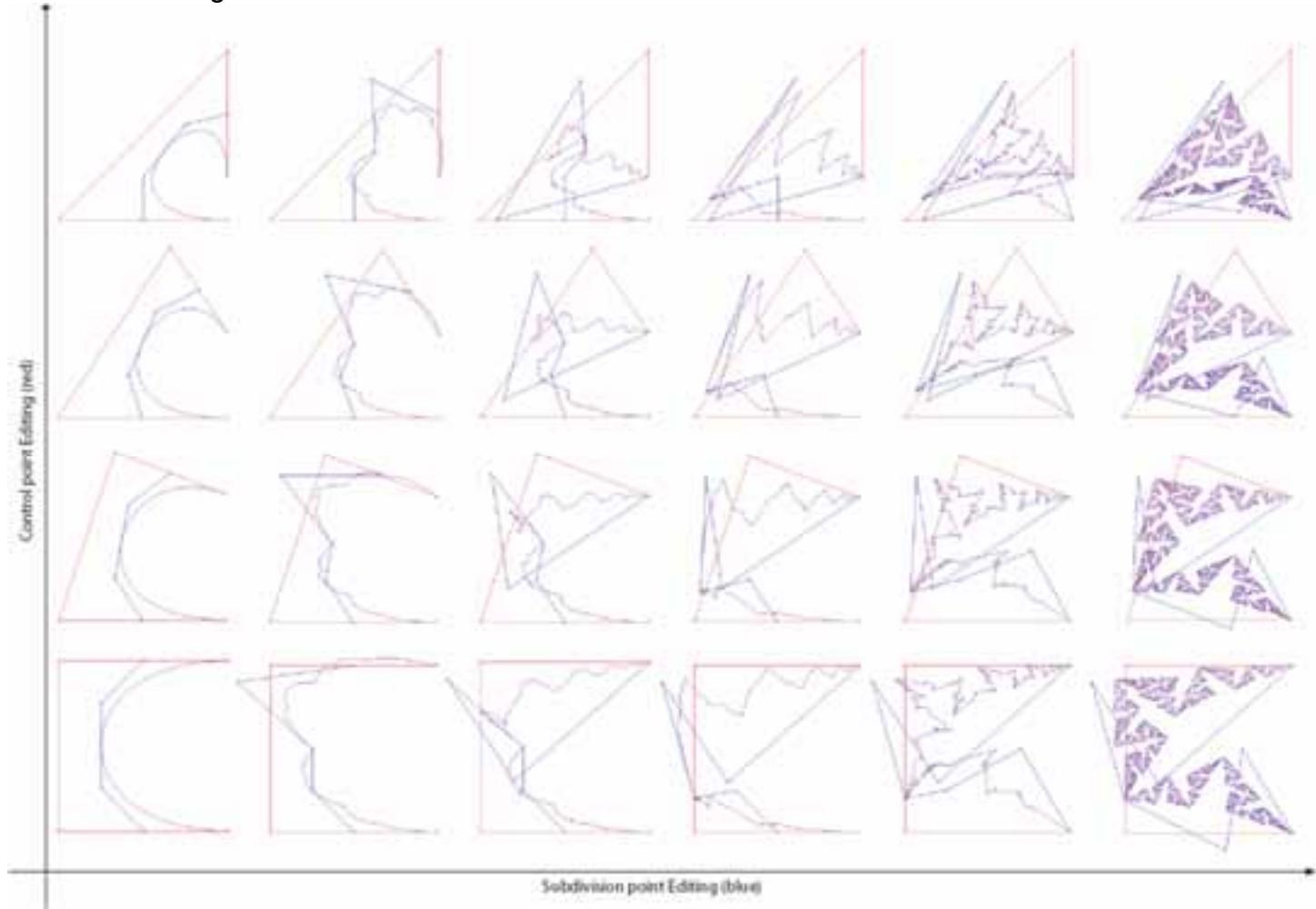


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Software Development

How to: discrete curve design

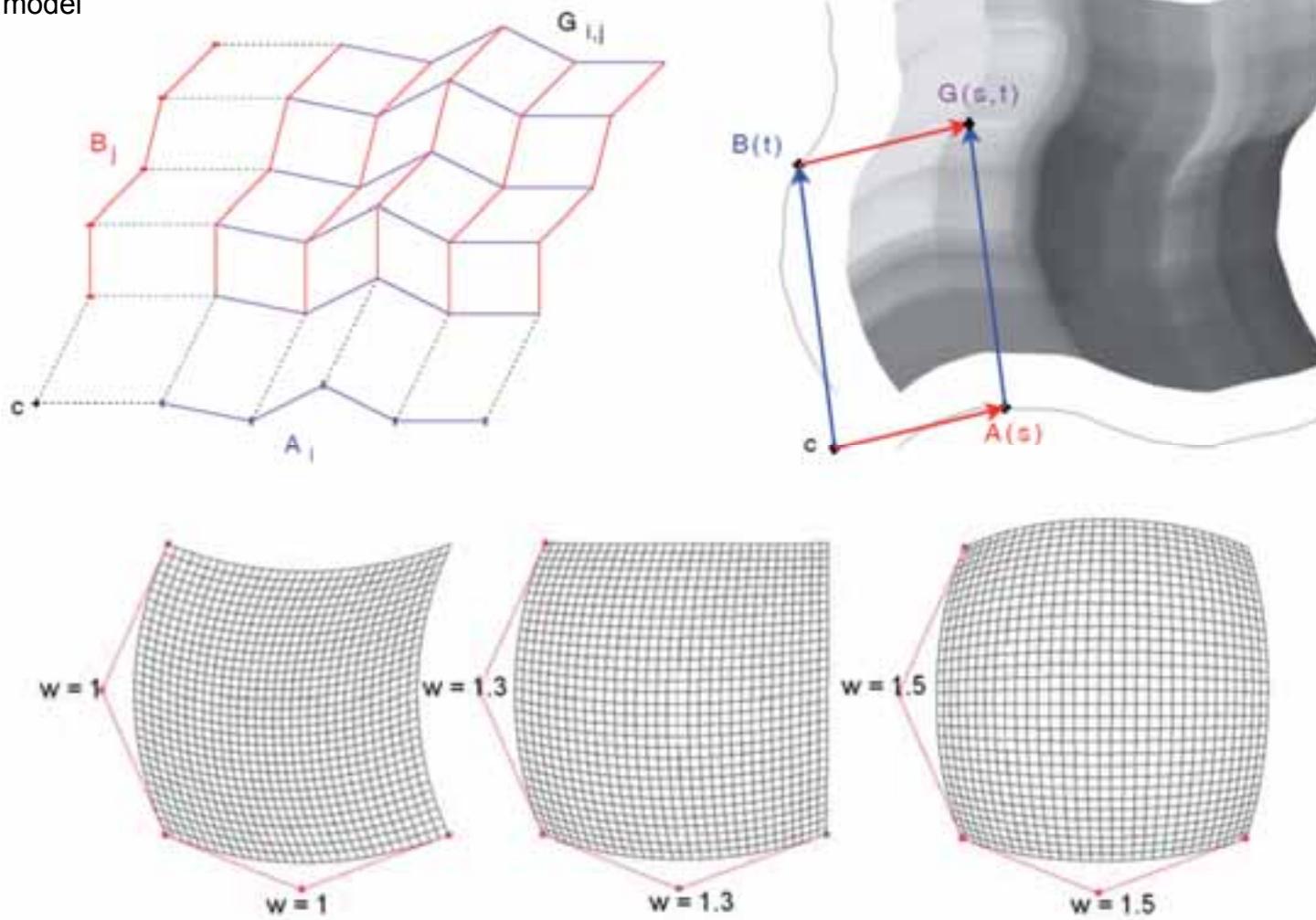


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Software Development

A new surface model

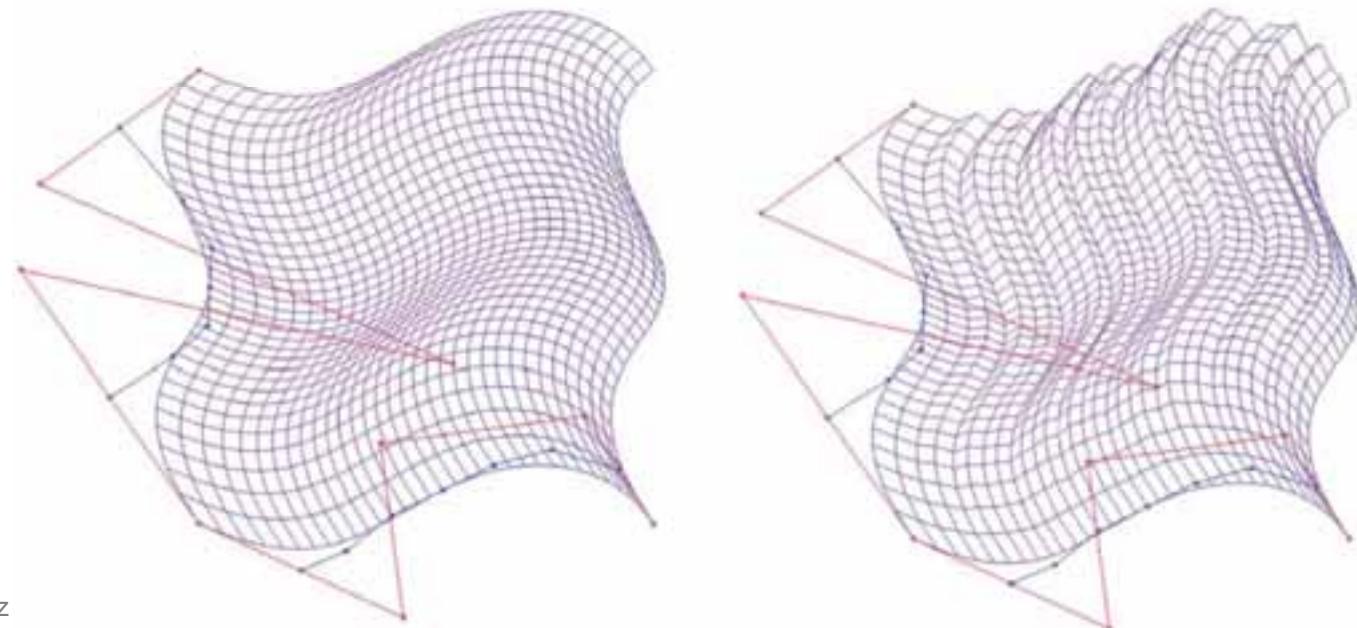
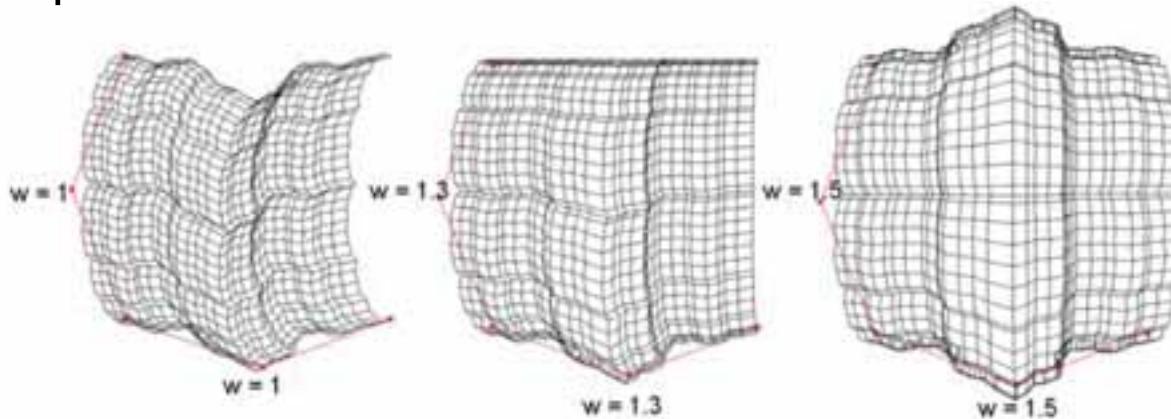


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Software Development

A new surface model



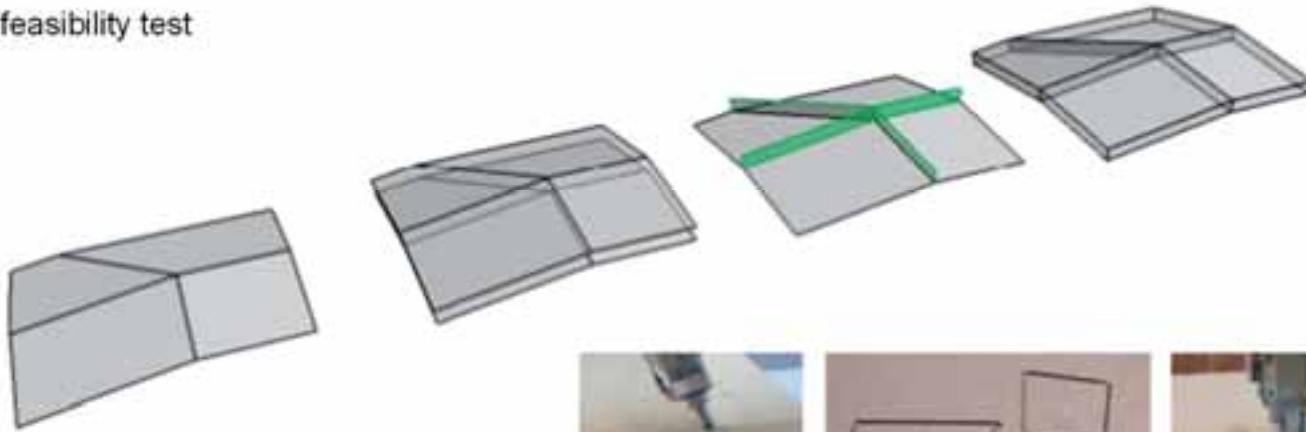
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Prototypes

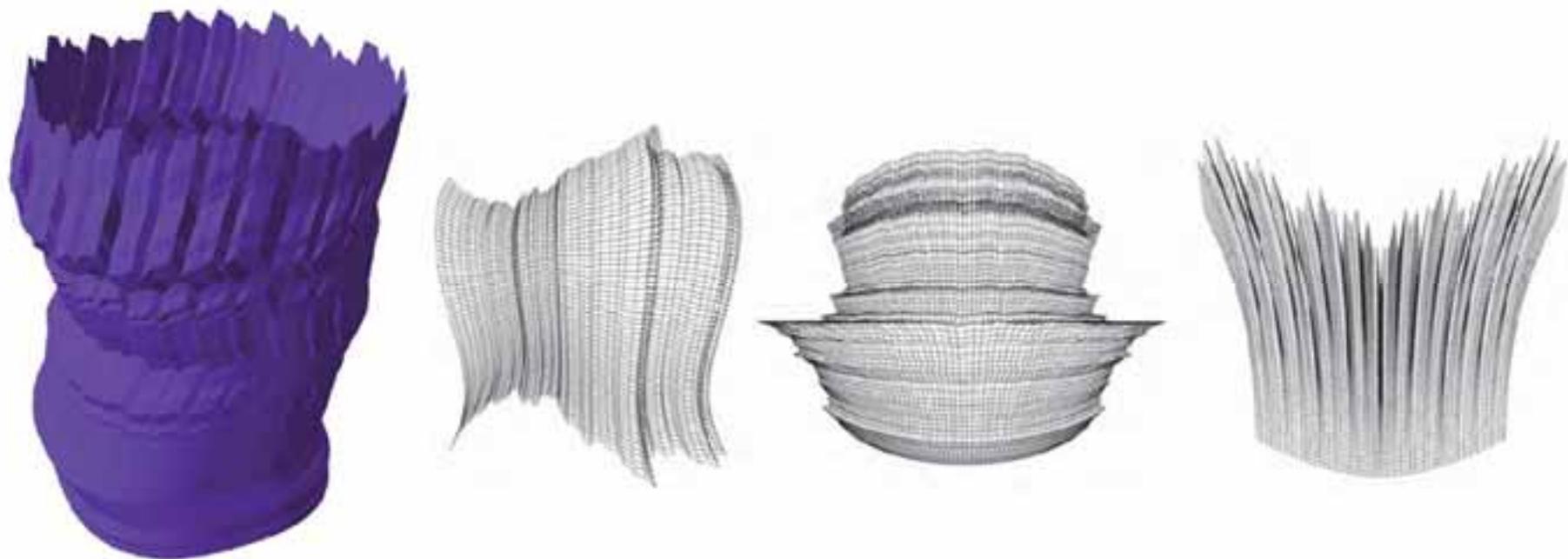
Shell structure – feasibility test



Gilles Gouaty, Ivo Stotz

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Yves Weinand

Design Possibilities



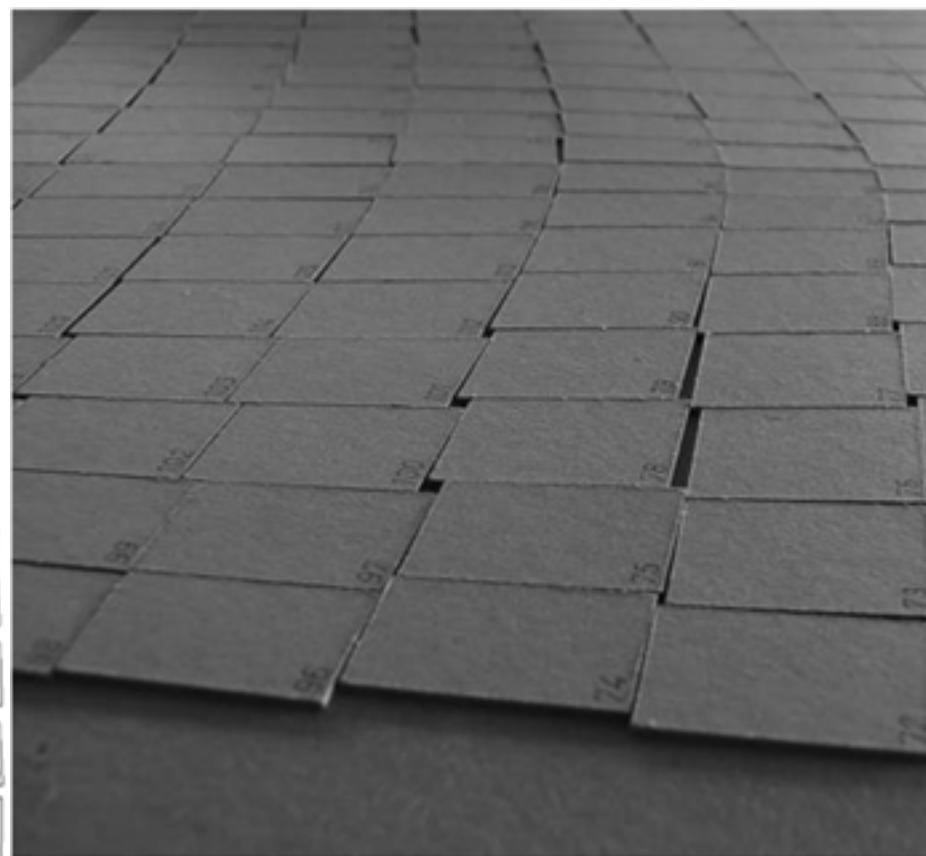
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application: B-Spline Shell

Unrolled and addressed list of construction elements

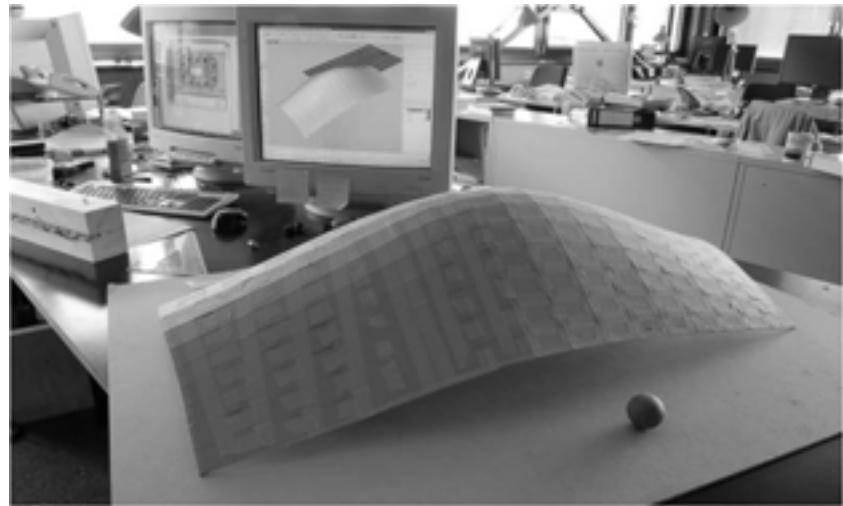
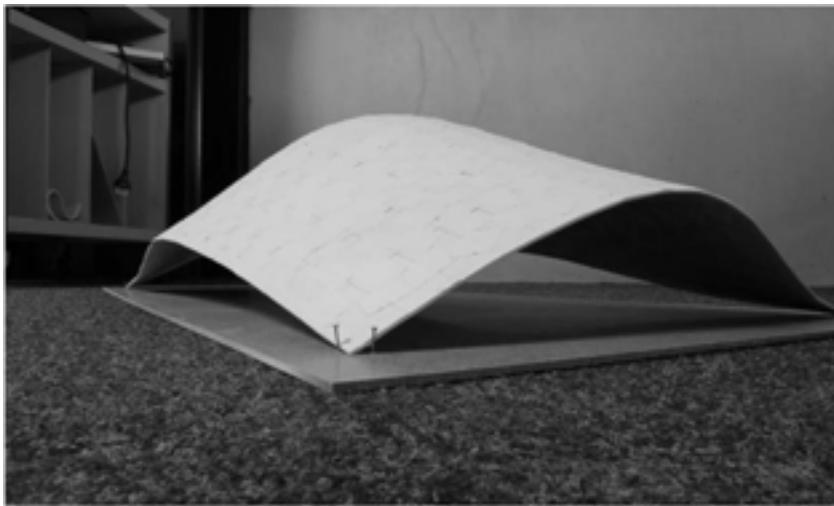
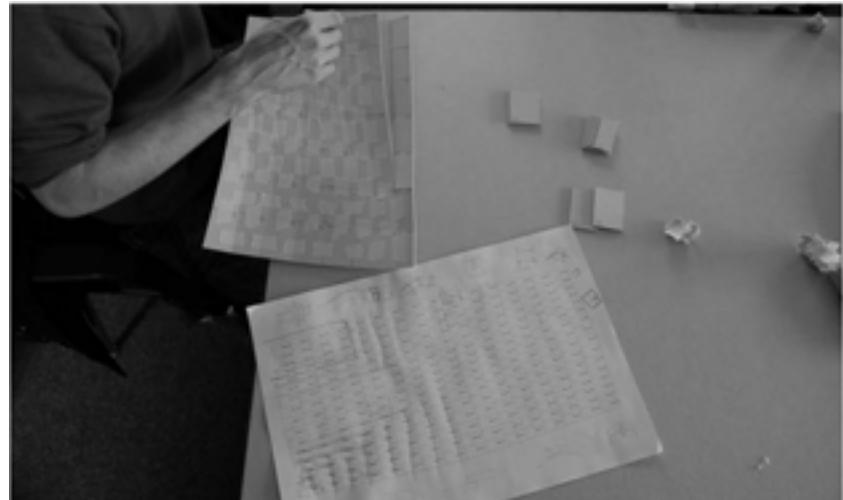
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59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40
79	78	77	76	75	74	73	72	71	70	69	68	67	66	65	64	63	62	61	60
99	98	97	96	95	94	93	92	91	90	89	88	87	86	85	84	83	82	81	80
119	118	117	116	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100
139	138	137	136	135	134	133	132	131	130	129	128	127	126	125	124	123	122	121	120
159	158	157	156	155	154	153	152	151	150	149	148	147	146	145	144	143	142	141	140
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199	198	197	196	195	194	193	192	191	190	189	188	187	186	185	184	183	182	181	180
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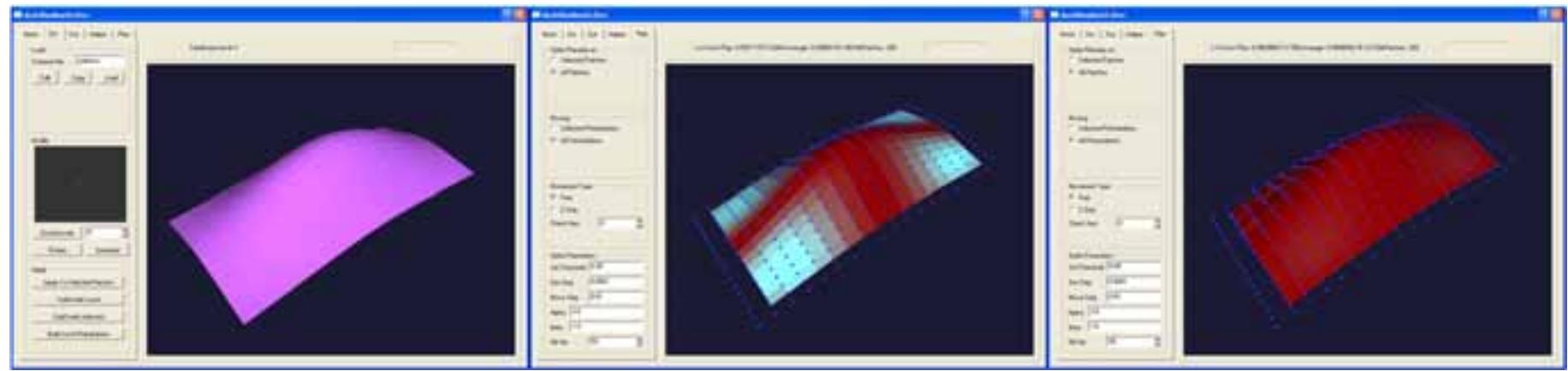
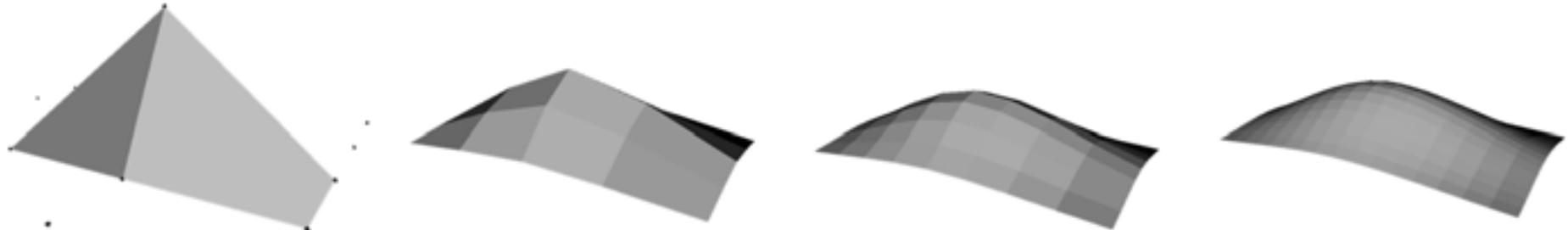
Assembly of the reduced scale model



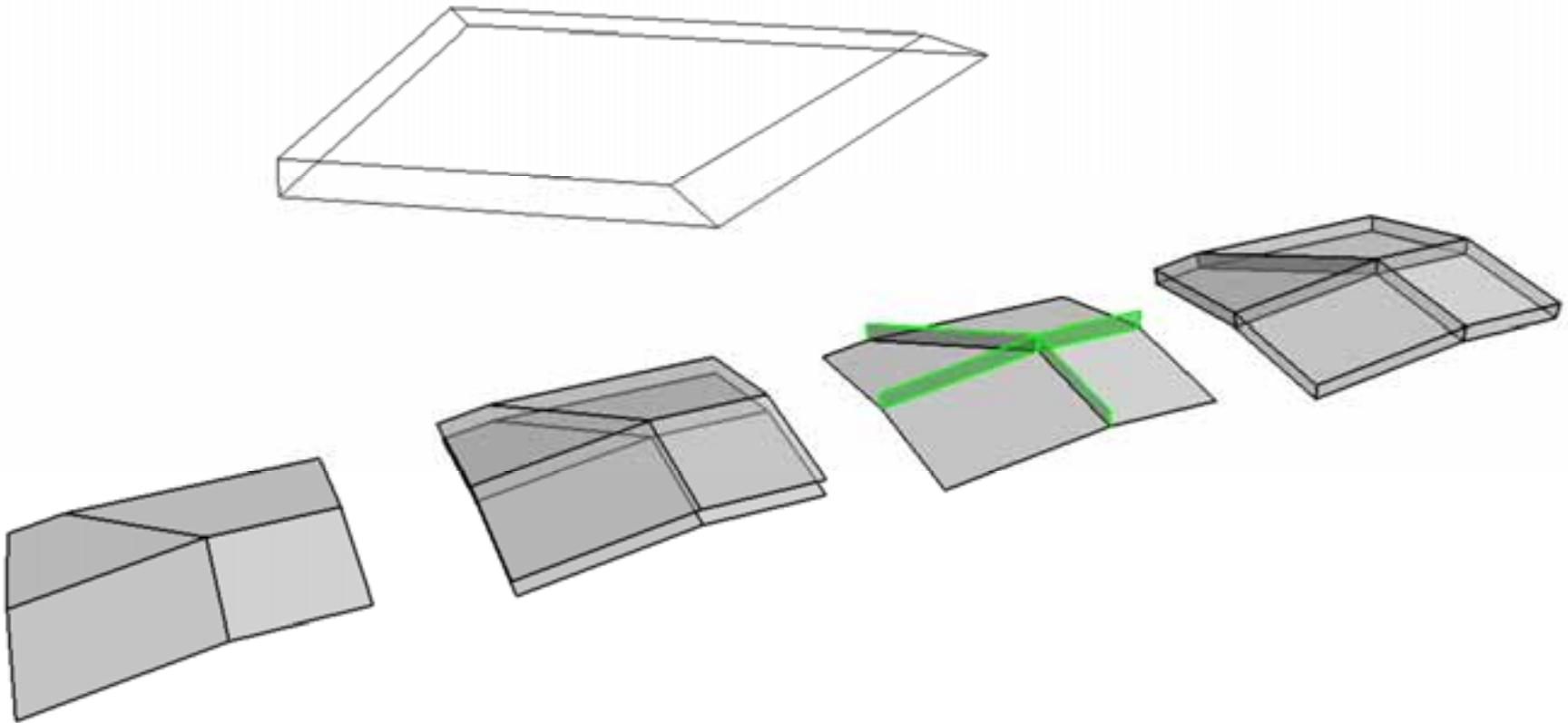
application: B-Spline Shell



application: B-Spline Shell

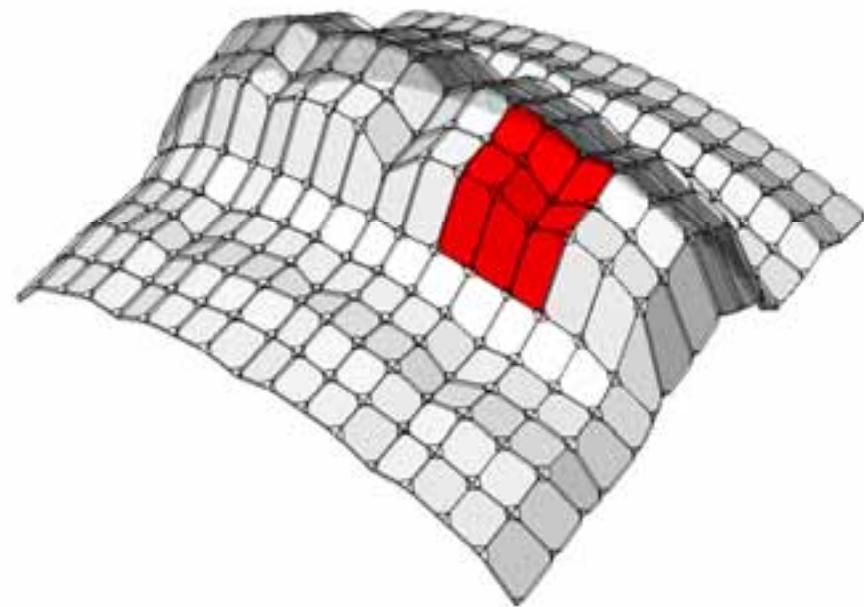
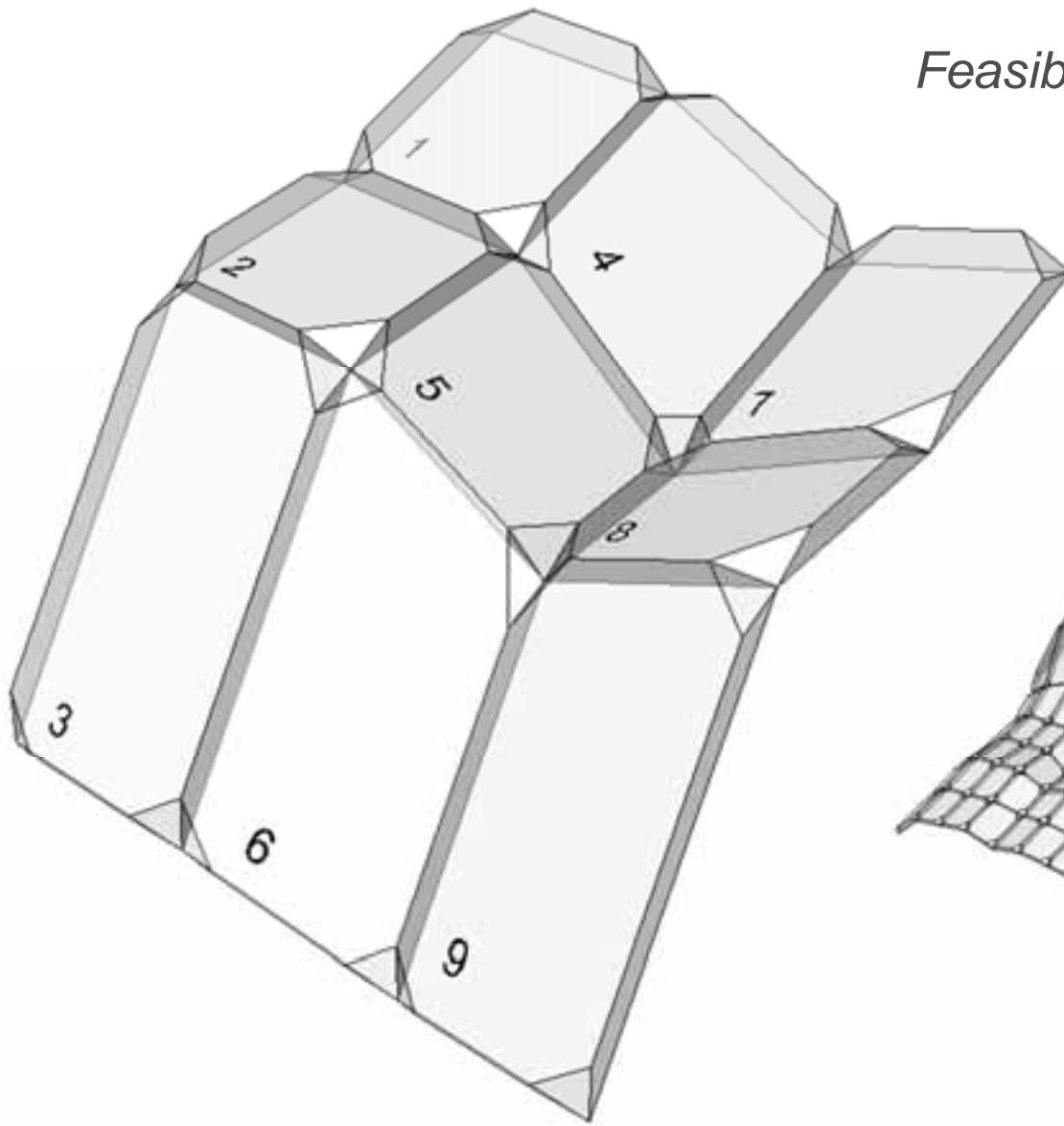


Thickening in order to obtain construction elements

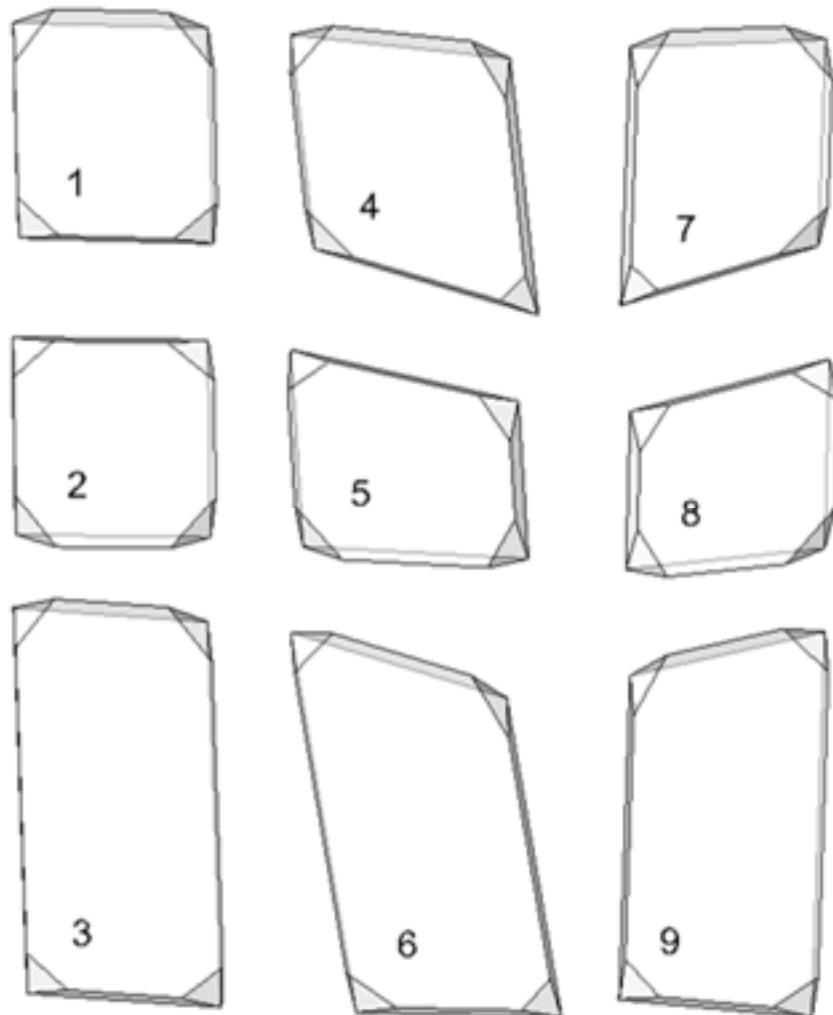


Parallel offset, bisector planes, volume elements

Feasibility study: Partial production



Feasibility study: G-code generation



ConTEXT - [C:\Documents and Settings\atetr\Bureau\Bois\frh001.mc]

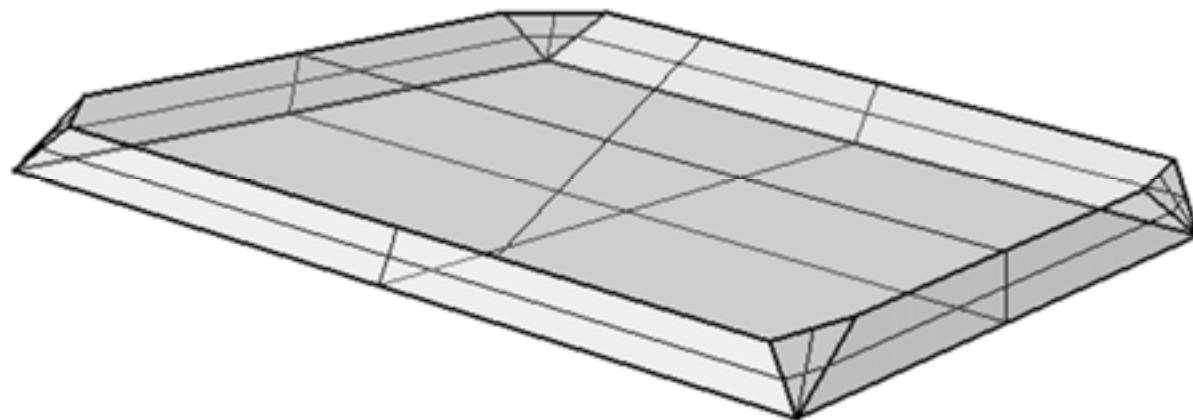
File Edit View Format Project Tools Options Window Help

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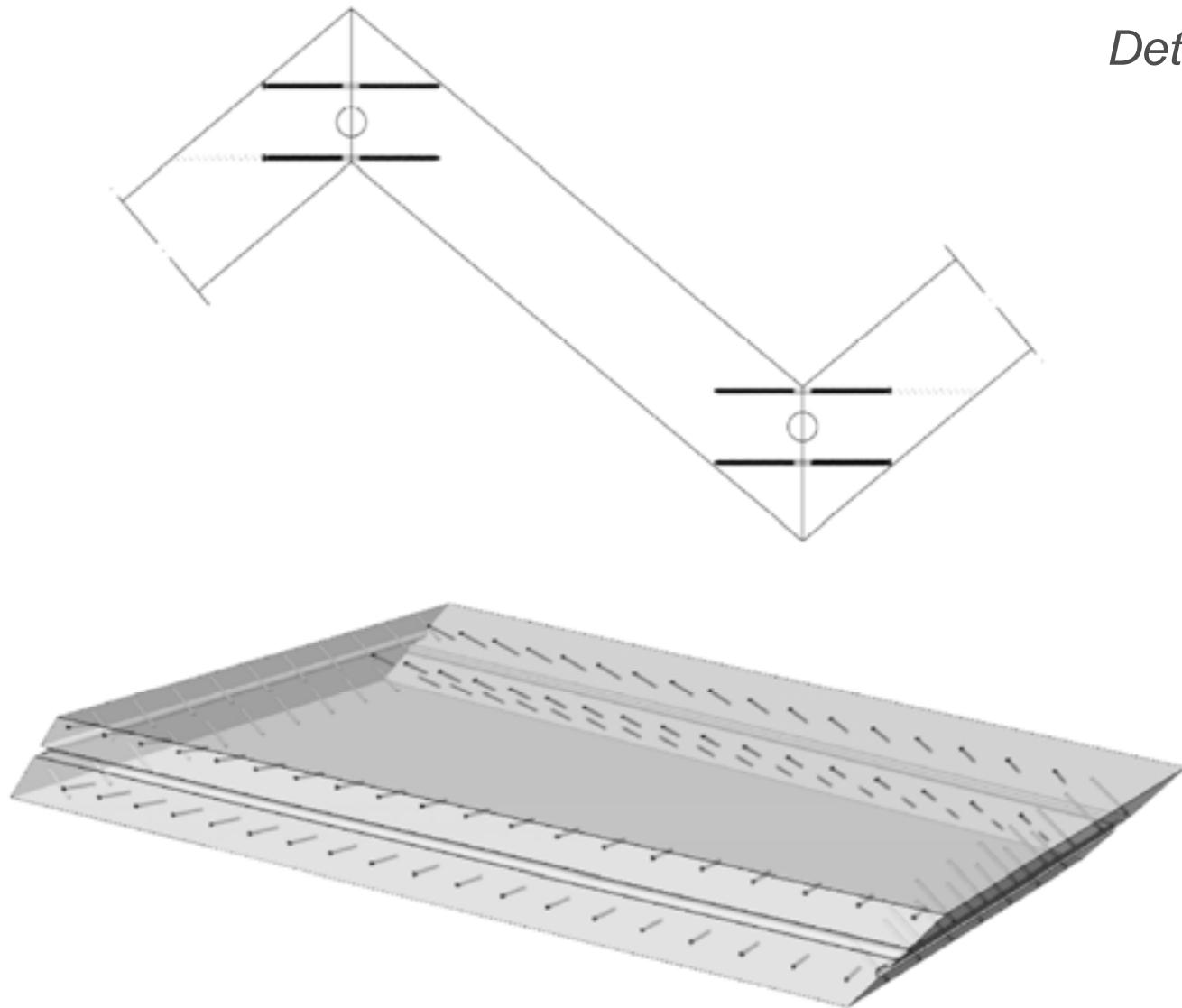
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N2 G71 T1 Z6
N3 G0 X93.0203260604704 Y62.5742002389245
N4 G1 Z-3
N5 G1 X173.8173437881376 Y32.3944638989584
N6 G1 Z6
N7 G0 X108.361877416148 Y60.3013778158484
N8 G1 Z-3
N9 G1 X107.858915143915 Y30.1236414758803
N10 G1 Z6
N11 G0 X94.8557138994148 Y62.005994633157
N12 G1 Z-3
N13 G1 X94.352751627002 Y31.8282582931889
N14 G1 Z6
N15 G0 X104.526489577304 Y60.8495834216179
N16 G1 Z-3
N17 G1 X104.023527304971 Y30.6918470316498
N18 G1 Z6
N19 G0 X100.691101738359 Y61.4277890273875
N20 G1 Z-3
N21 G1 X100.188139464026 Y31.2400526874193
N22 G1 Z6
N23 G0 X154.38653148358 Y53.482910546614
N24 G1 Z-3
N25 G1 X153.881589311248 Y33.3051742044458
N26 G1 Z6
N27 G0 X116.0312653094137 Y59.1649666043093
N28 G1 Z-3
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N30 G1 Z6
N31 G0 X119.868040933081 Y58.5967609985398
N32 G1 Z-3
N33 G1 X119.365078460748 Y28.4190246585716
N34 G1 Z6
N35 G0 X112.197265255192 Y59.7331722100789
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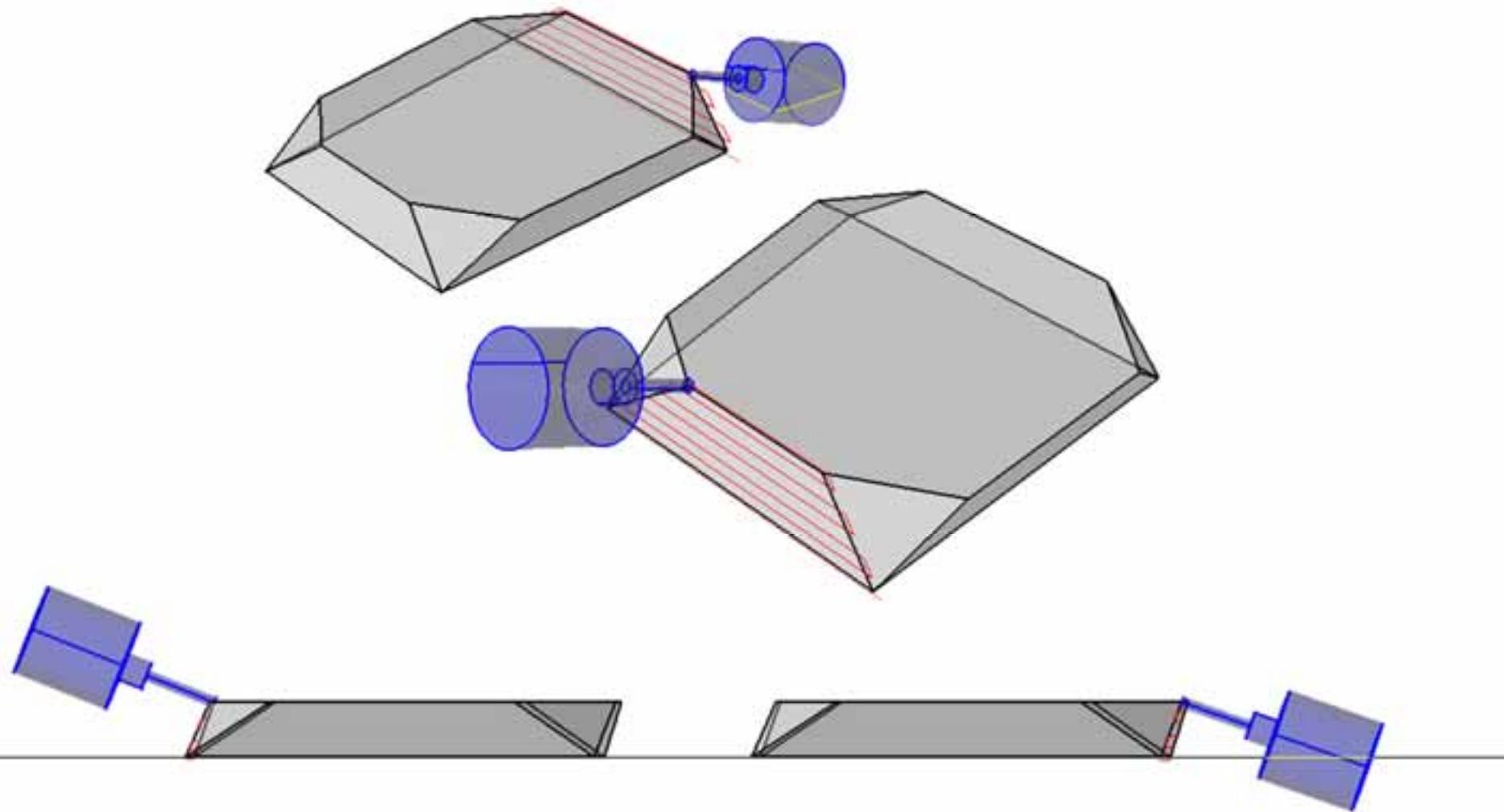
Automated detailing



Detail study



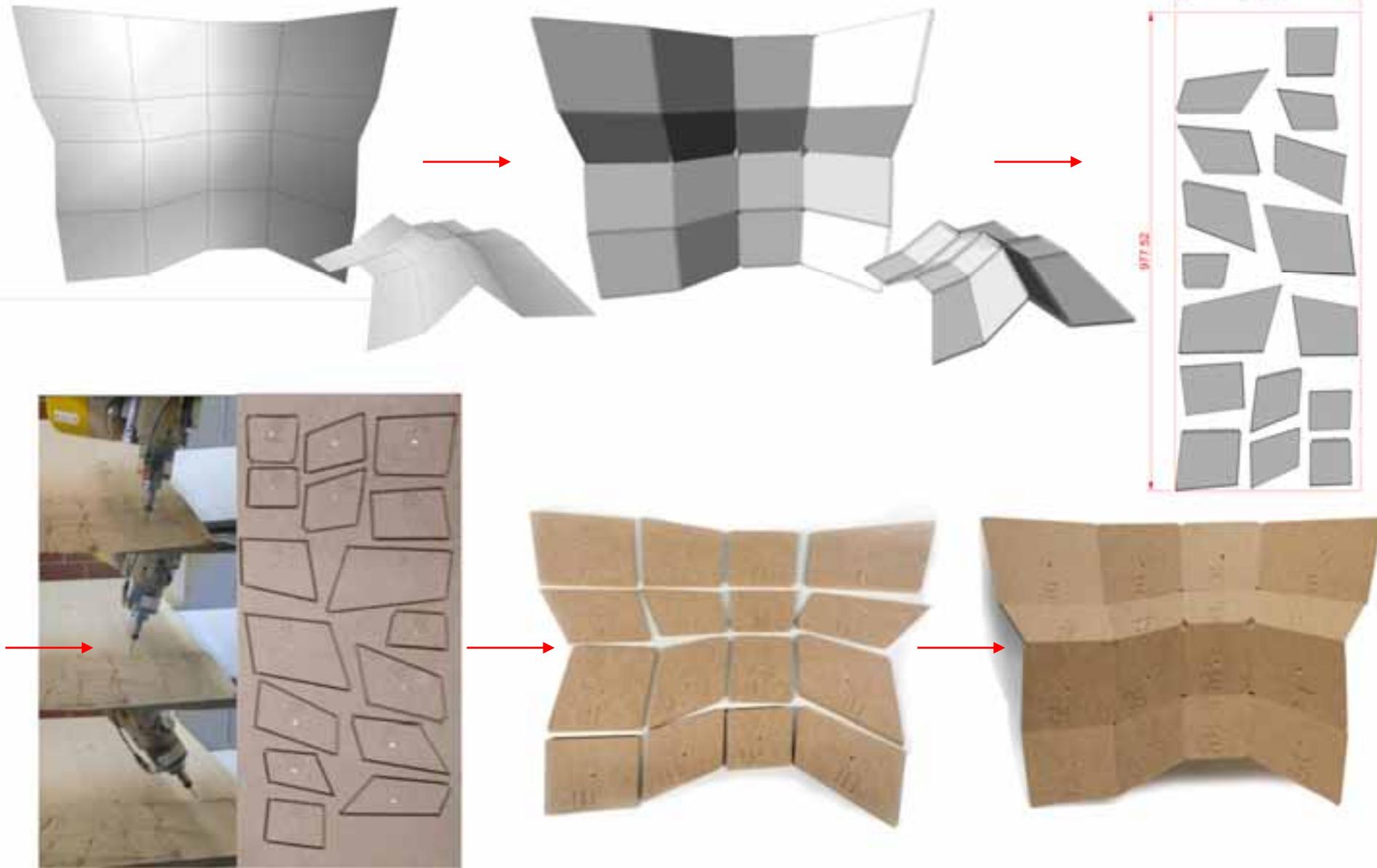
Feasibility study: G-code simulation

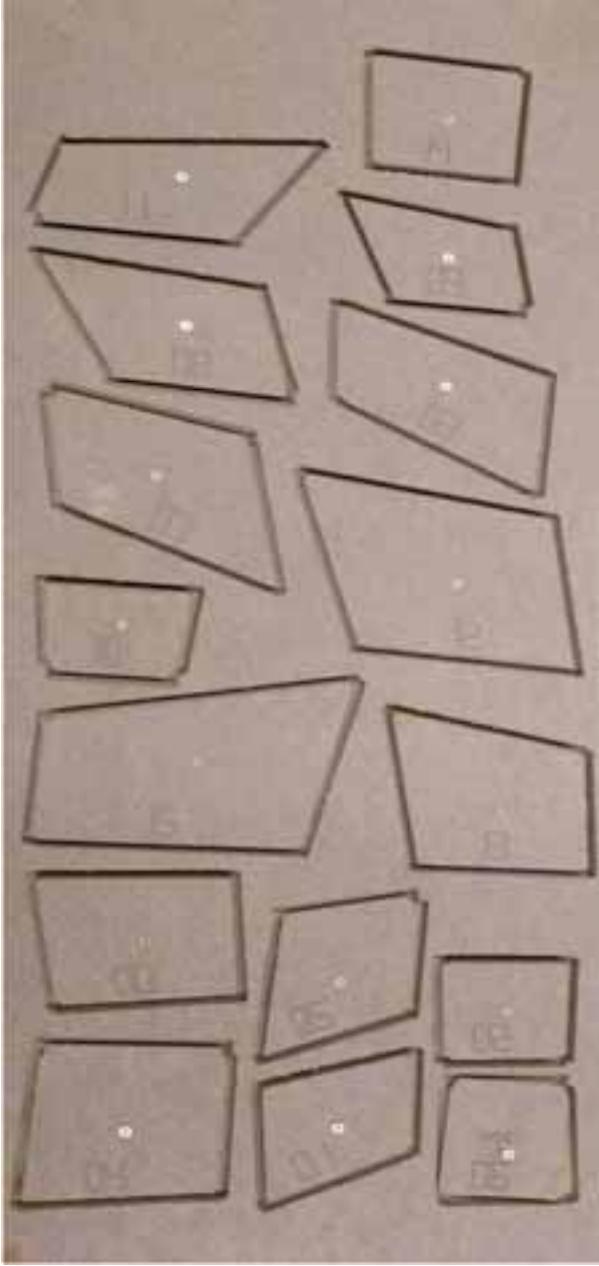




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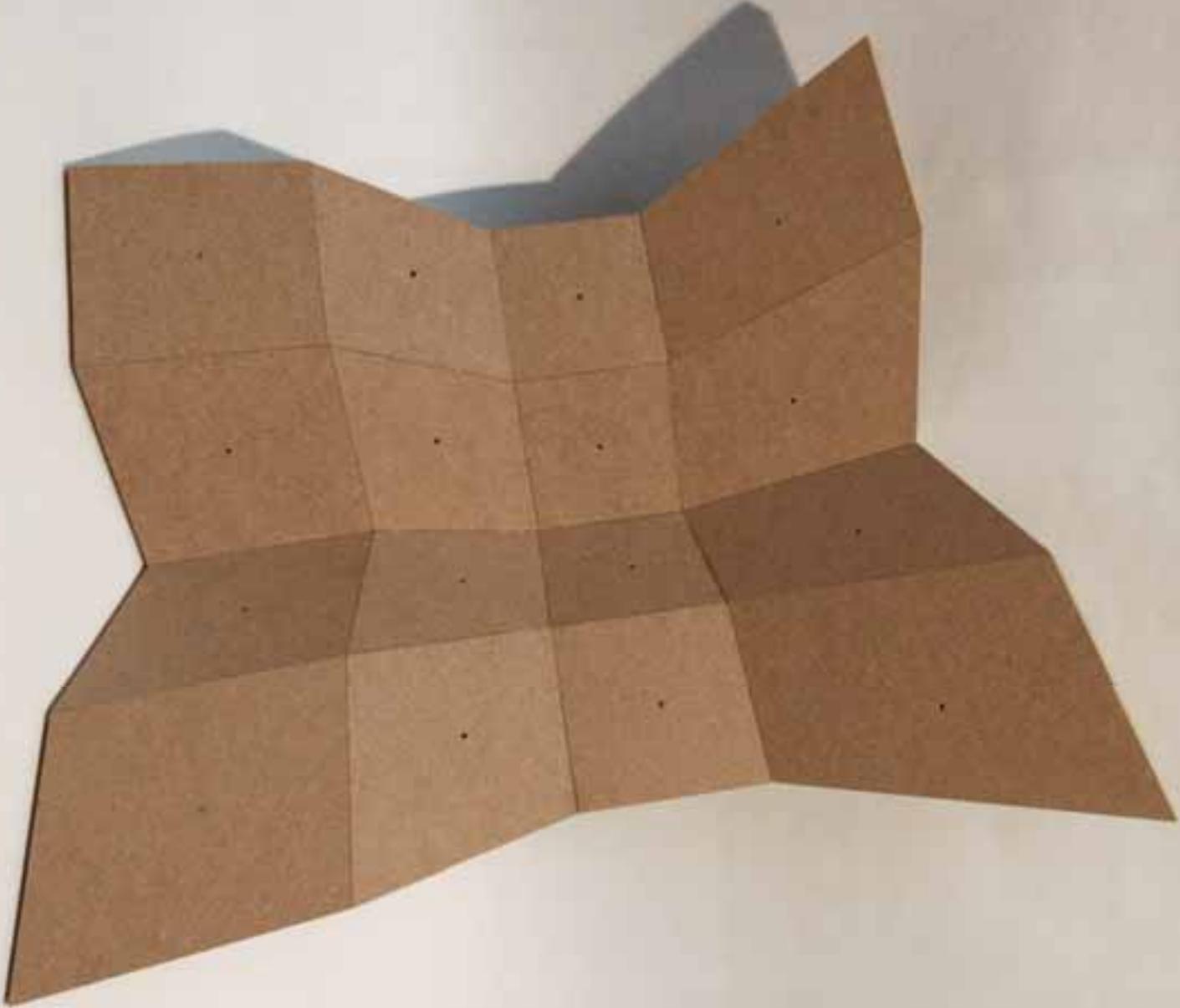
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Yves Weinand





Feasibility study: 4x4 Prototype





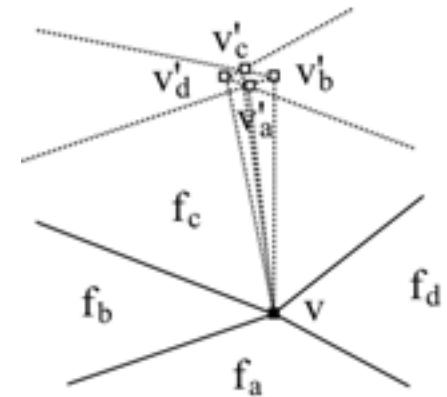
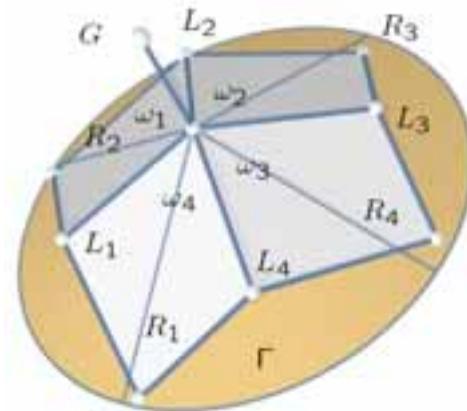
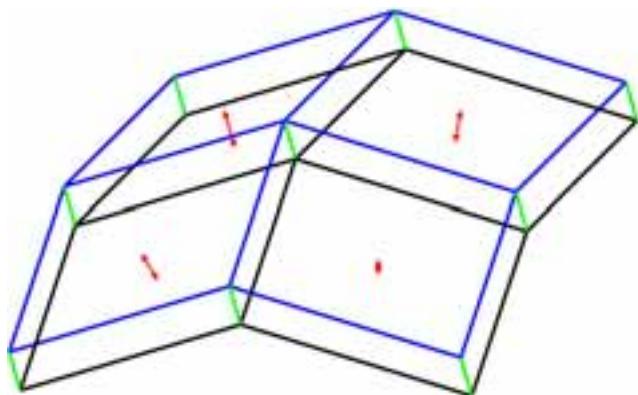
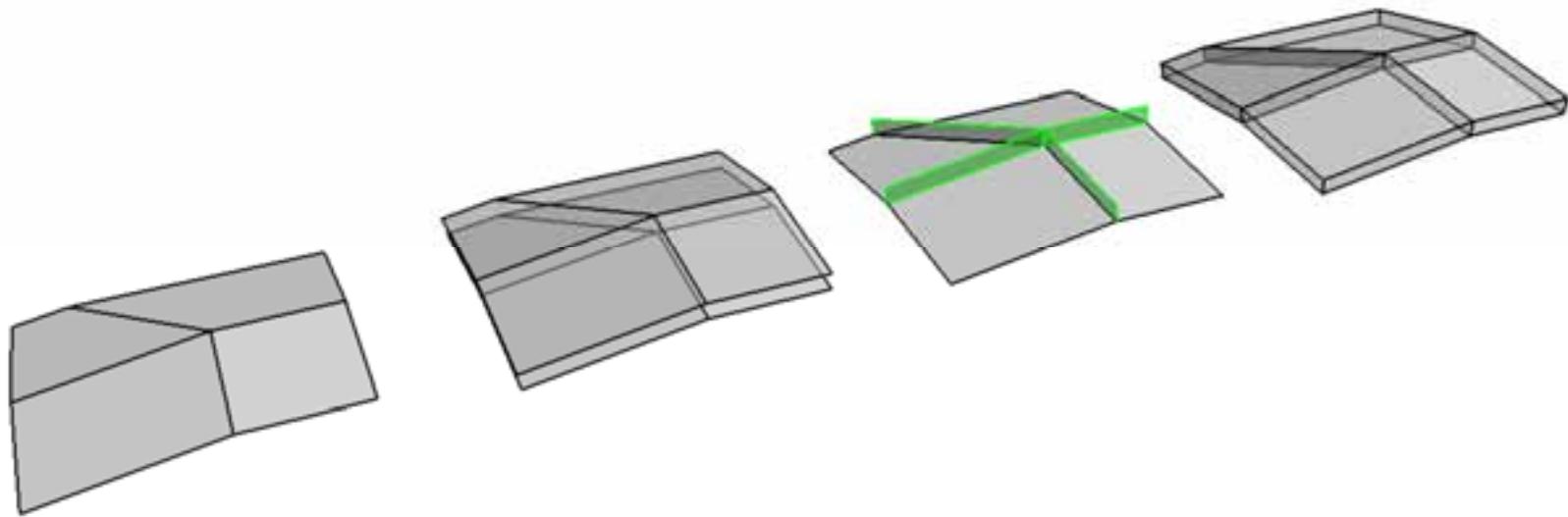
Feasibility study: 8x8 Prototype



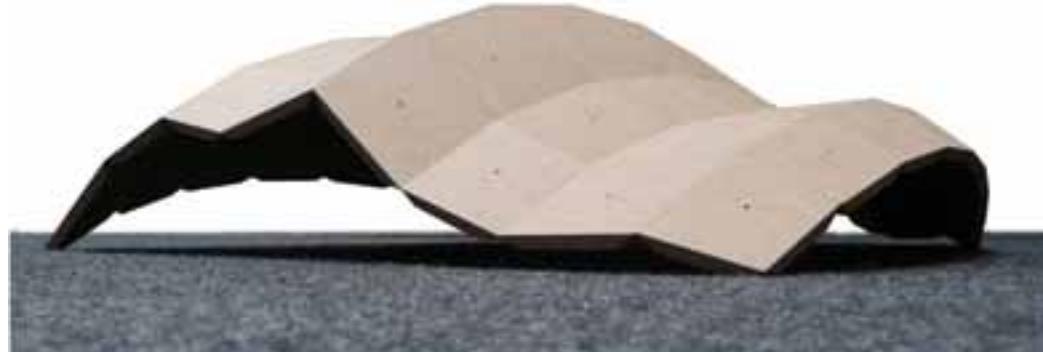
Gilles Gouaty, Ivo Stotz

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Offset

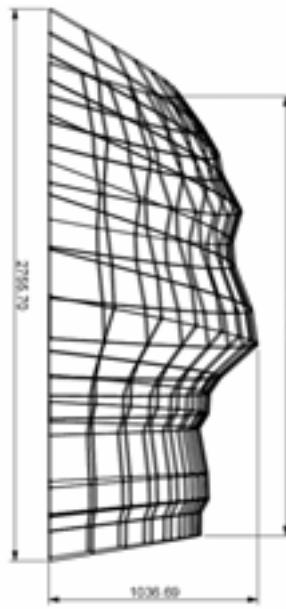
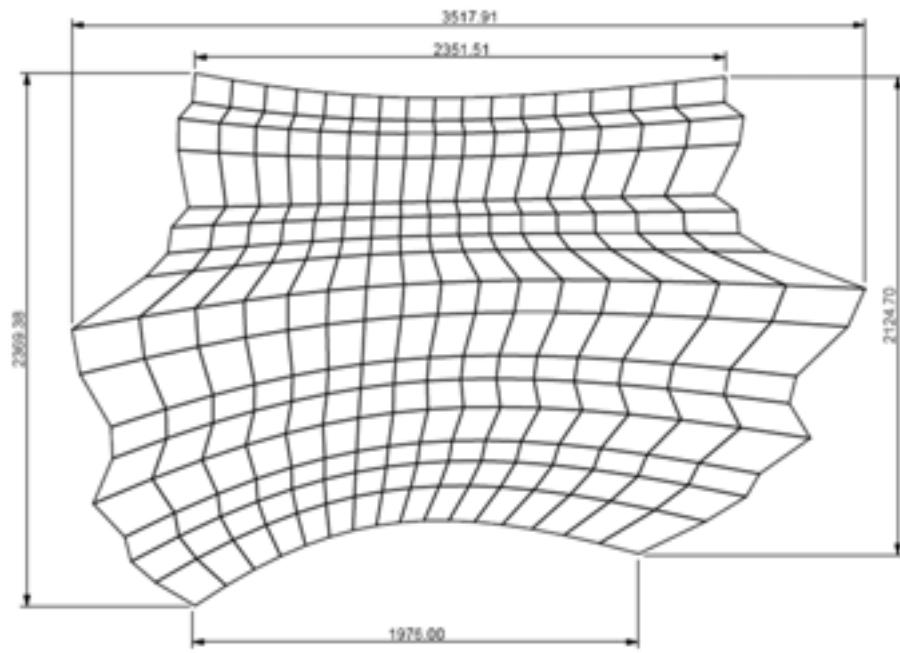
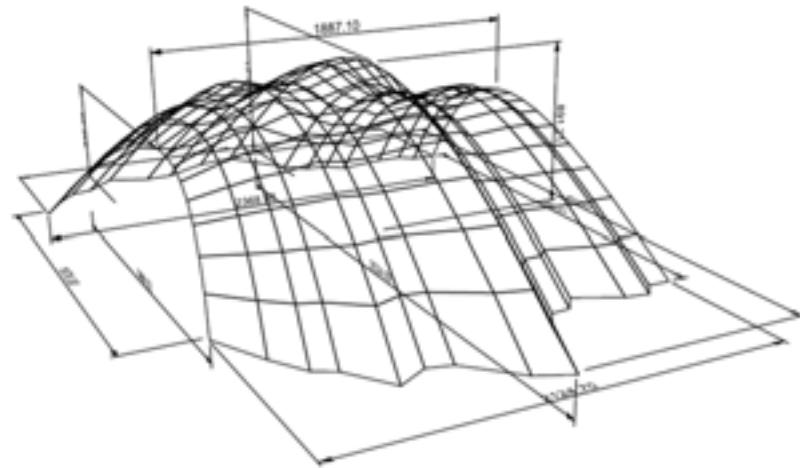
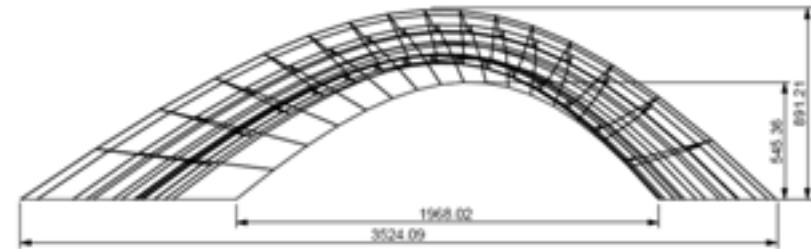


Feasibility study: 8x8 Prototype



Collaborators – Gilles Gouaty, Ivo Stotz

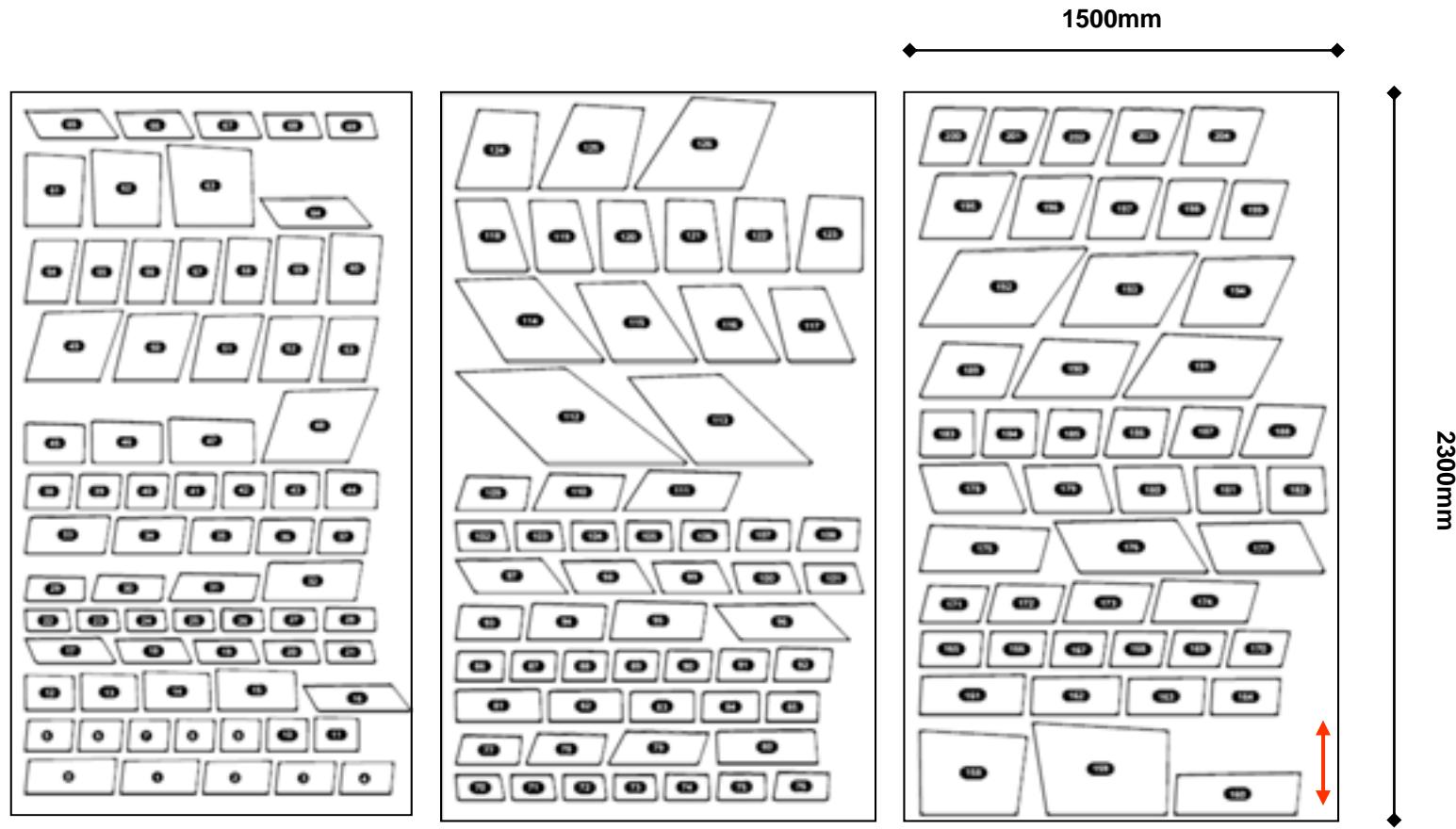
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Collaborators – Gilles Gouaty, Ivo Stotz

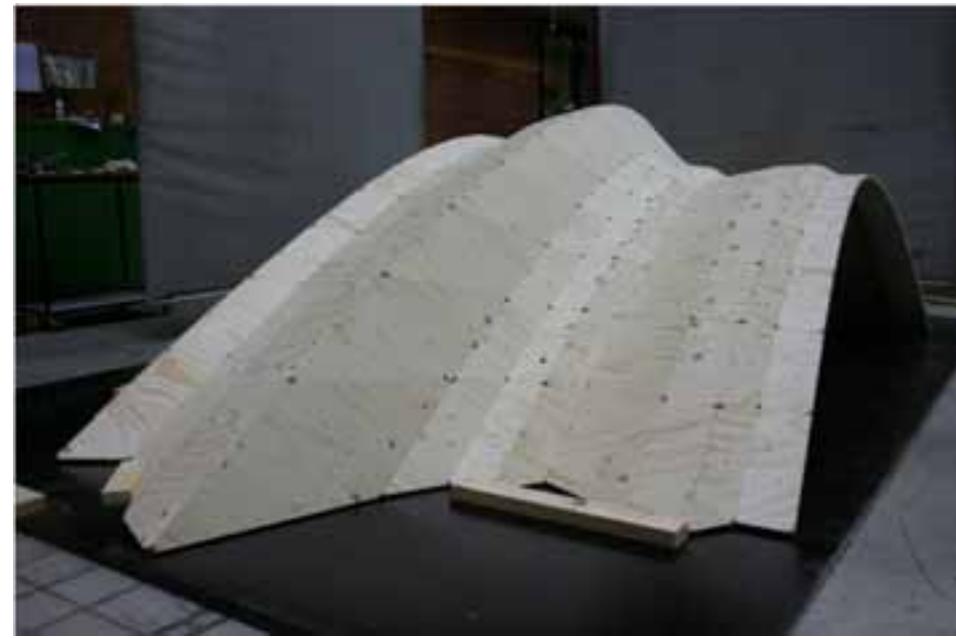
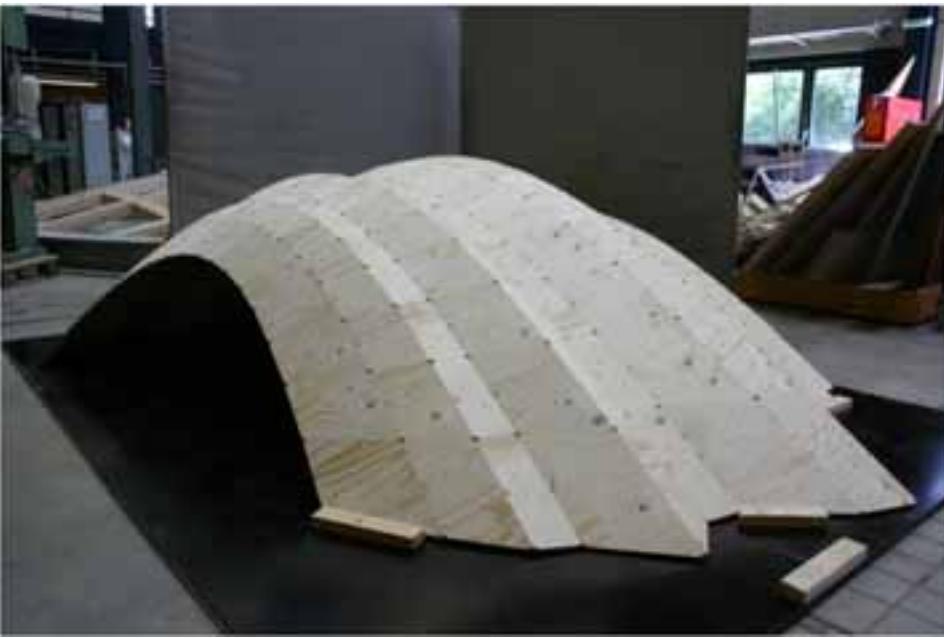
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Gilles Gouaty, Ivo Stotz

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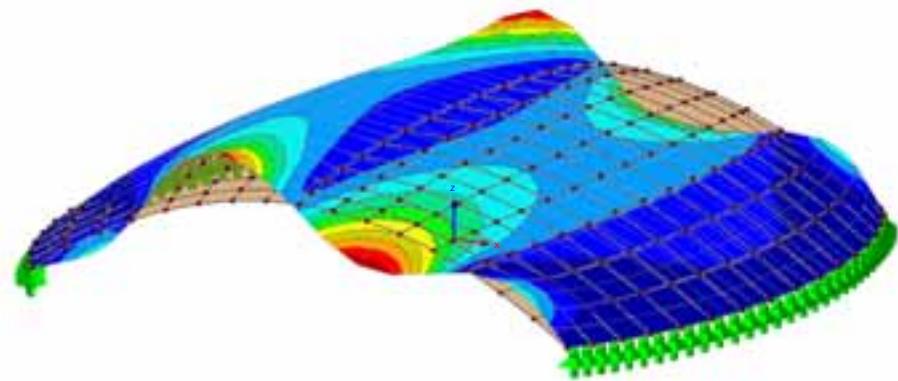
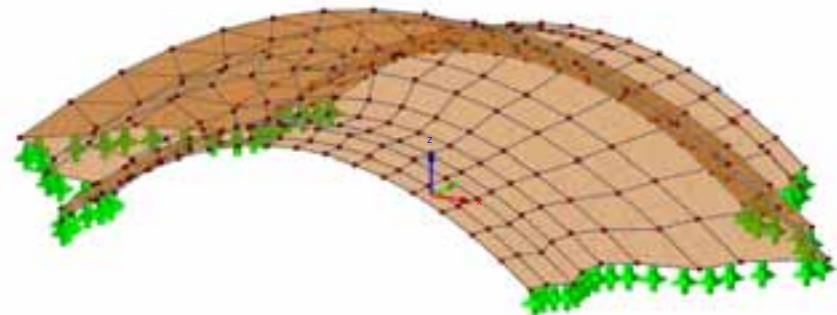
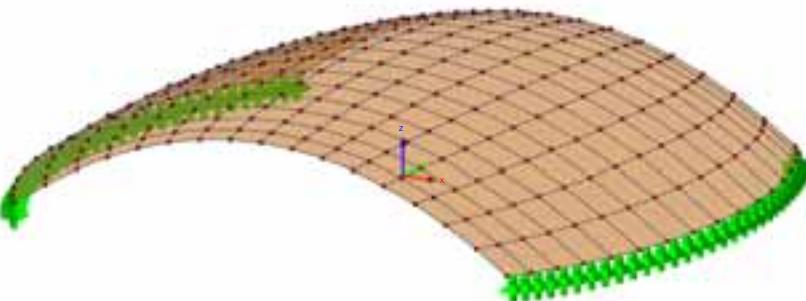


Gilles Gouaty, Ivo Stotz

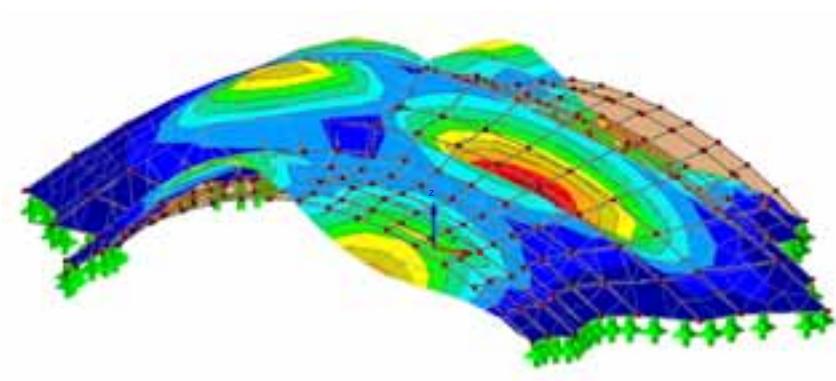
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Yves Weinand

iBOIS 
ÉCOLE POLYTECHNIQUE
FÉDÉRALE DE LAUSANNE

Exemple d'une coque mince (20mm) de 12m de portée sous un cas de charge asymétrique (neige) :



dZmax = 220mm



dZmax = 45mm

Gilles Gouaty, Ivo Stotz

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Yves Weinand

Origami, architecture Goal

Folded plate structures with cross laminated timber panels



Hani Buri

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Yves Weinand

iBOIS EPFL
ÉCOLE POLYTECHNIQUE
FÉDÉRALE DE LAUSANNE

Geodesic rib shells



Johannes Natterer

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Yves Weinand

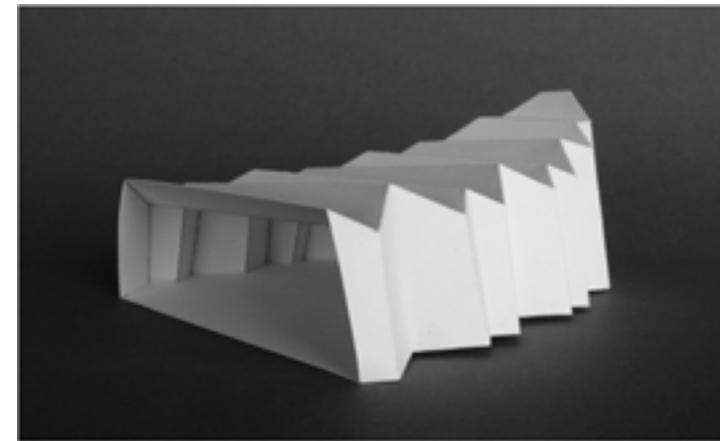
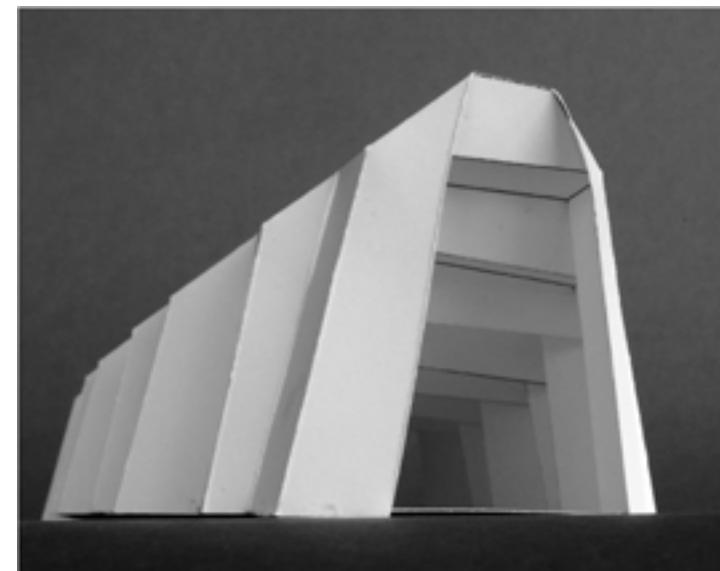
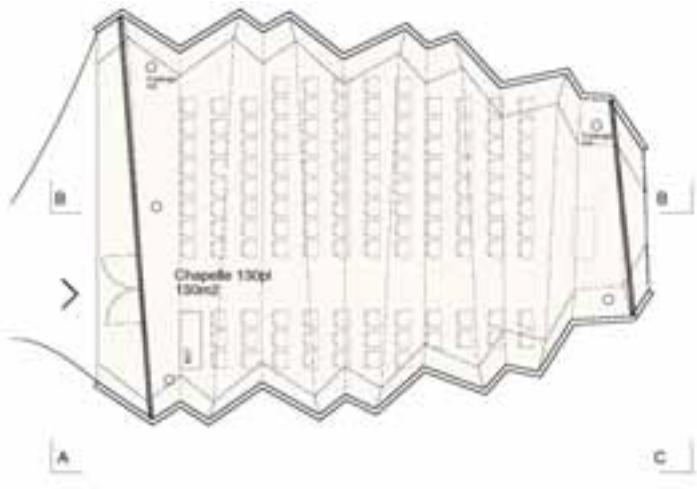
2008, Chapelle St-Loup

Maître d'ouvrage : Communauté de diaconesses de Saint Loup

Architecte: Localarchitecture / Atelier d'architecture Danilo Mondada, Shel

(Hani Buri, Yves Weinand; Architecture, engineering and production

Design)



GROUPEMENT D'ARCHITECTES

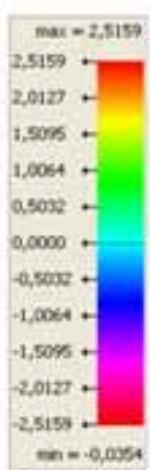
Localarchitecture, Atelier d'architecture Danilo Mondada

Innovative Timber Constructions

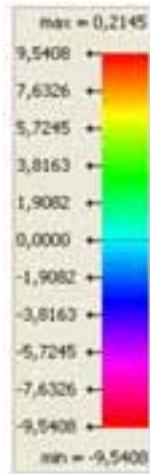
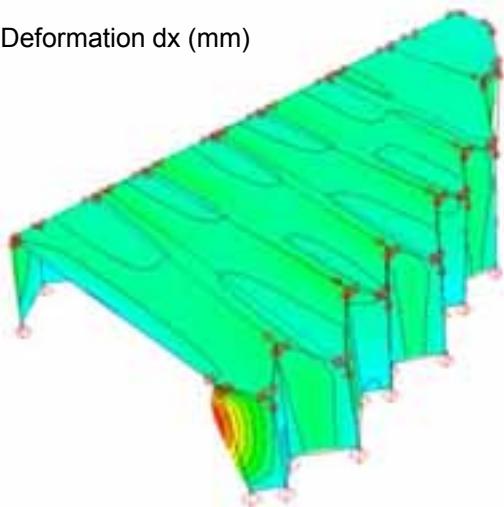
Yves Weinand

SHEL (architecture, engineering, production design

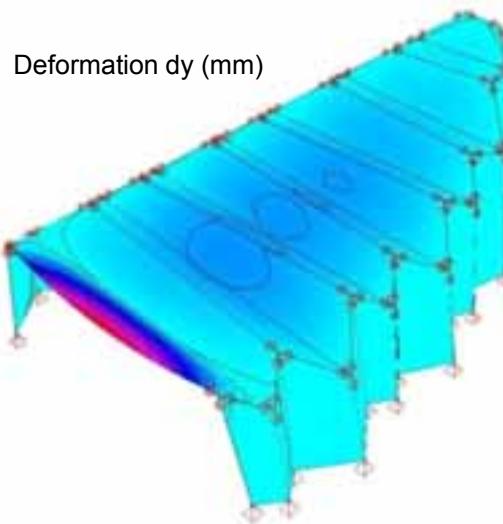
Hani Buri, Yves Weinand



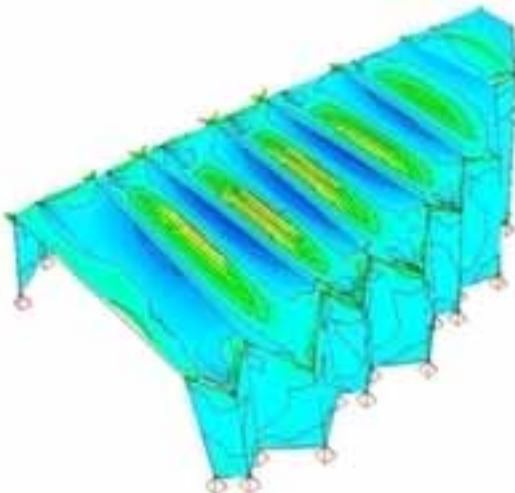
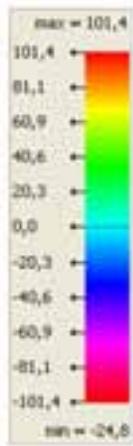
Deformation dx (mm)



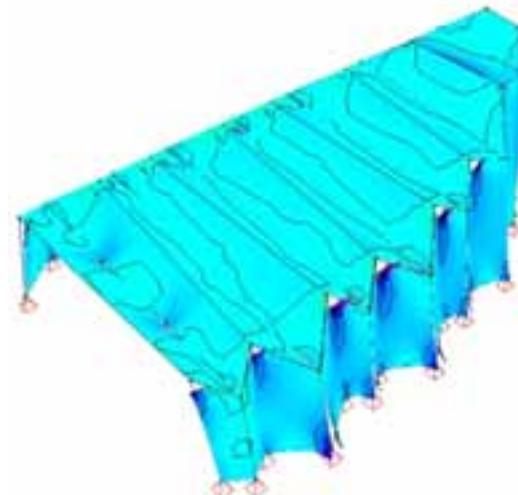
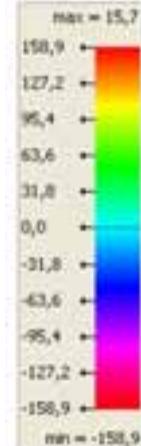
Deformation dy (mm)



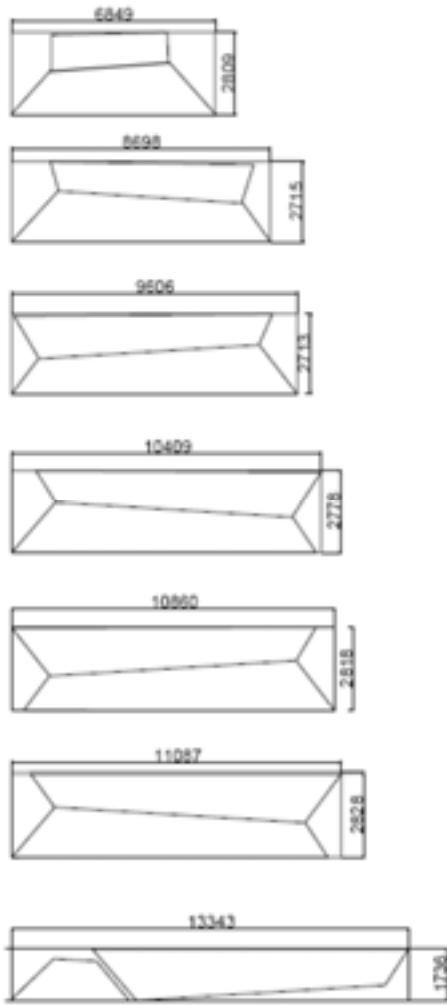
Membrane effort Nx



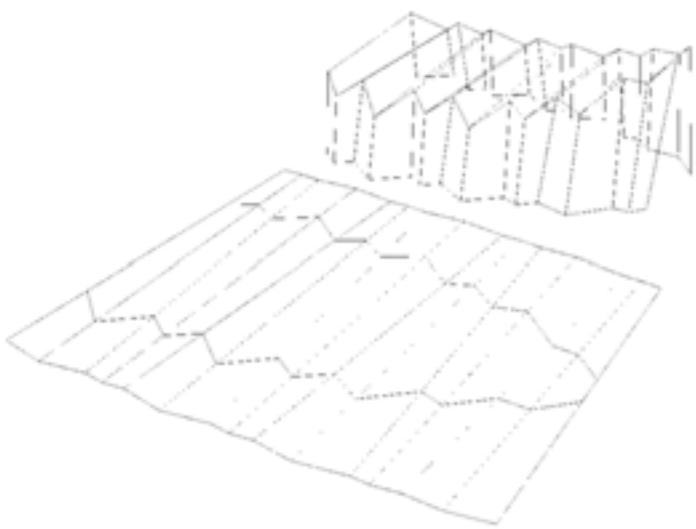
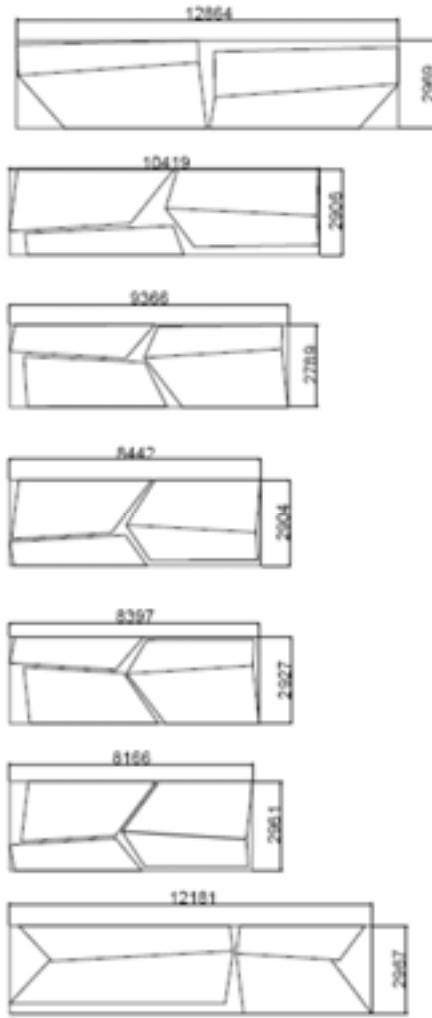
Membrane effort Nz

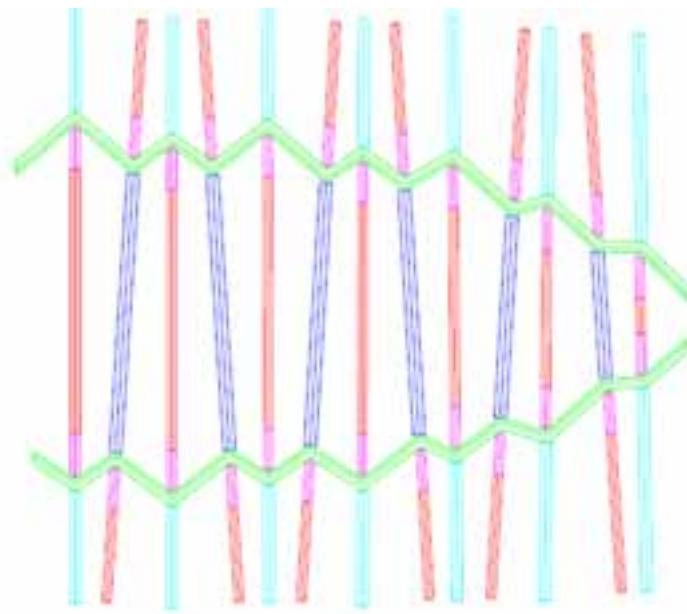
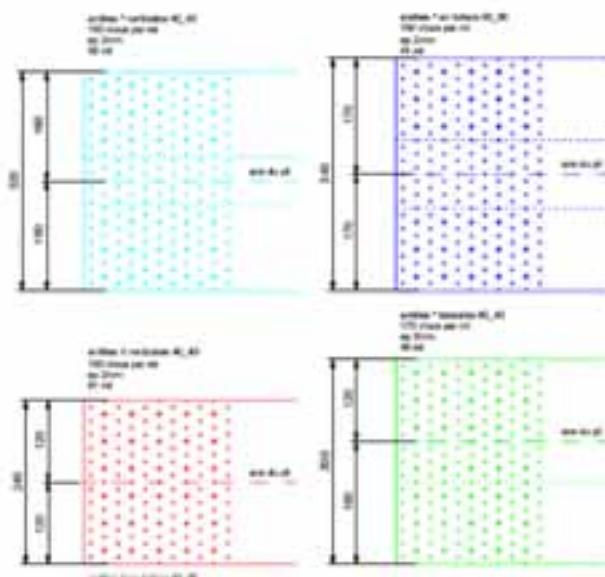


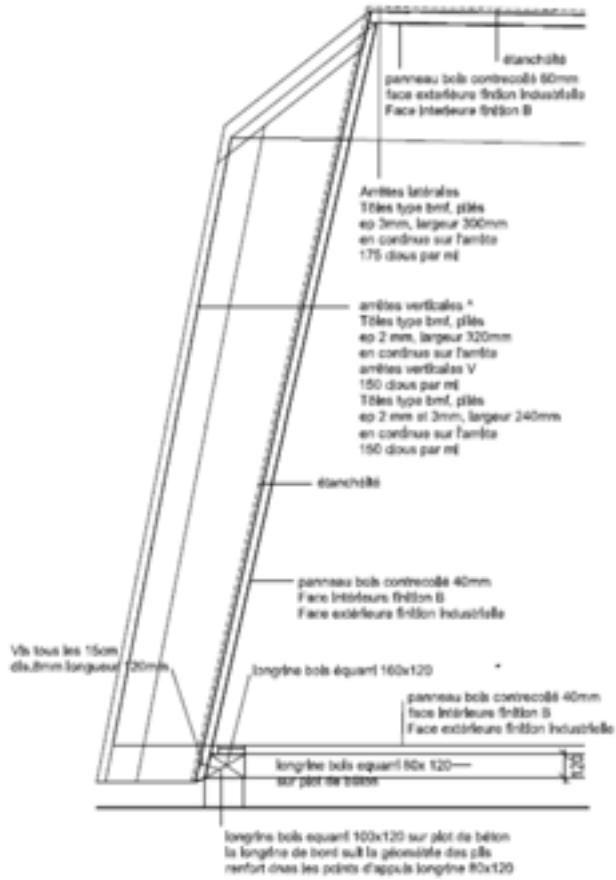
Timber block panels horizontal 60mm 151m² net



Timber block panels vertical 40mm 175m² net









Innovative Timber Constructions
Yves Weinand



Innovative Timber Constructions
Yves Weinand

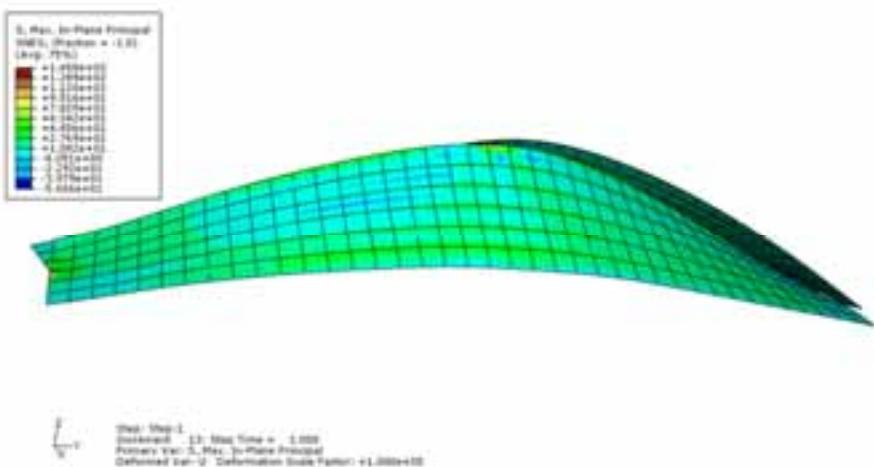
Maximum principal internal stresses for two proportion

Proportion (length/width)= 7

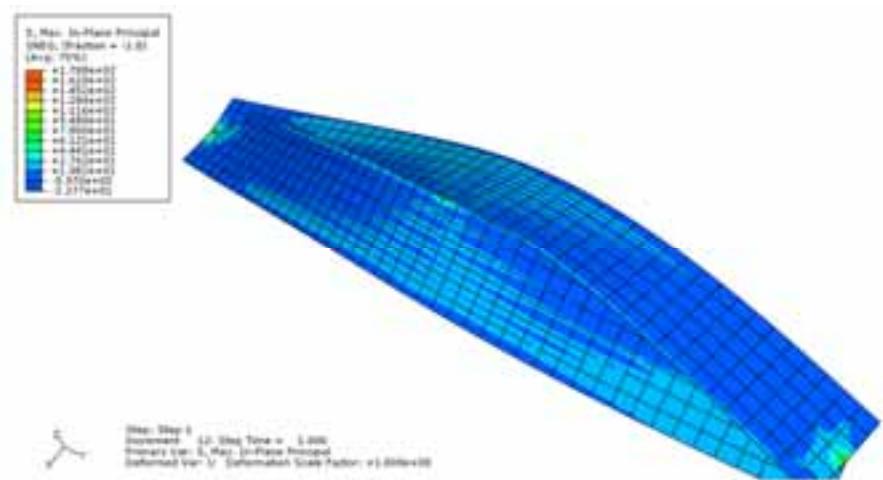
Length= 11.55 m, Width= 1.65 m

Proportion (length/width)= 8.7

Length= 11.55 m, Width= 1.32 m

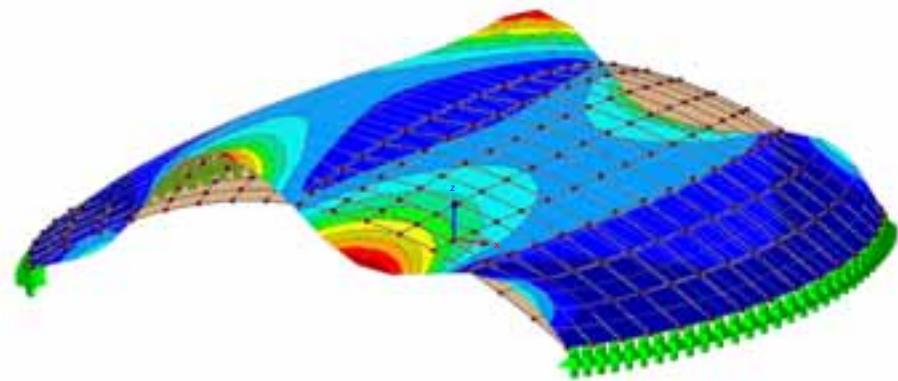
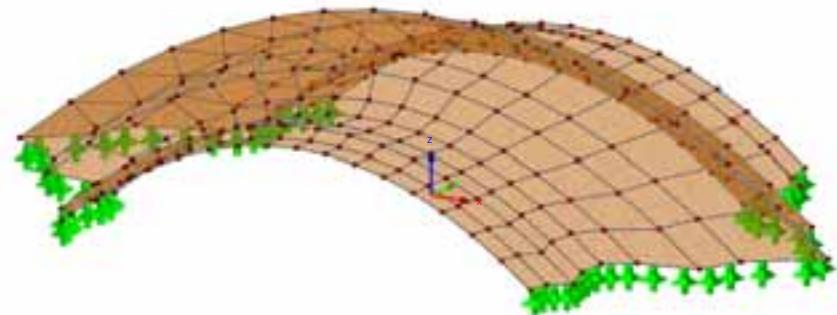
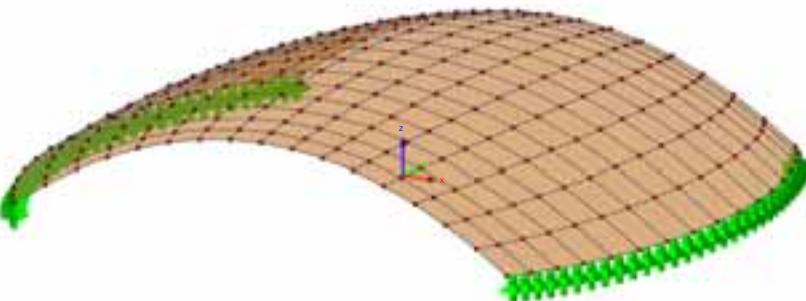


Maximum Principal stress= 46 MPa

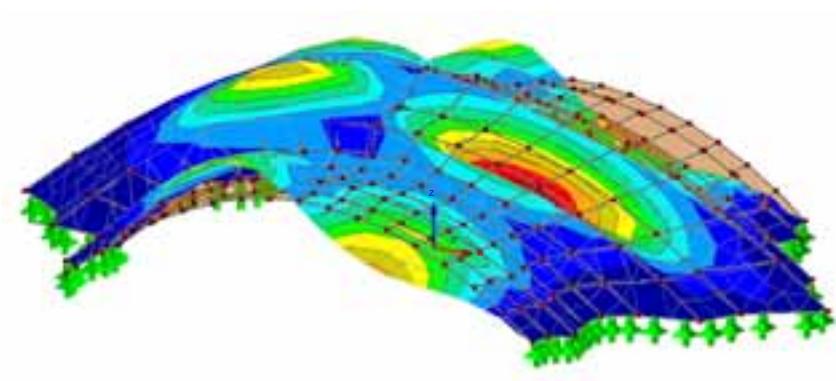


Maximum Principal stress= 29 MPa

Exemple d'une coque mince (20mm) de 12m de portée sous un cas de charge asymétrique (neige) :



dZmax = 220mm

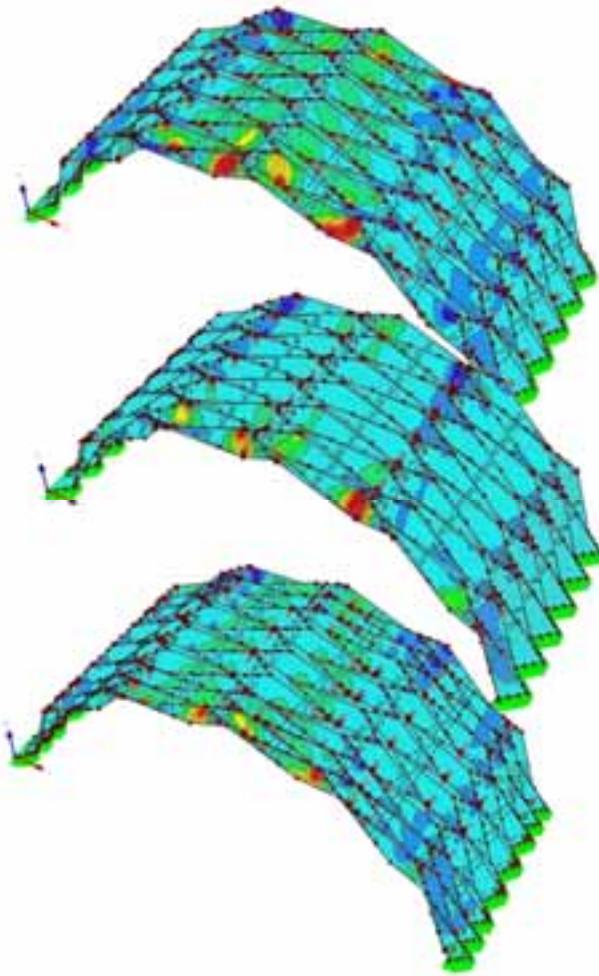


dZmax = 45mm

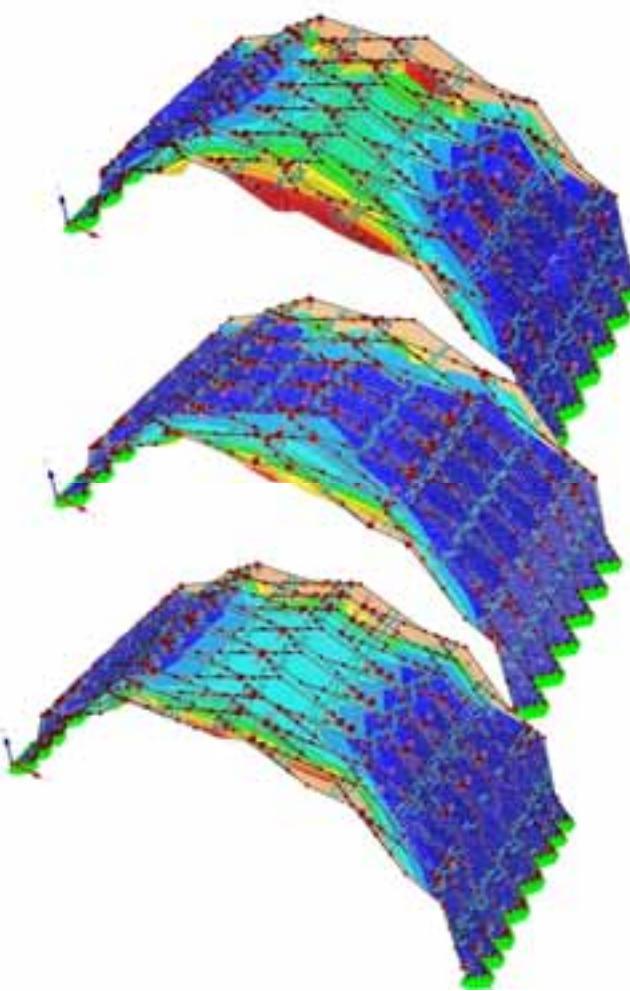
Gilles Gouaty, Ivo Stotz, Johannes Natterer

Innovative Timber Constructions
Yves Weinand

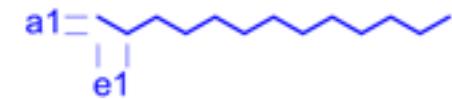
Internal forces



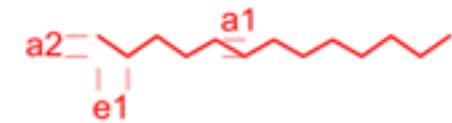
Deformations



1. Max vectorial displacement 3.3 mm



2. Max vectorial displacement 2.2 mm



3. Max vectorial displacement 1.9 mm



Hani Buri, Johannes Natterer

Innovative Timber Constructions
Yves Weinand

Atelier Weinand

Structural Fibres, Autumn 2007



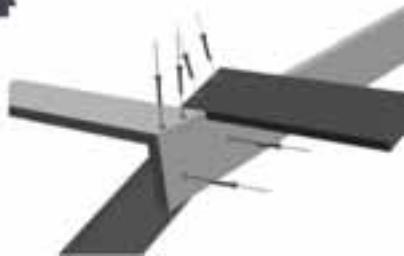
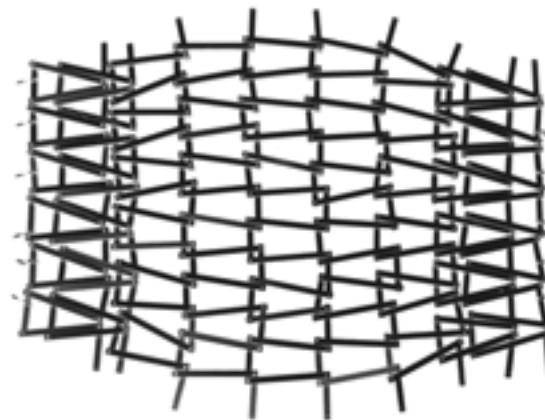
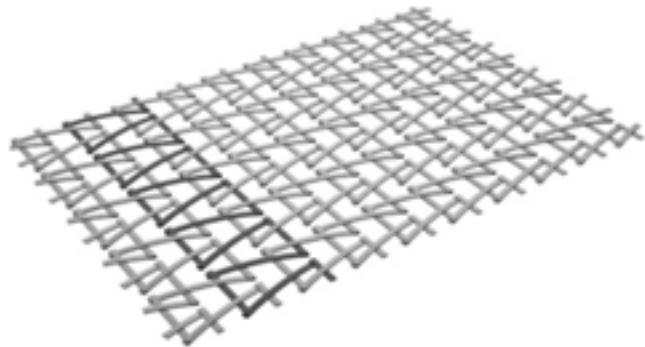
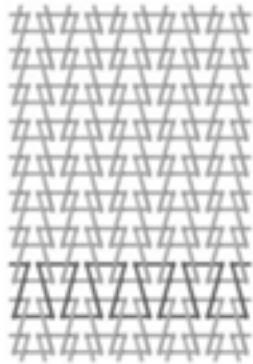
Research & Teaching

Practical implementation of knowledge



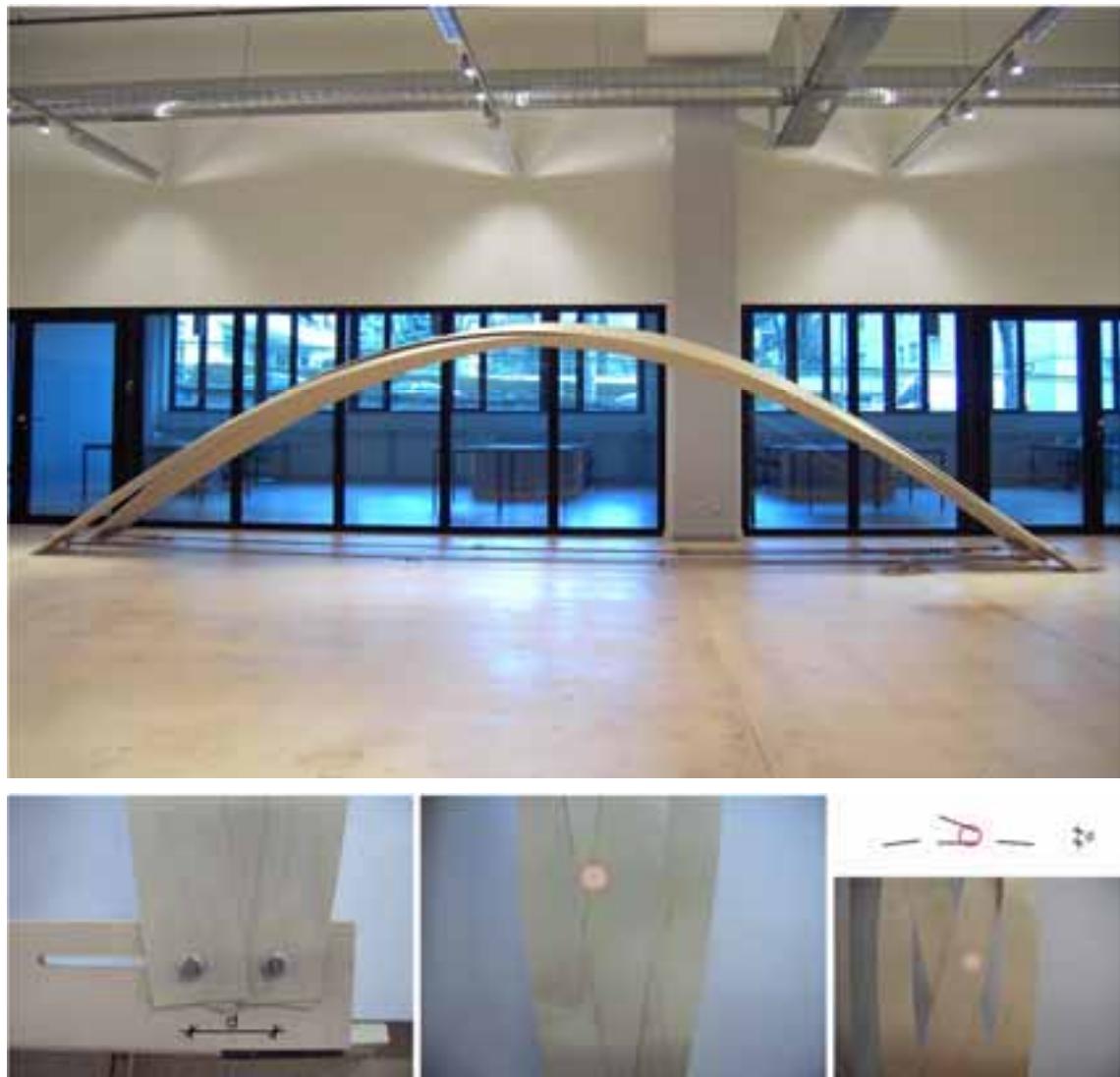
Atelier Weinand Autumn 07 Prof. Yves Weinand, Hani Buri, Markus Hudert
Students Pietro Ramondo , Jacopo Laffranchini

Innovative Timber Constructions
Yves Weinand



Atelier Weinand Spring 08 Prof. Yves Weinand, Hani Buri, Markus Hudert
Student Thomas Austerveil

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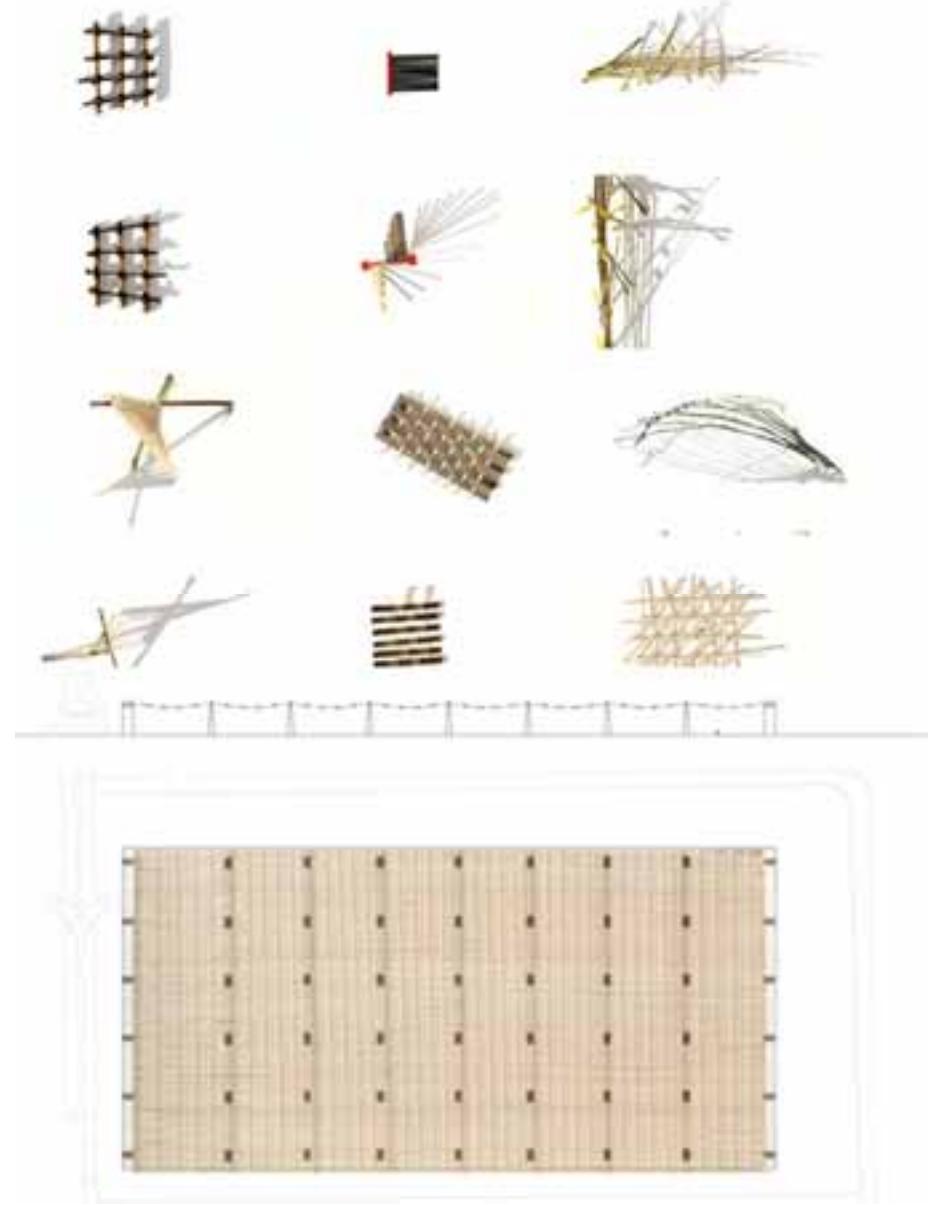
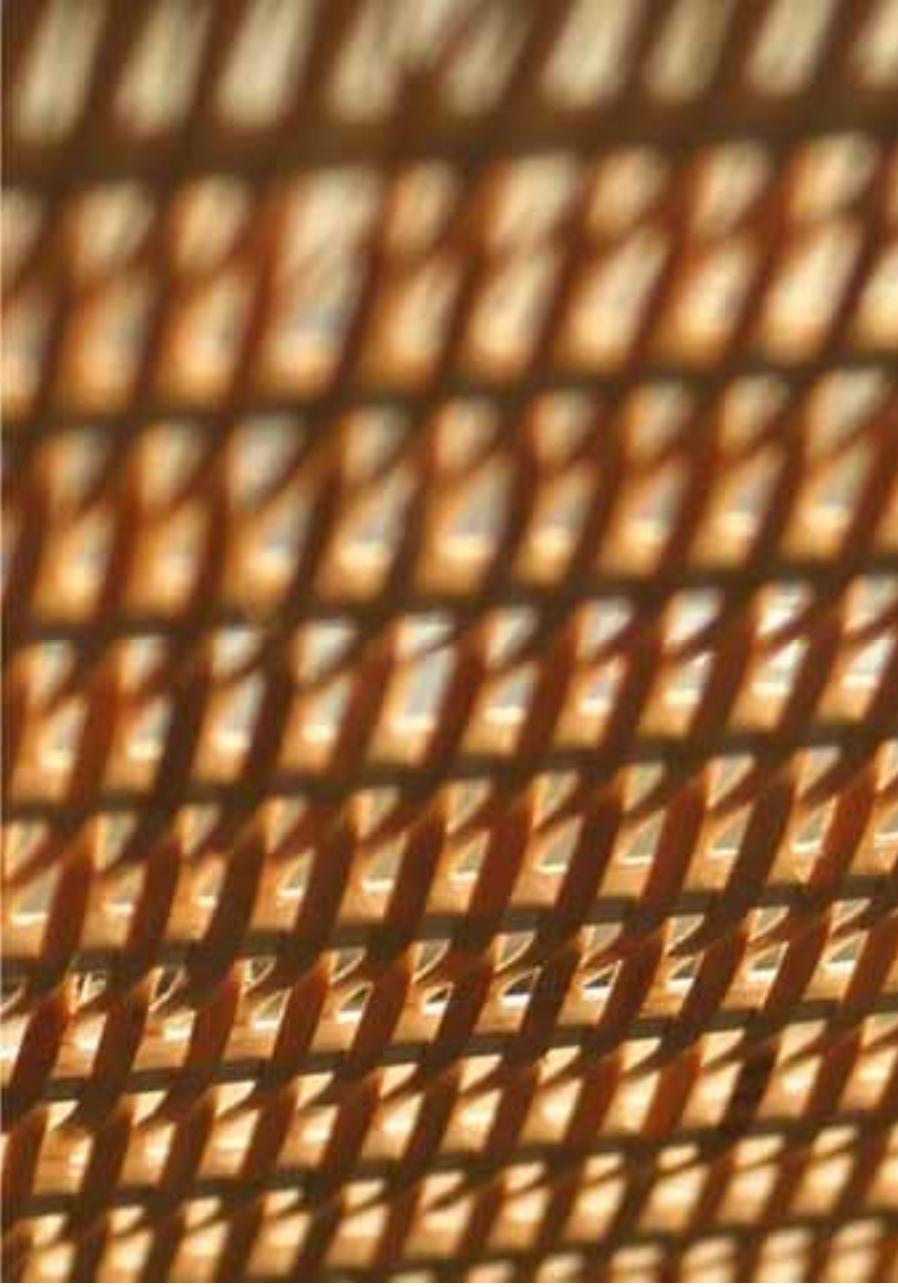


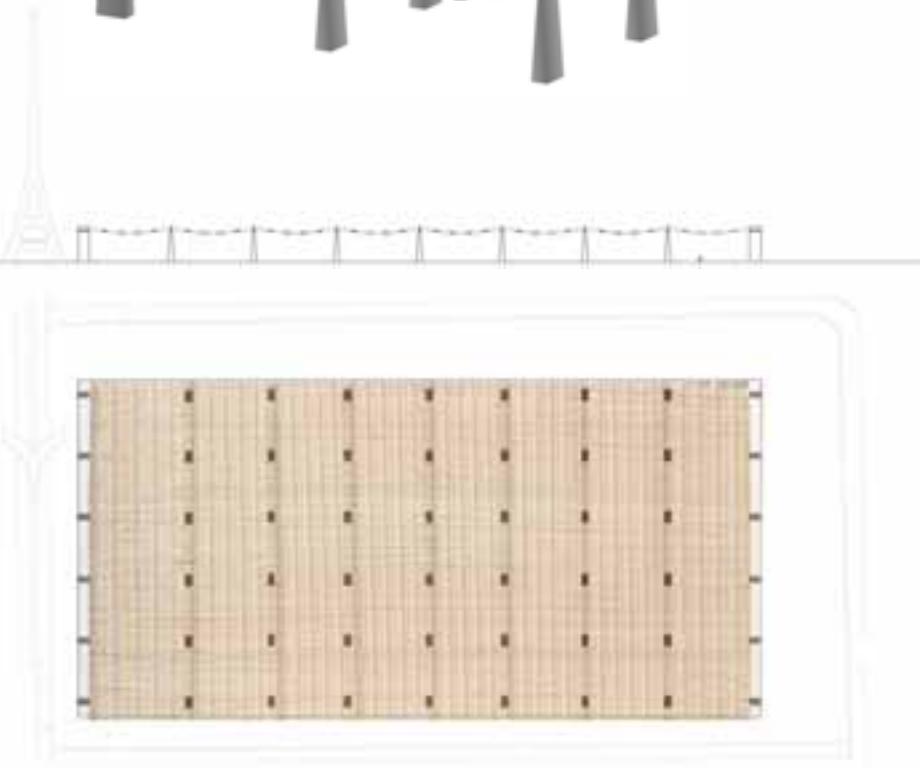
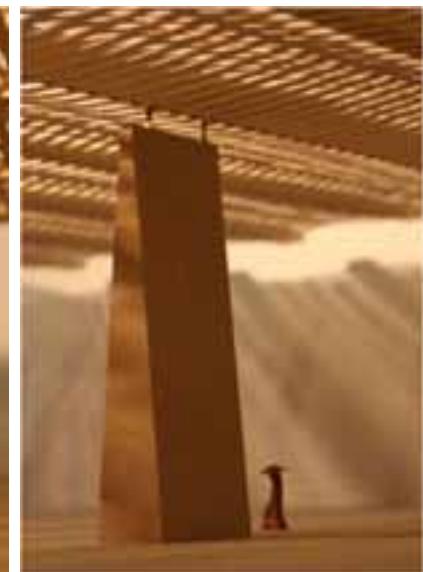
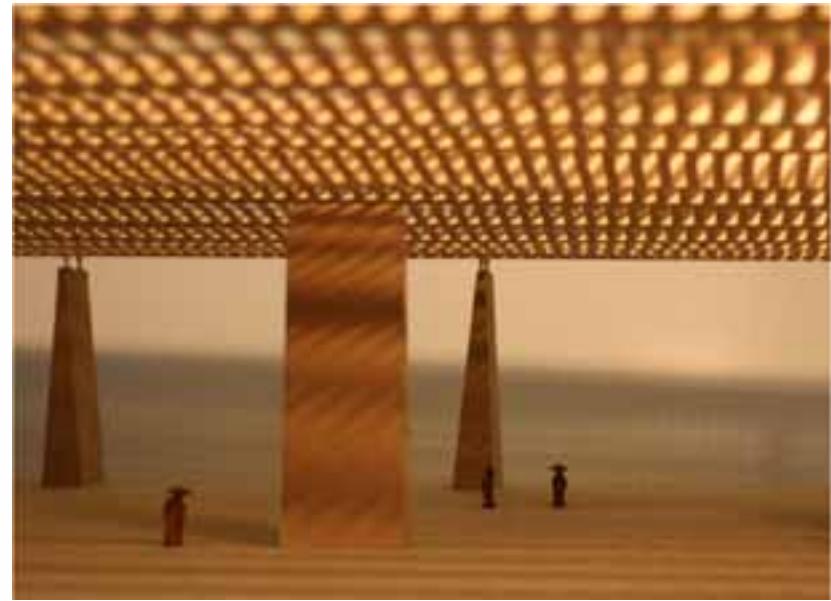
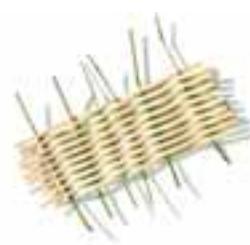
Atelier Weinand Autumn 07 Prof. Yves Weinand, Hani Buri, Markus Hudert
Student Jacopo Laffranchini

Innovative Timber Constructions
Yves Weinand



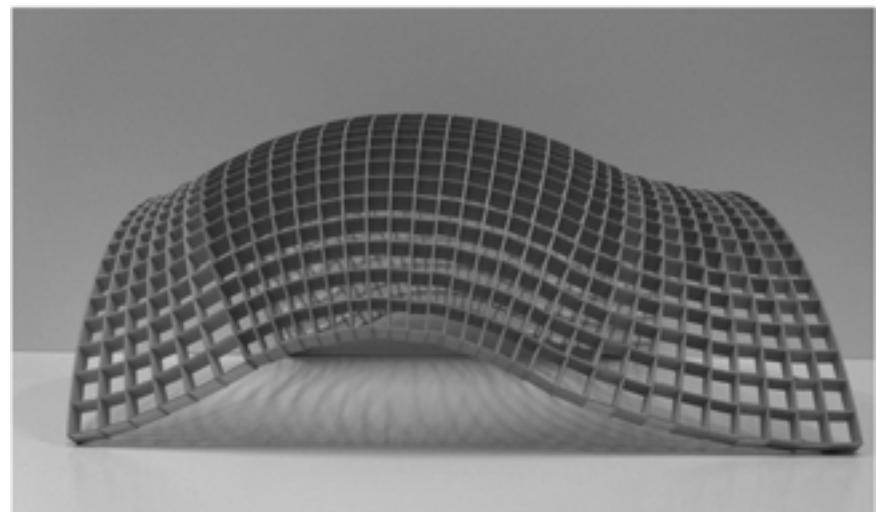
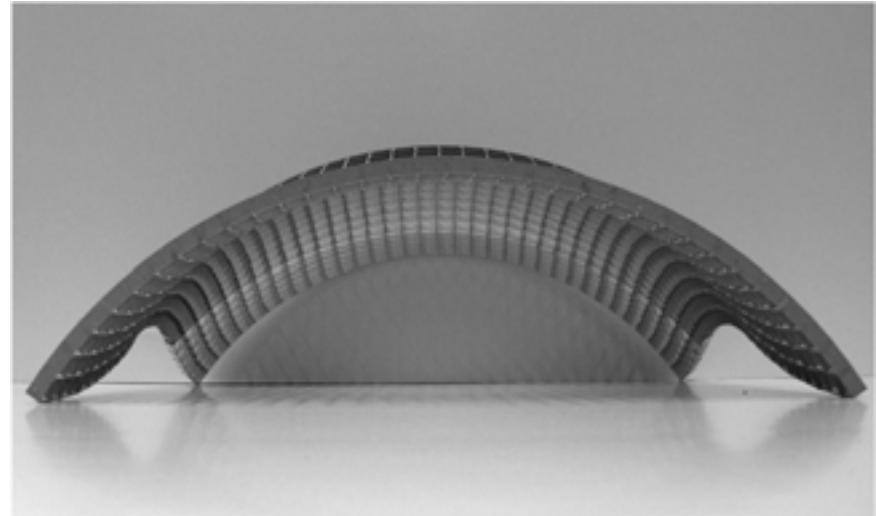
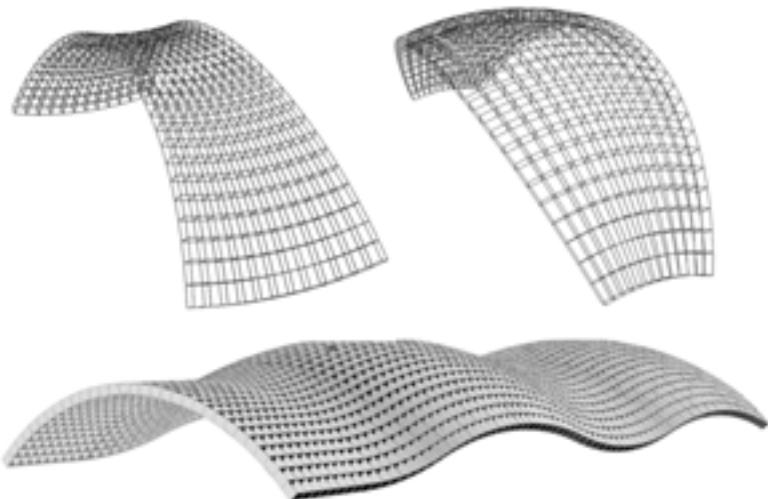
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Atelier Weinand Spring 07 Prof. Yves Weinand, Hani Buri, Ivo Stotz
Student Sophie Carpentieri

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Yves Weinand



Atelier Weinand Autumn 06 Prof. Yves Weinand, Hani Buri, Ivo Stotz
Student Celine Kobel

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Yves Weinand



Atelier Weinand Autumn 09 Prof. Yves Weinand, Fred Hatt, Markus Hudert
Student Magdalena Besomi

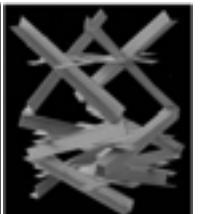
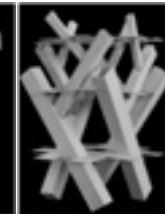
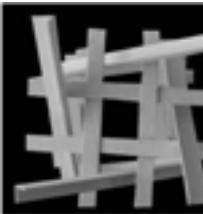
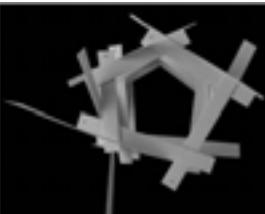
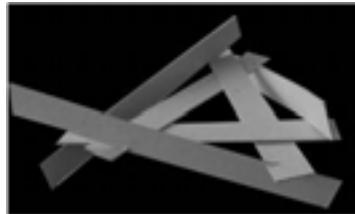
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2D

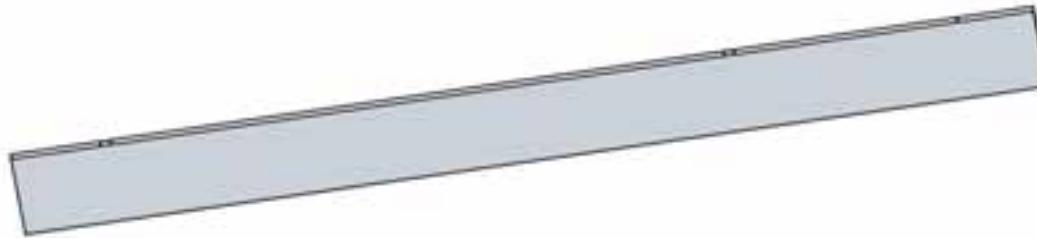


3D



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TISSU 1

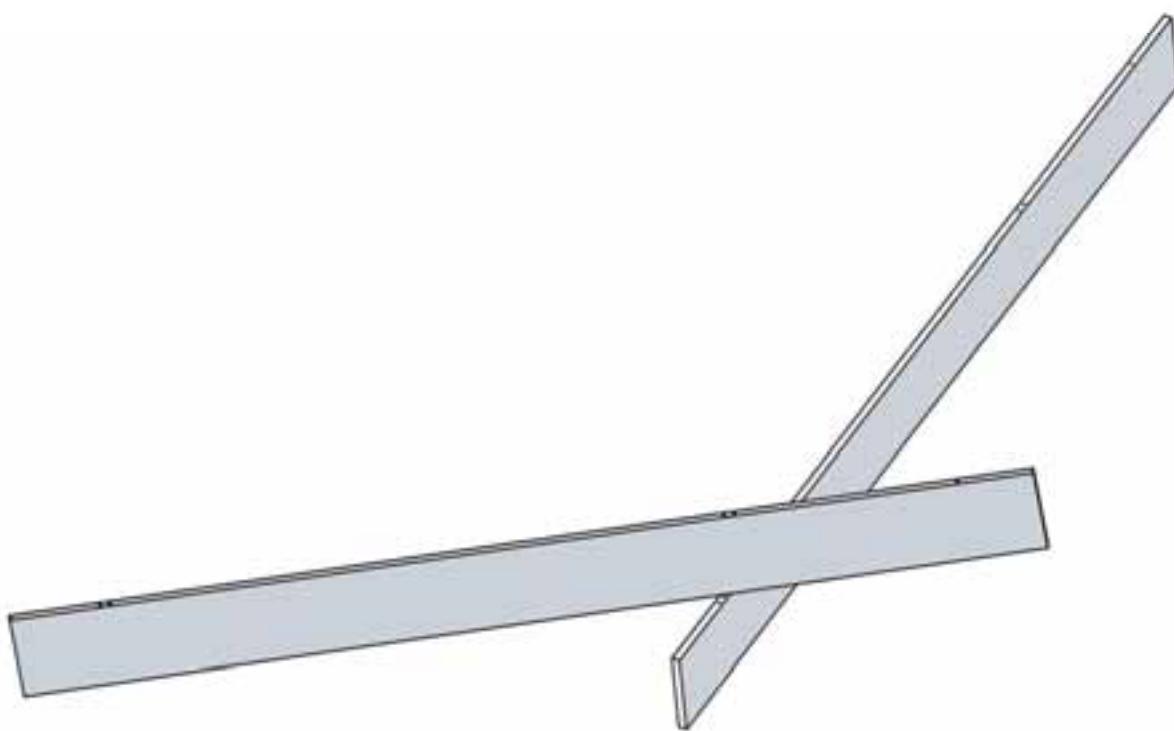


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TISSU 1

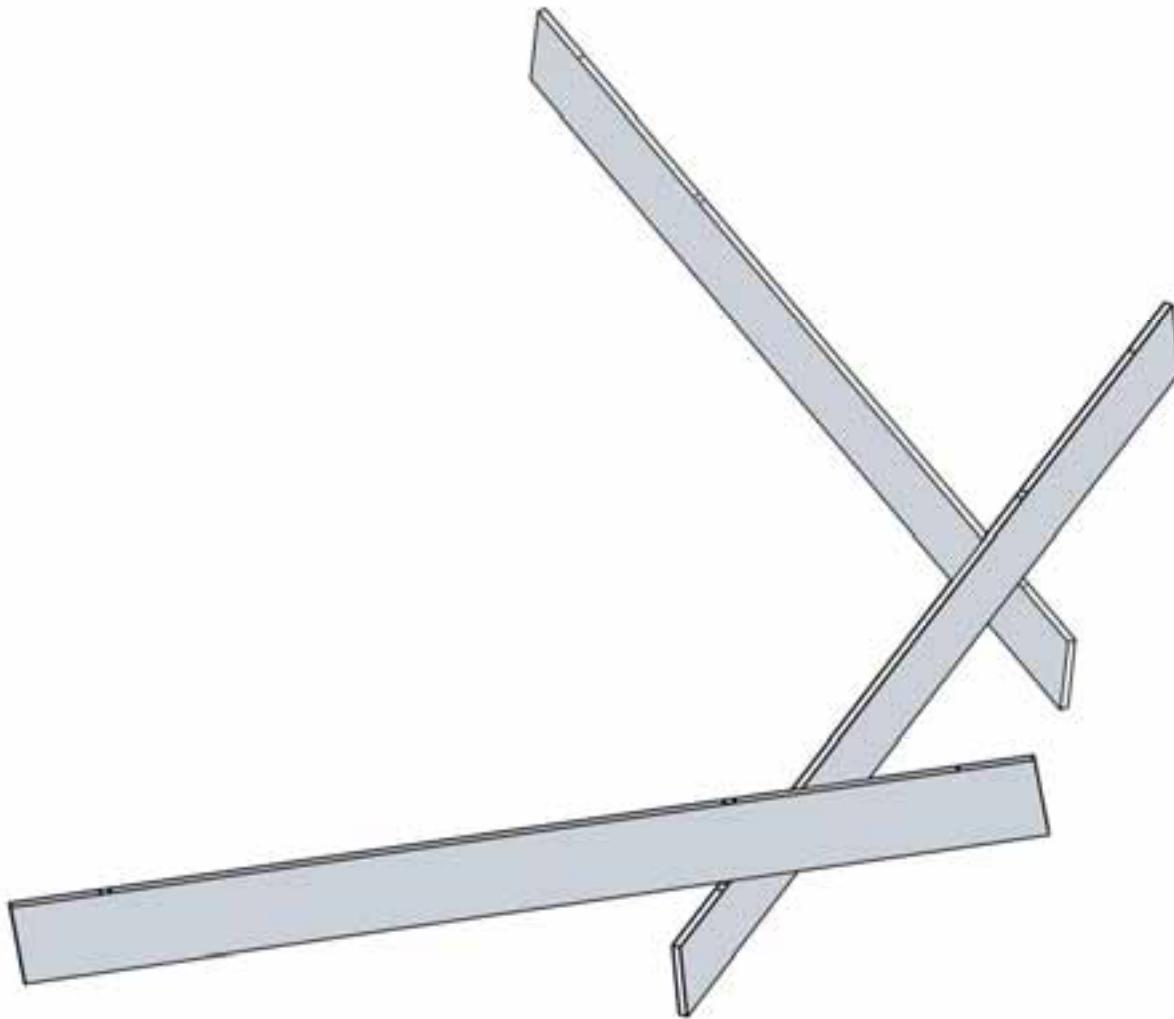


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Student Magdalena Besomi

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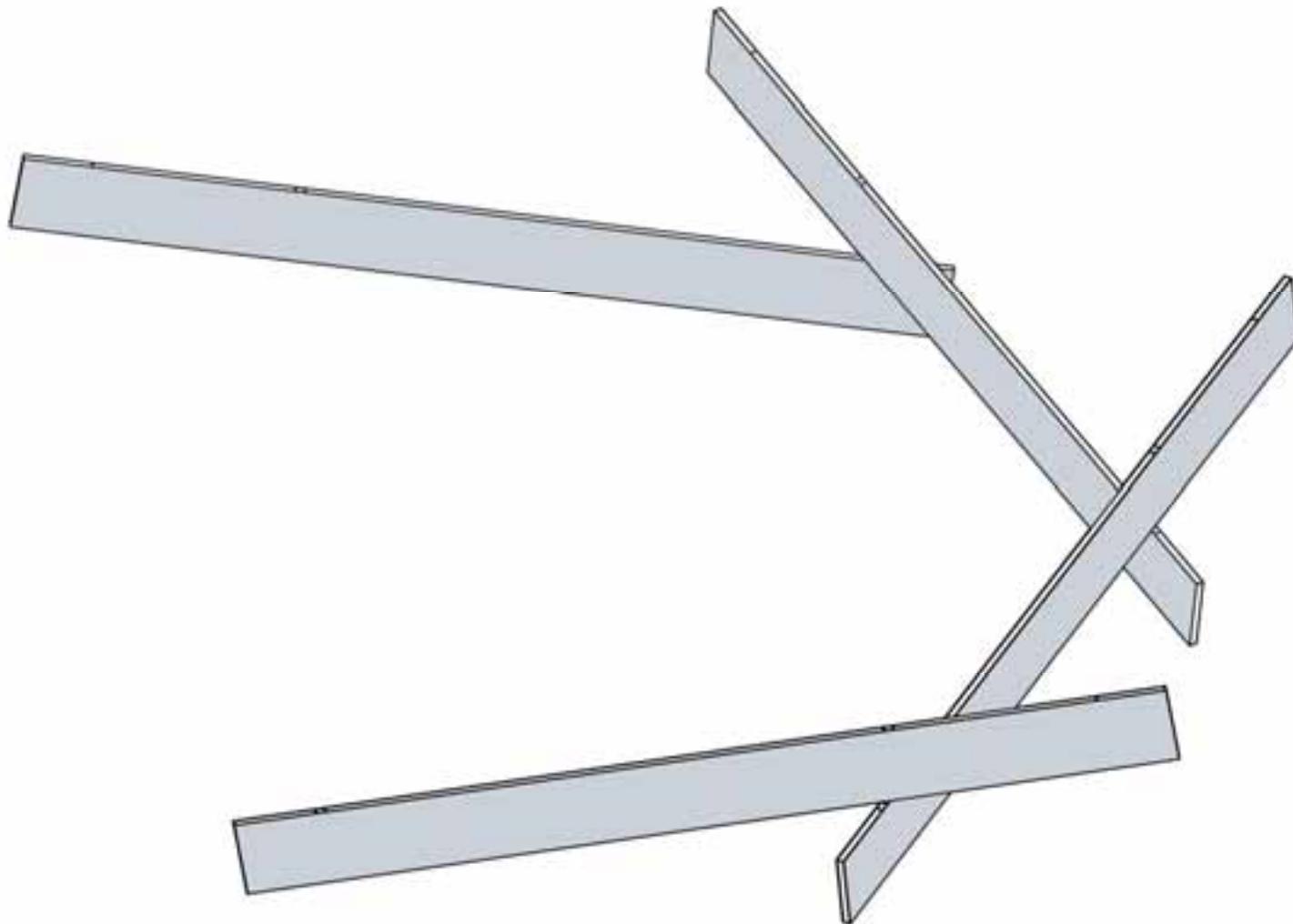
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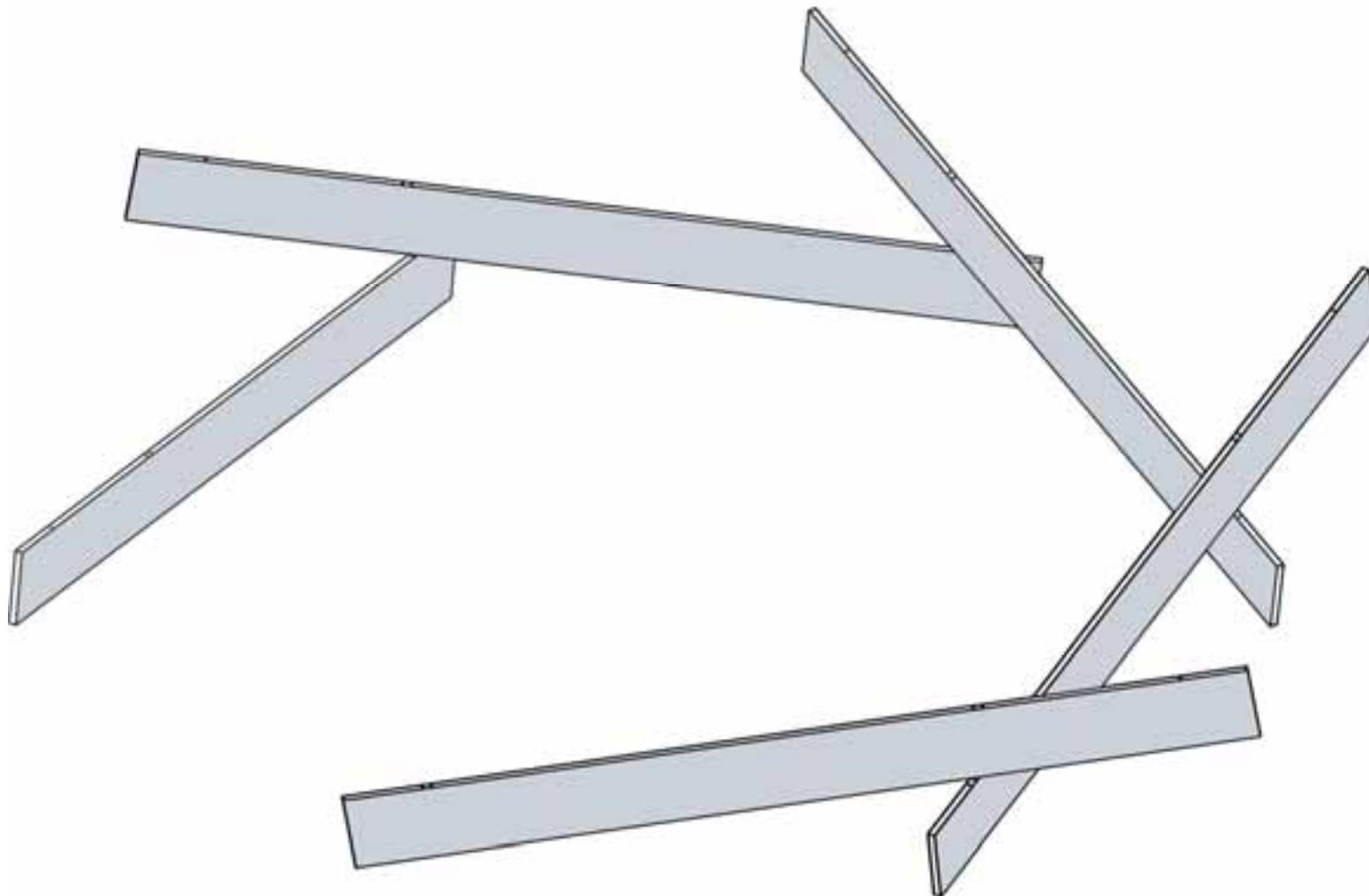
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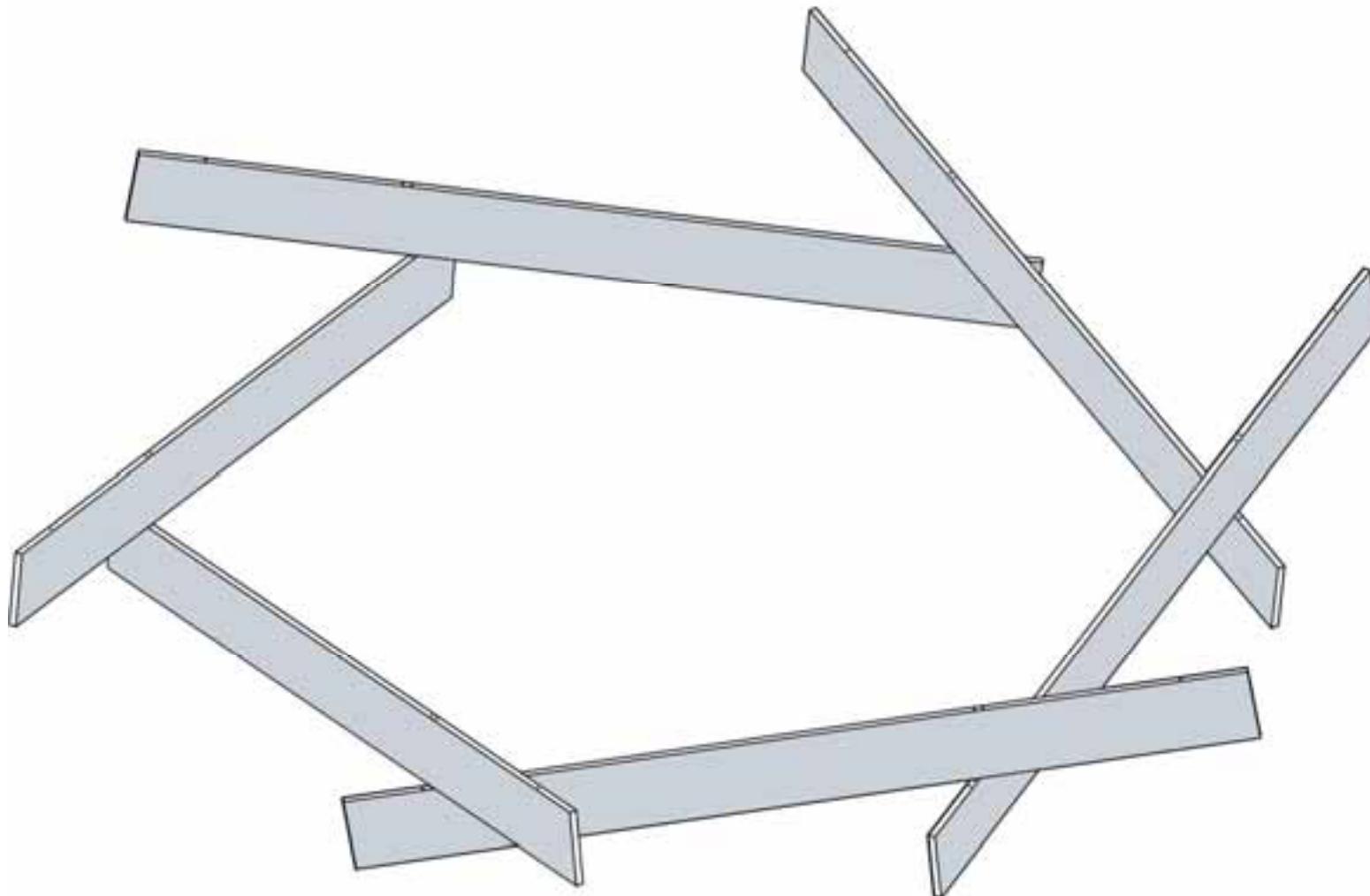
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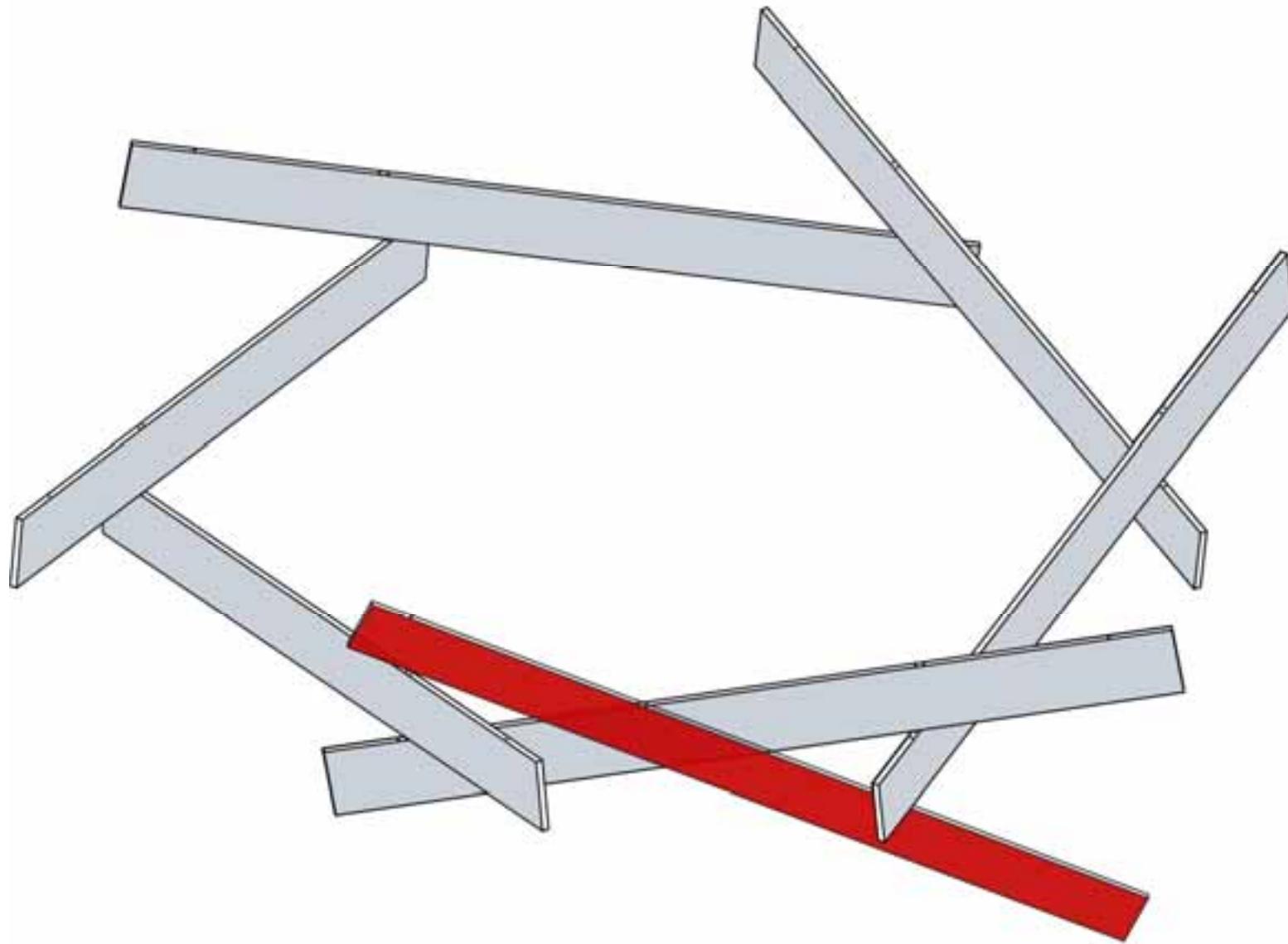
TISSU 1



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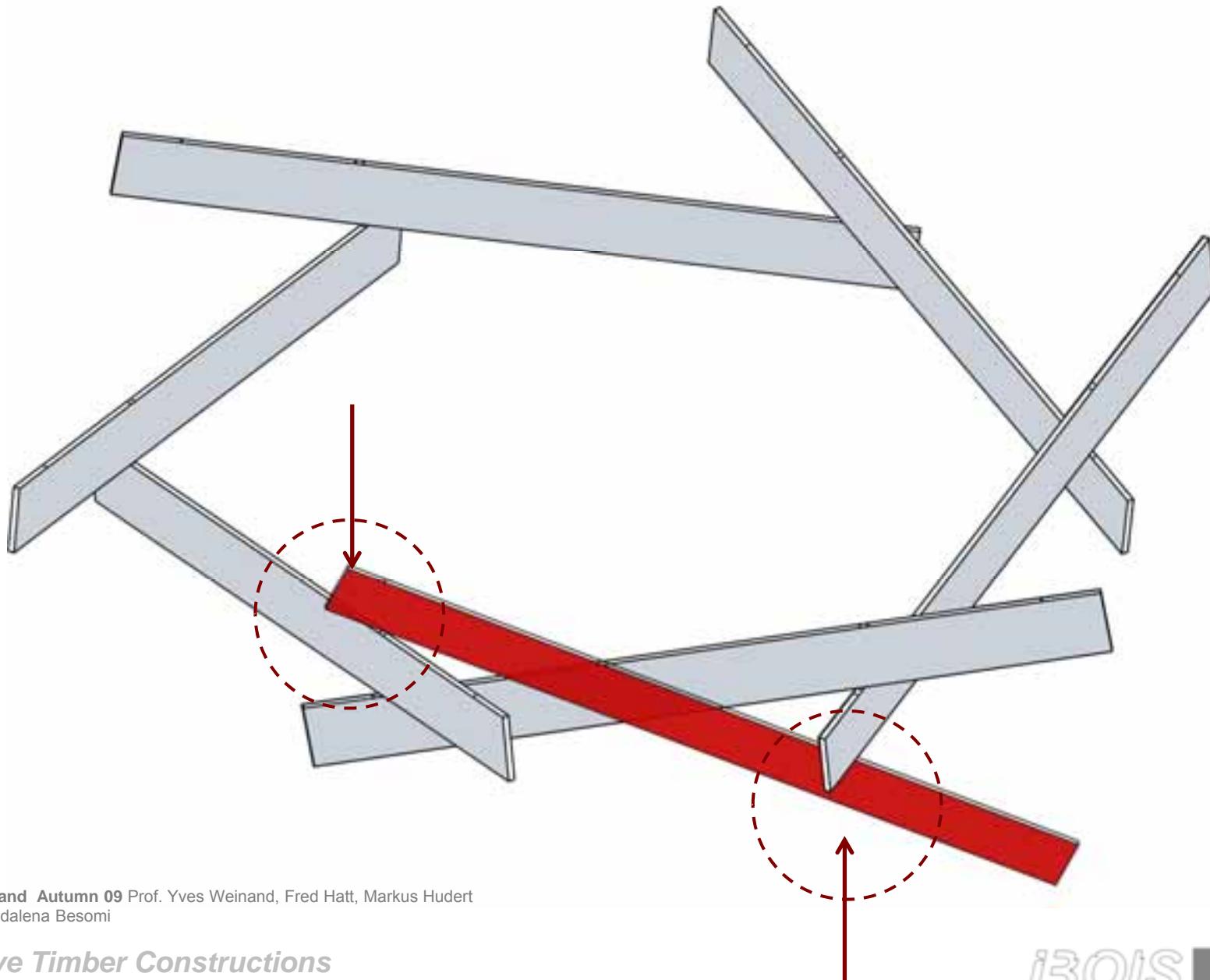
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Student Magdalena Besomi

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Yves Weinand

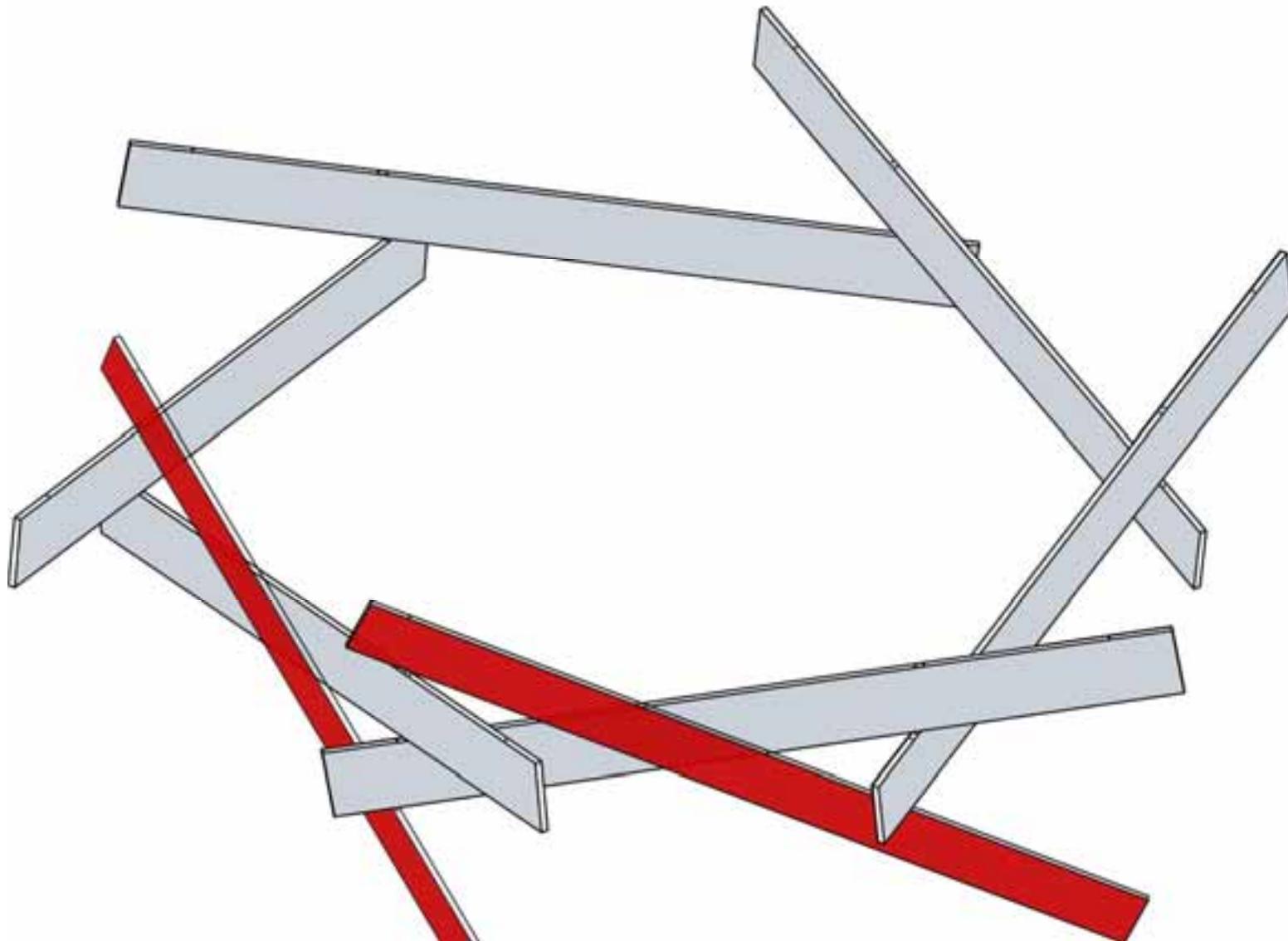
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Student Magdalena Besomi

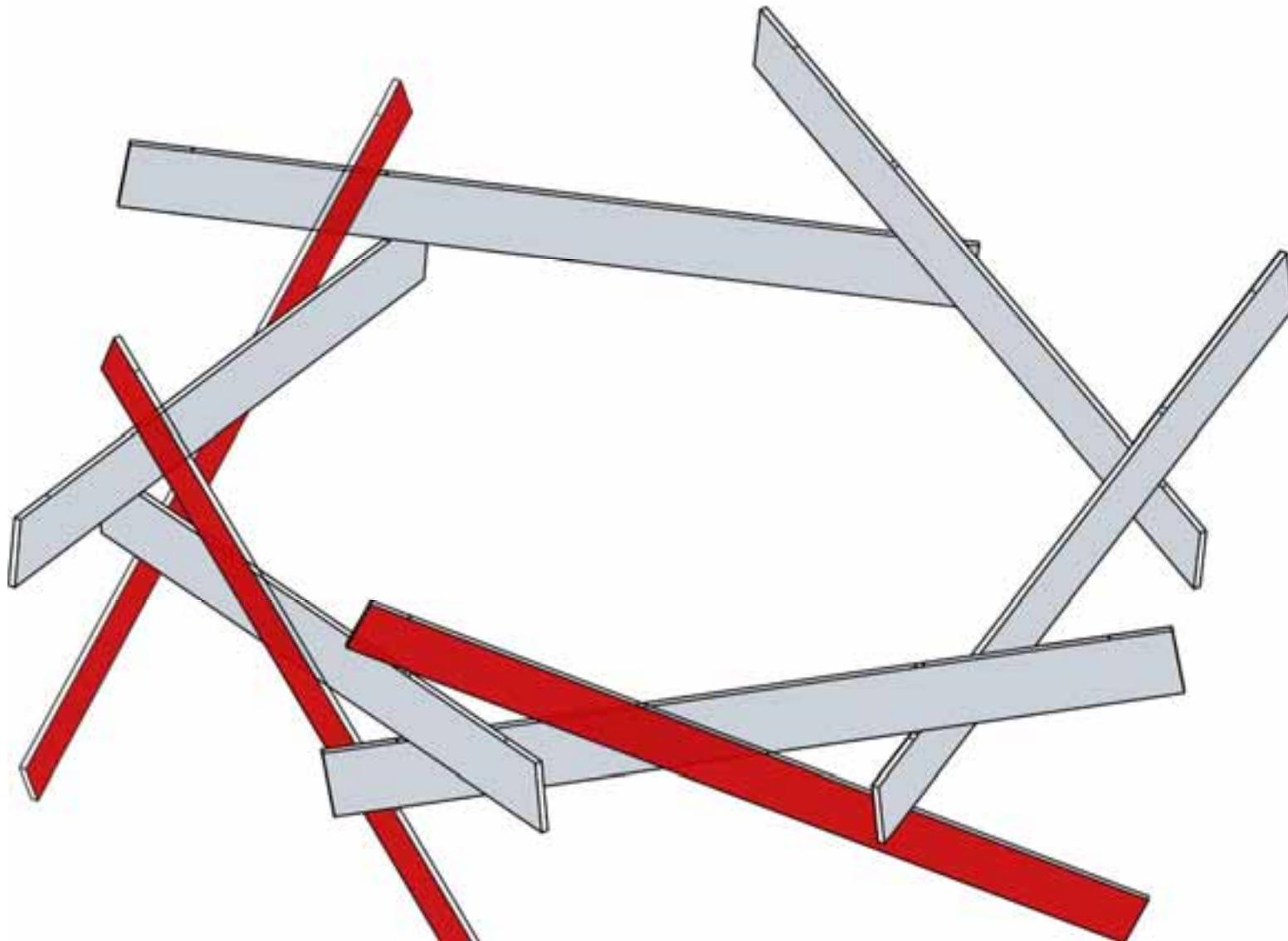
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TISSU 2



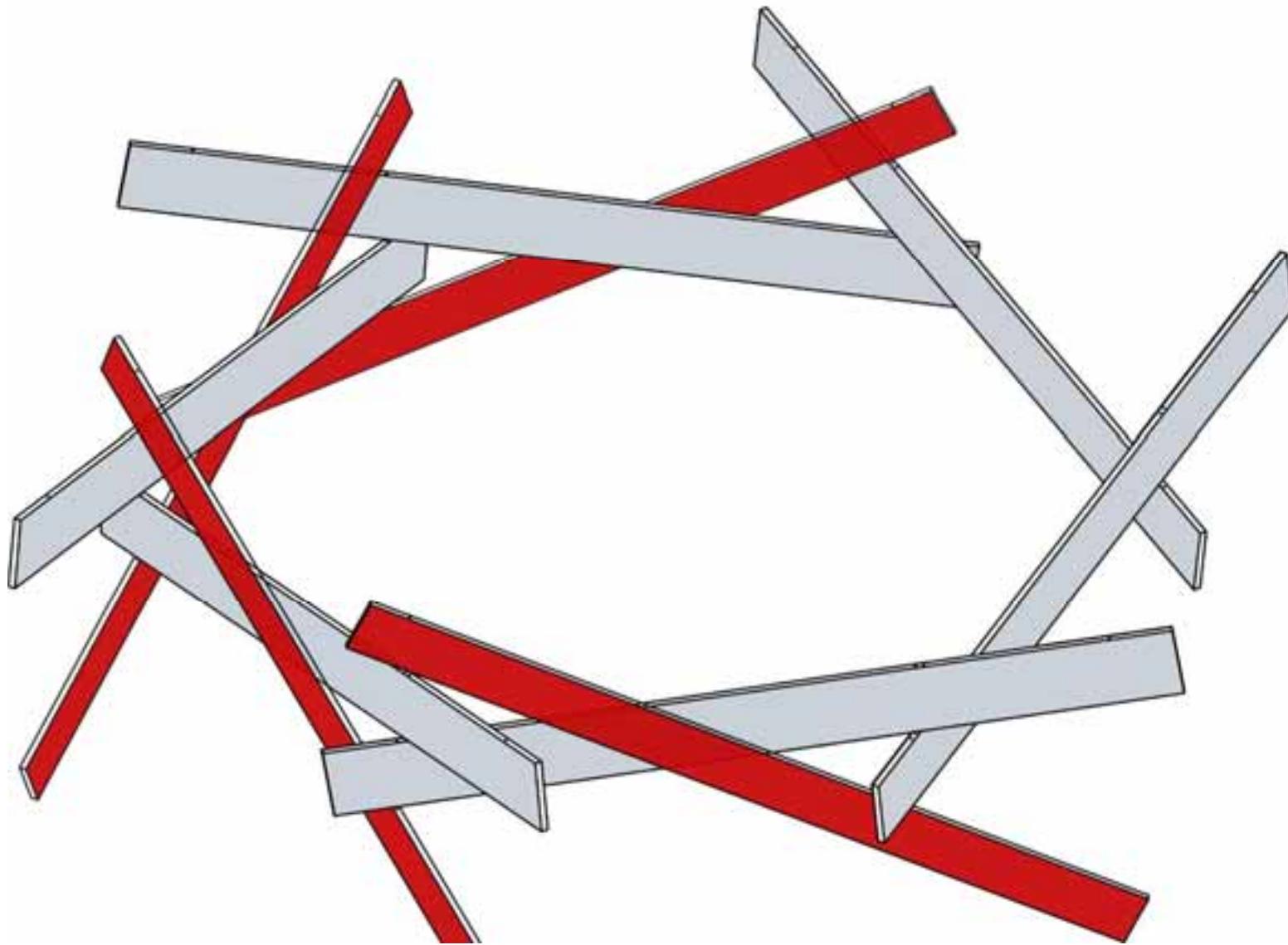
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Student Magdalena Besomi

TISSU 2



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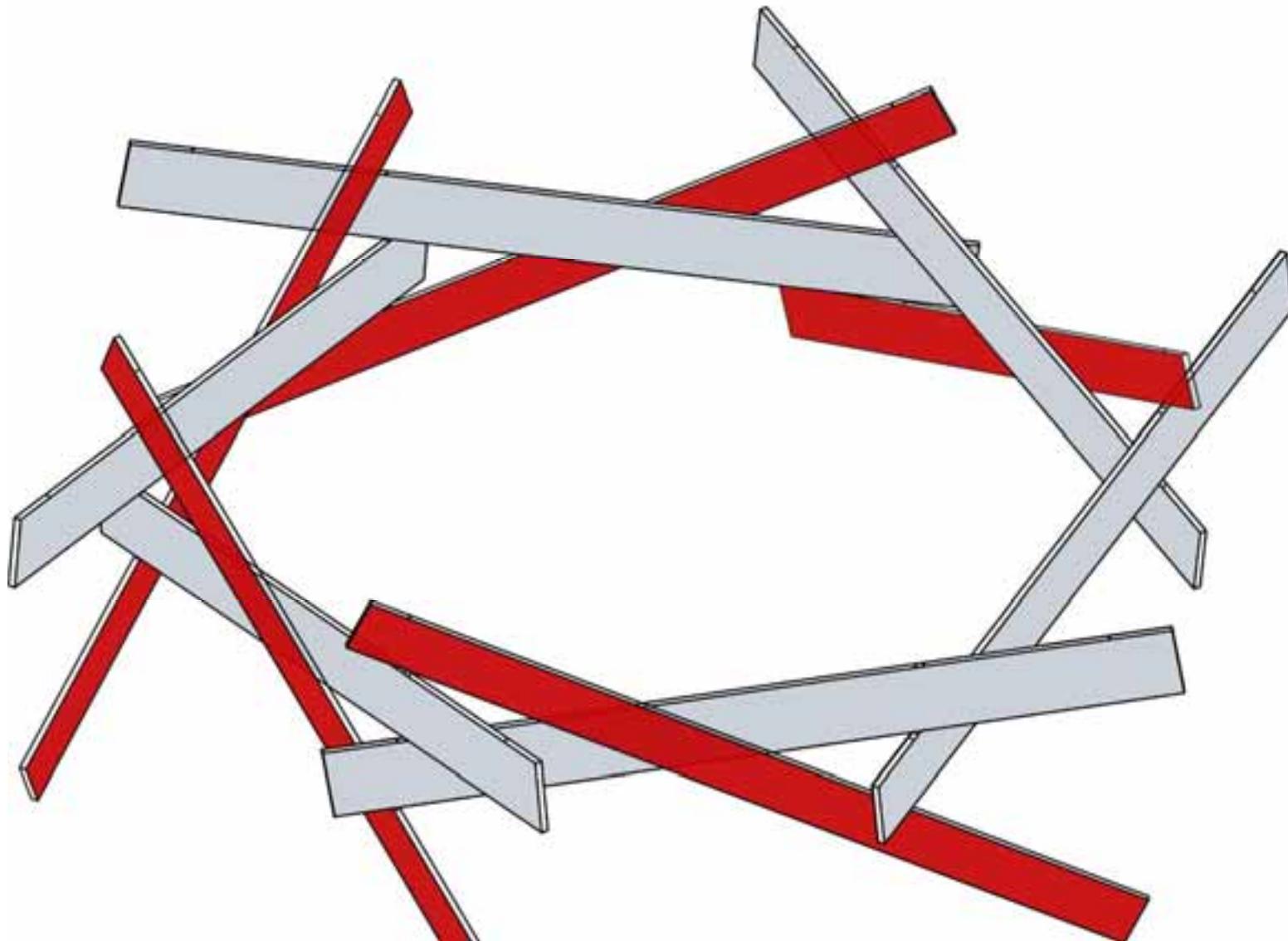
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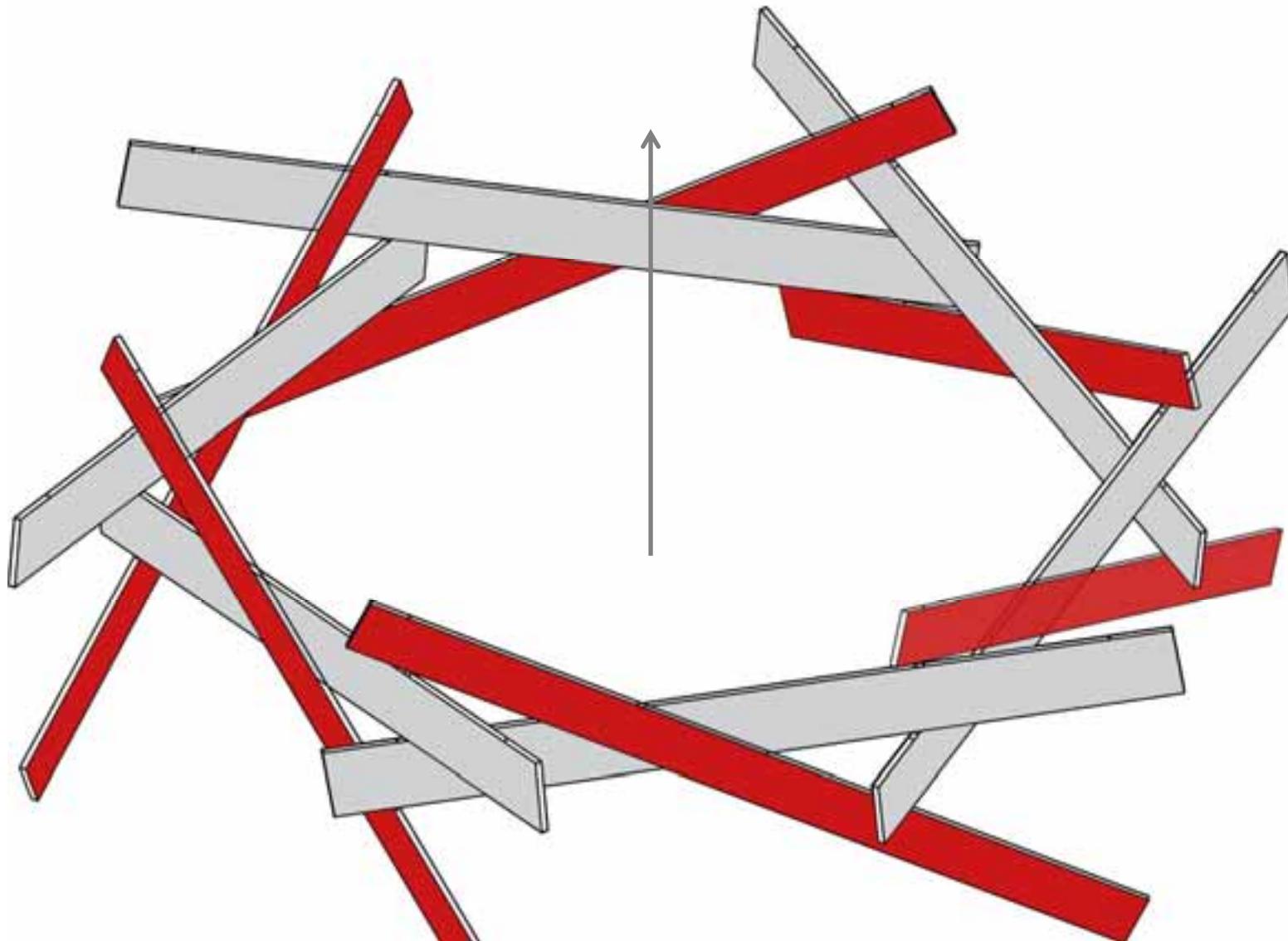
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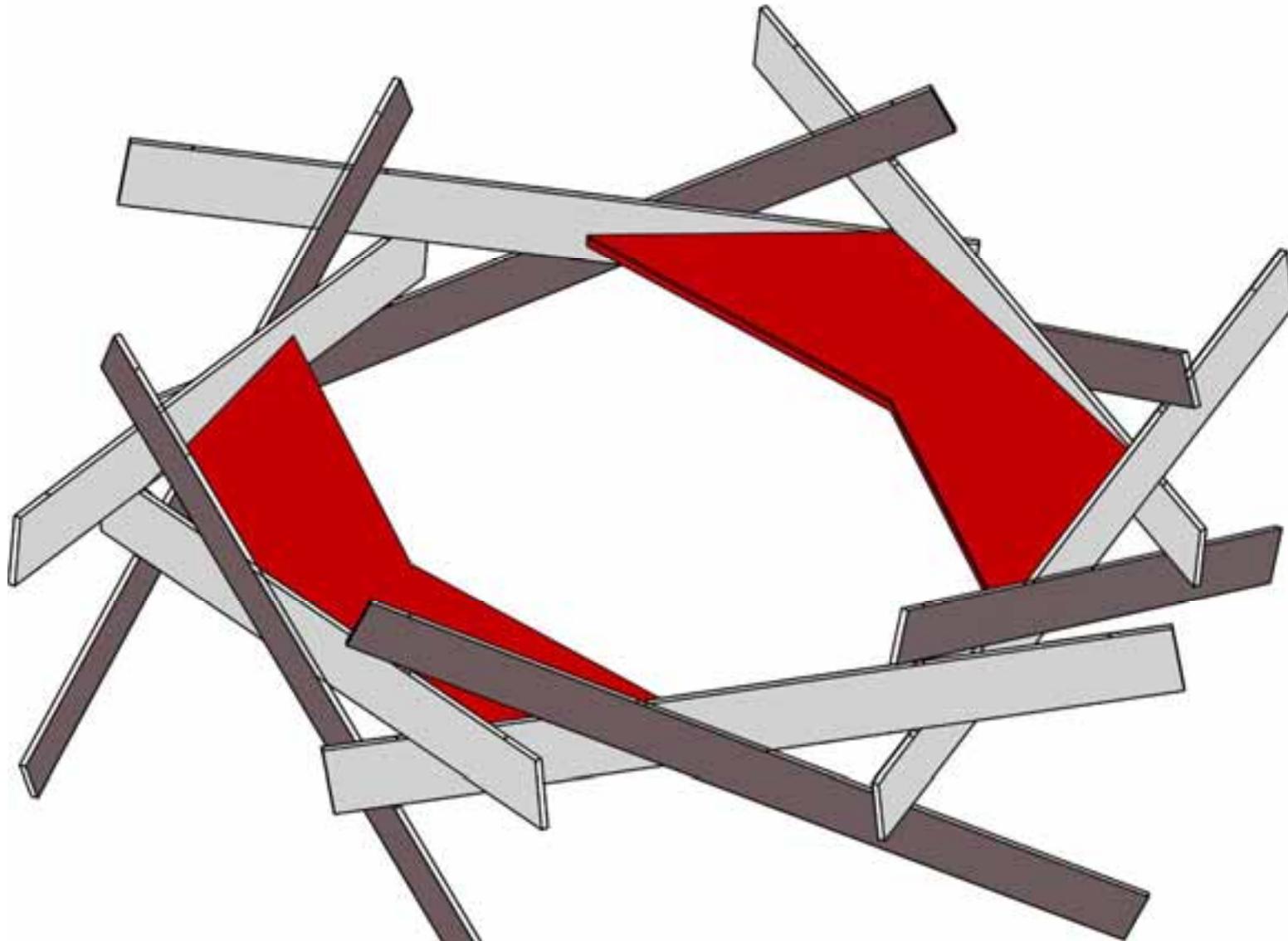
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TISSU 2



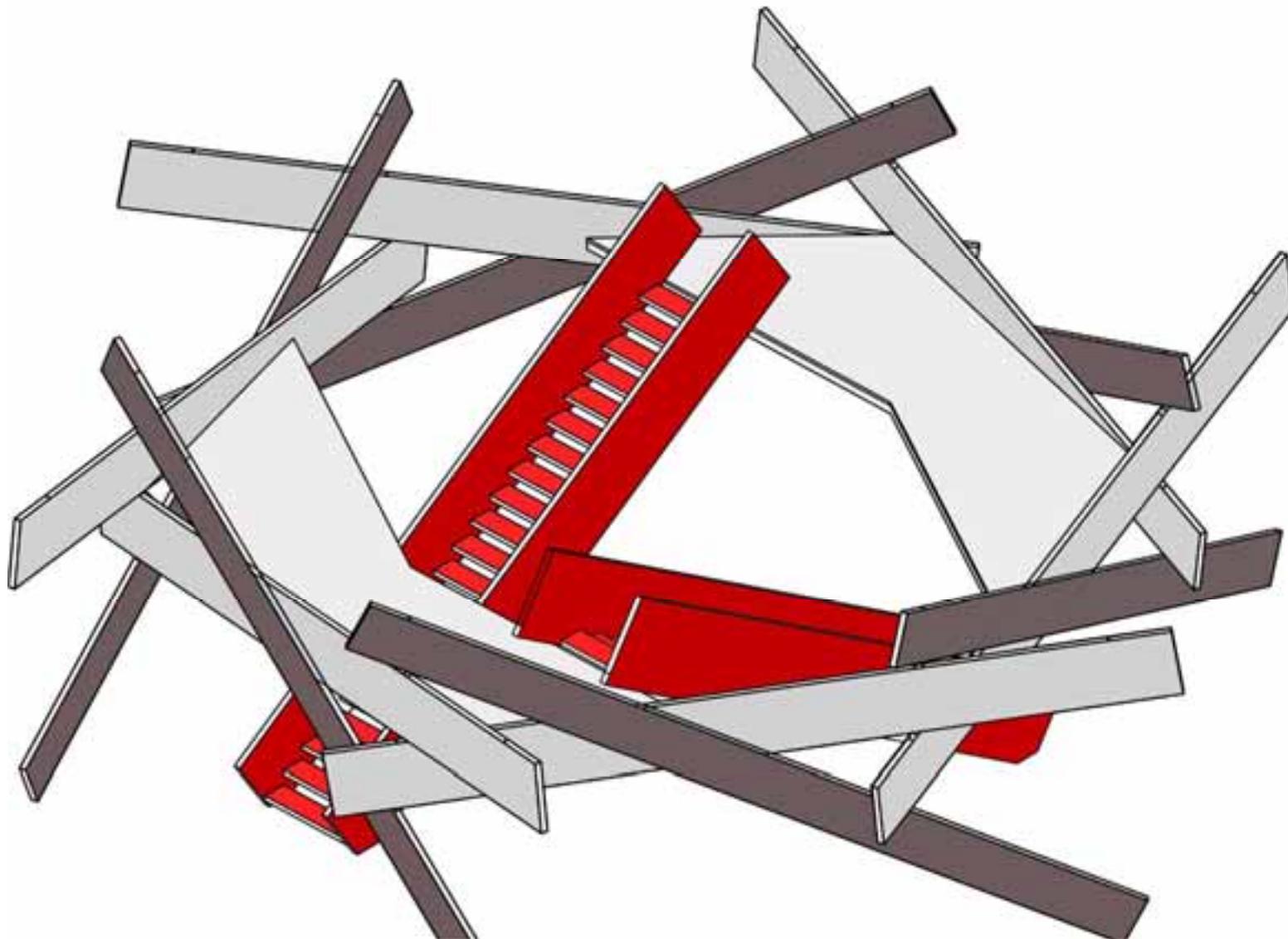
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PALIERS



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Student Magdalena Besomi

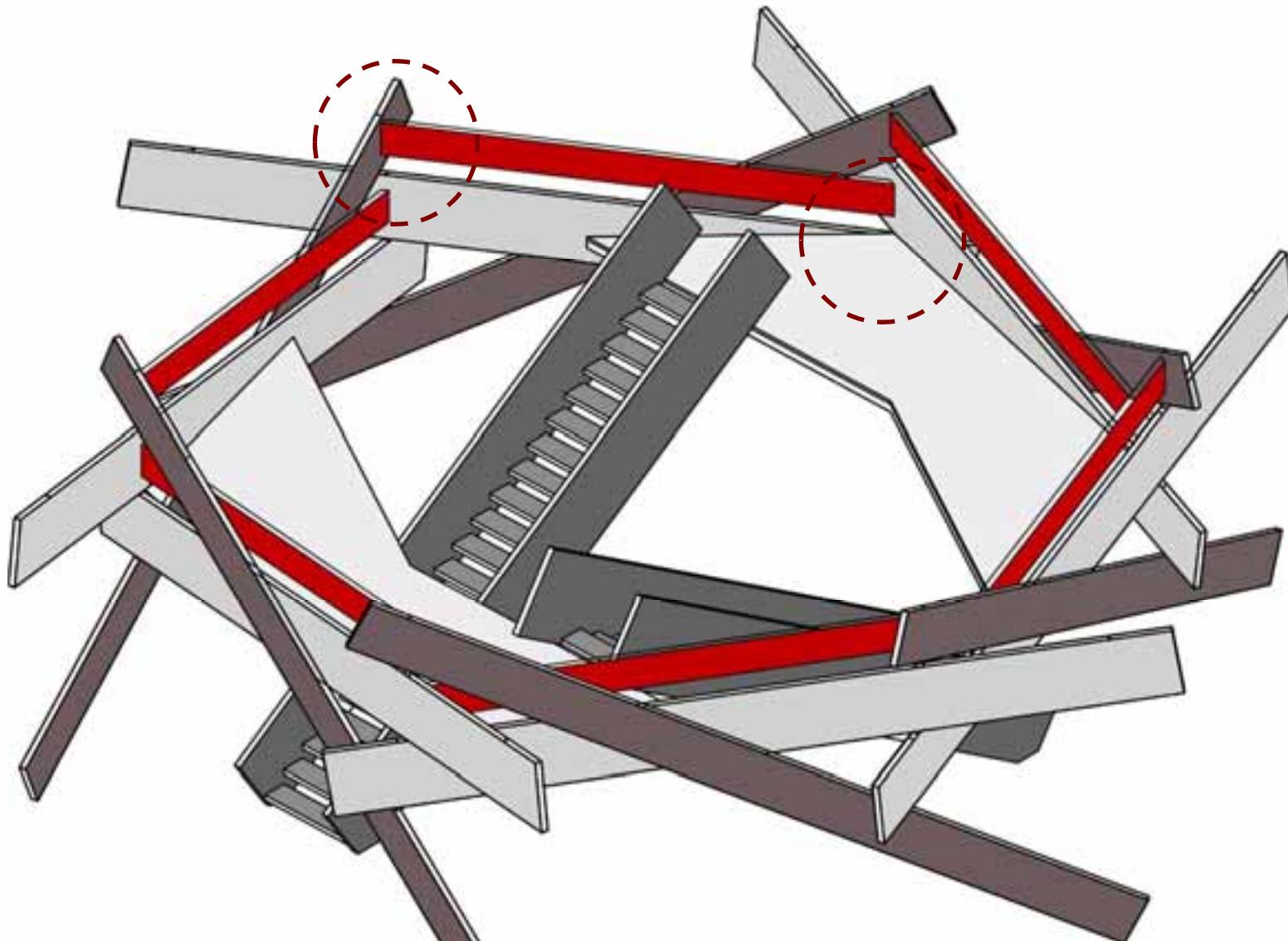
ESCALIERS



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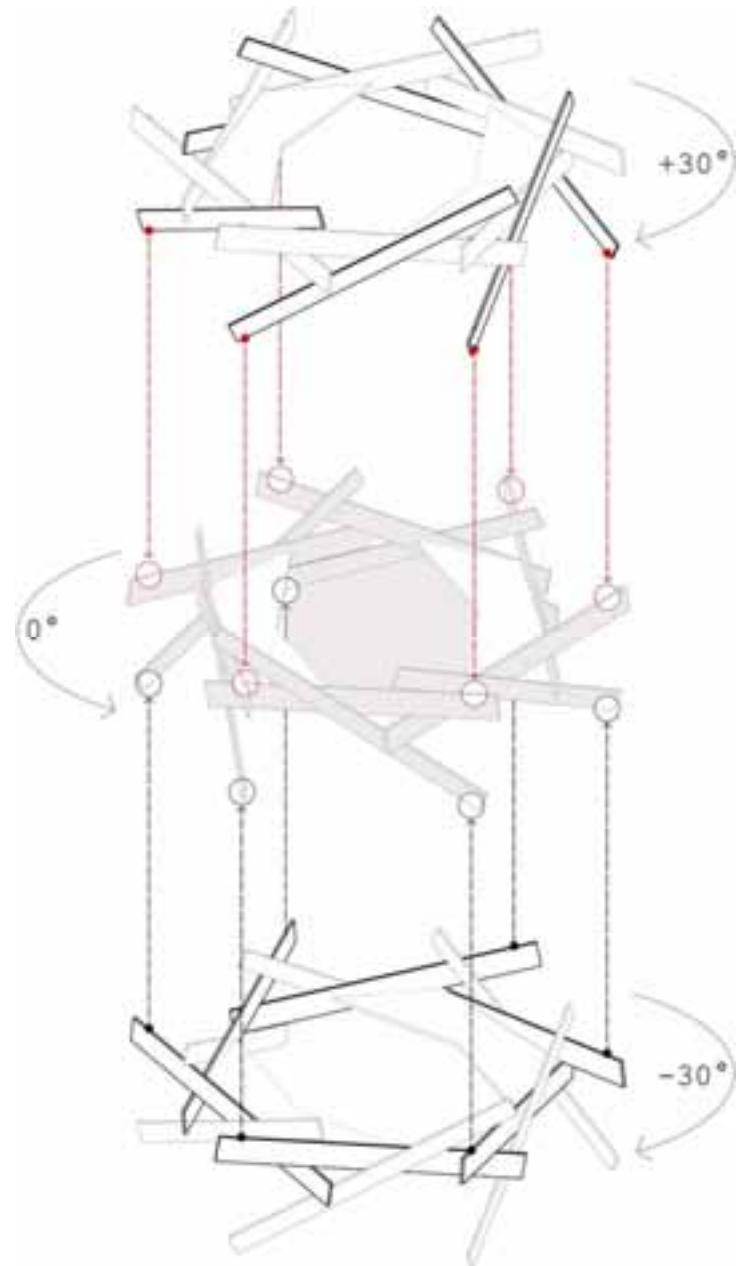
GARDES-CORPS

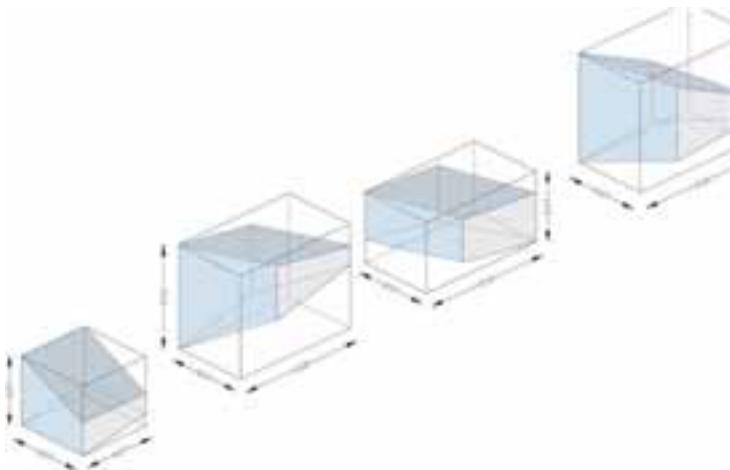


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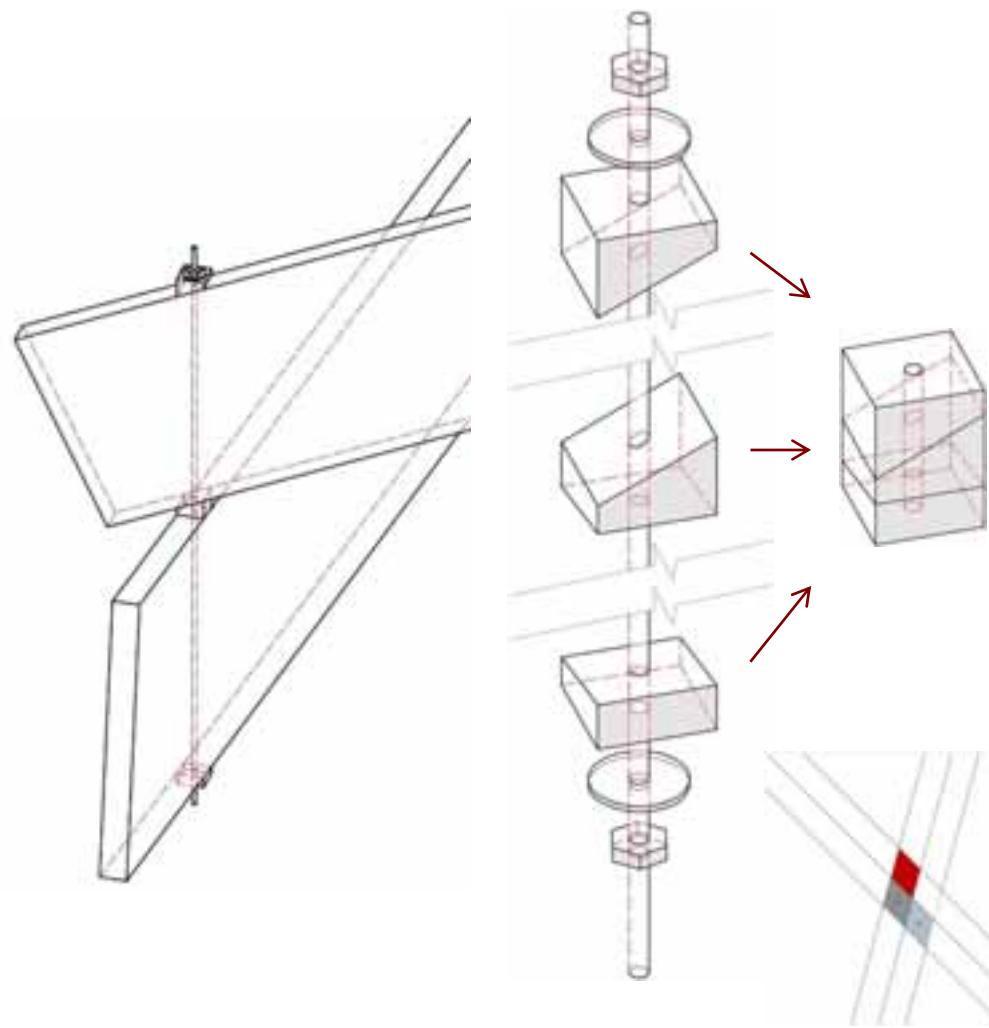


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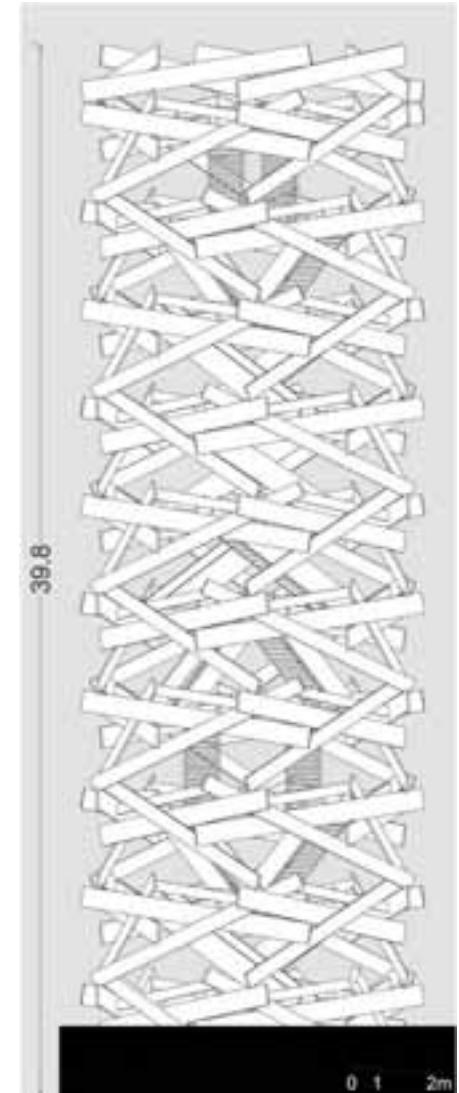
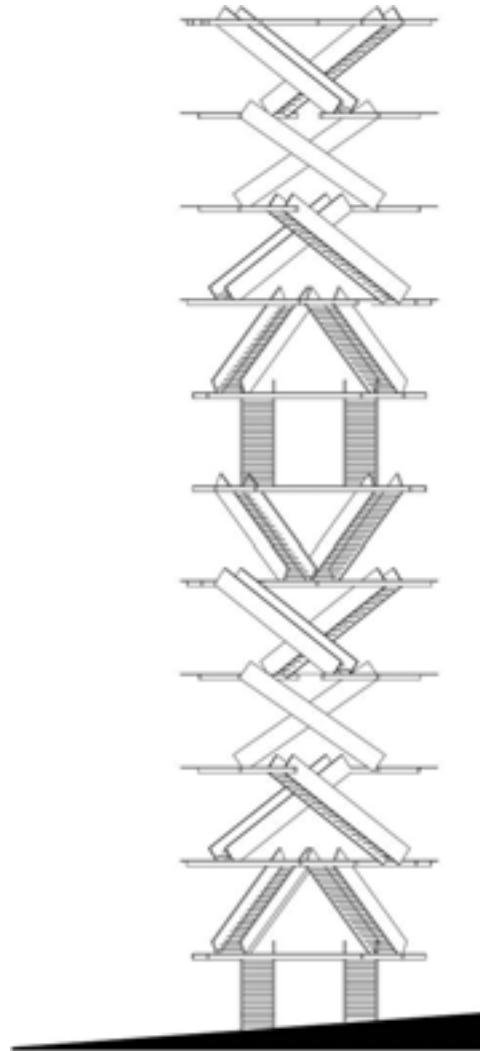


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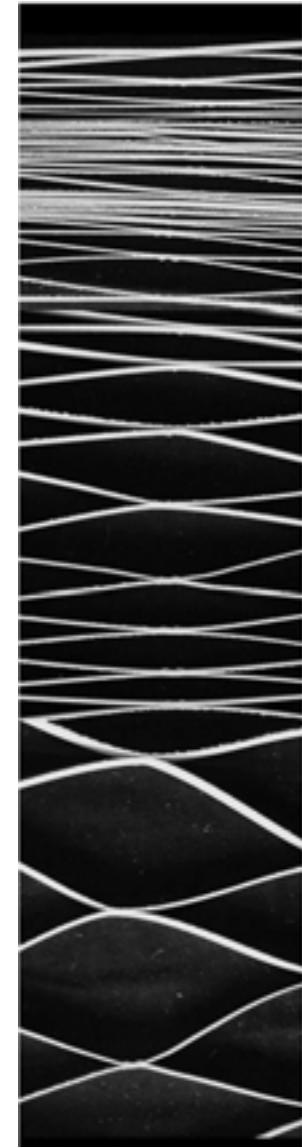
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tissage



module



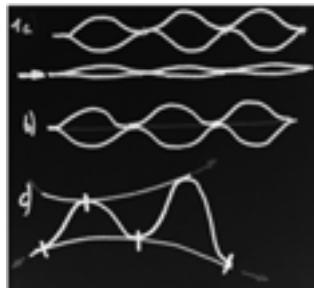
potentiel



géométrie



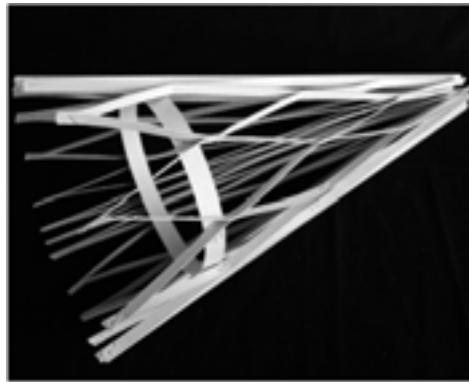
pattern



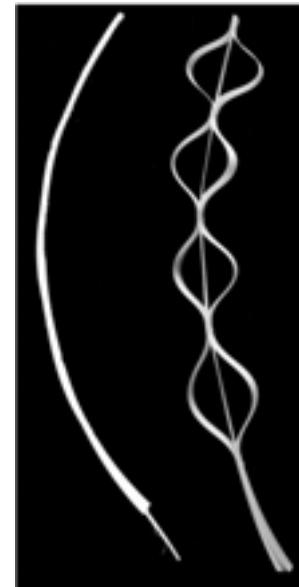
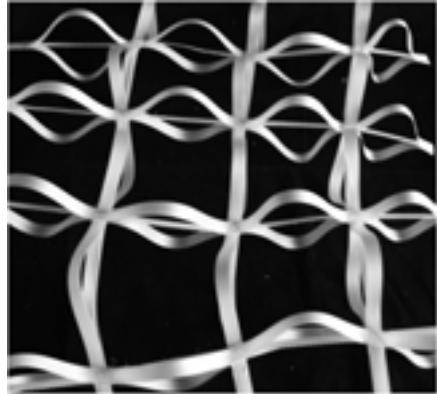
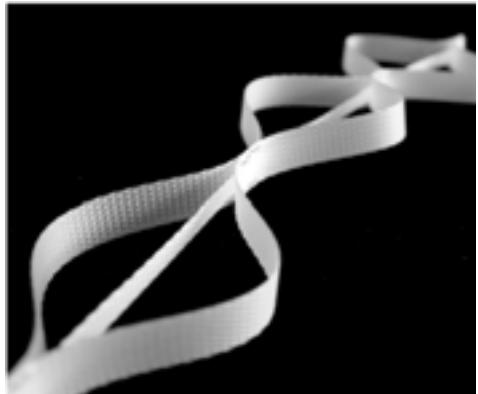
structure

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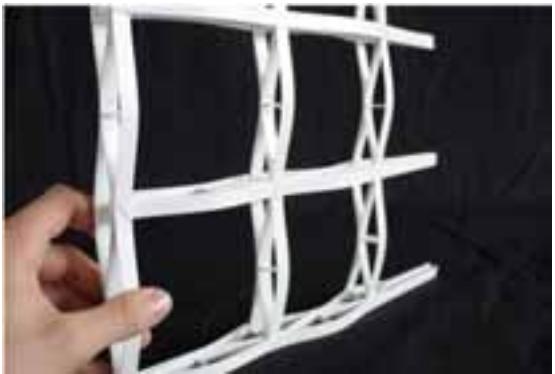
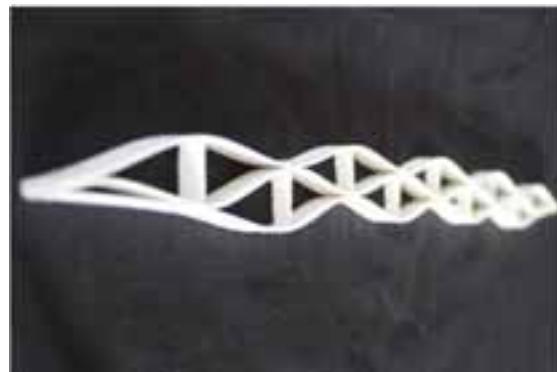
essai 01



essai 02

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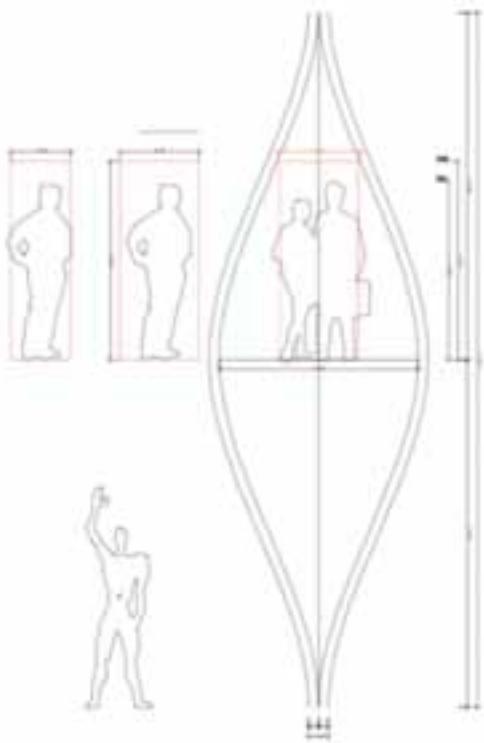
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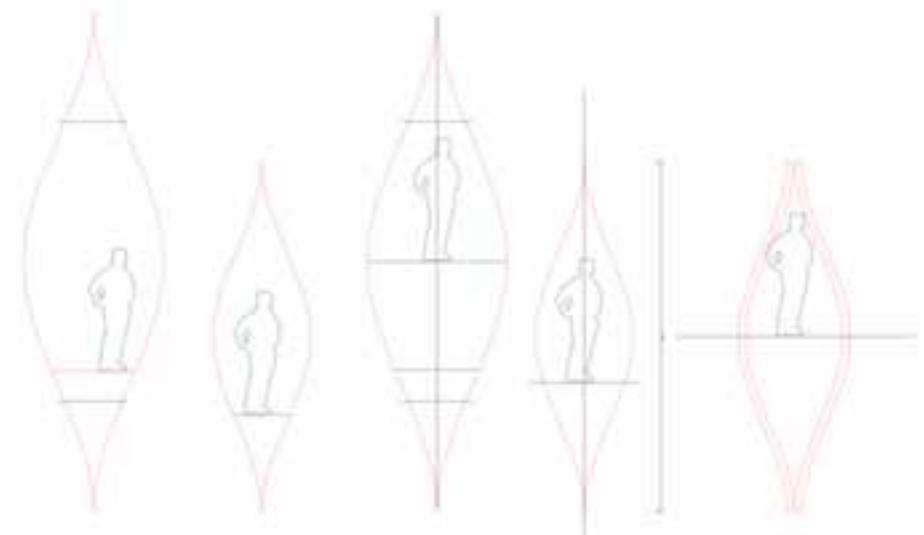
variantes d'utilisations du module

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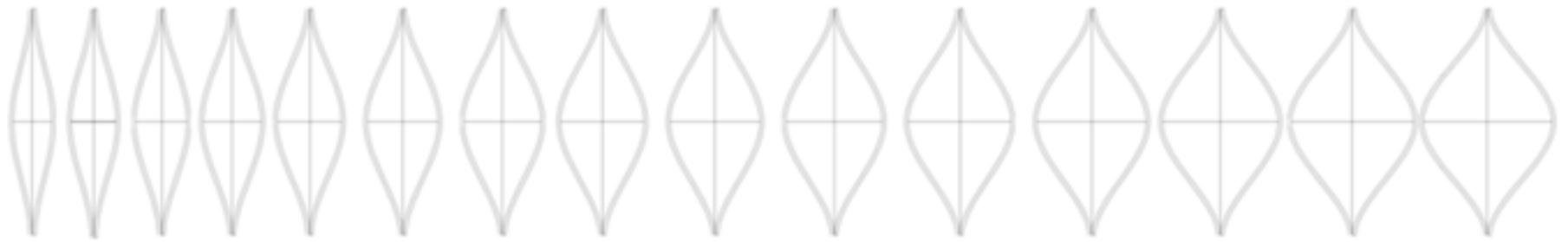
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échelle du module

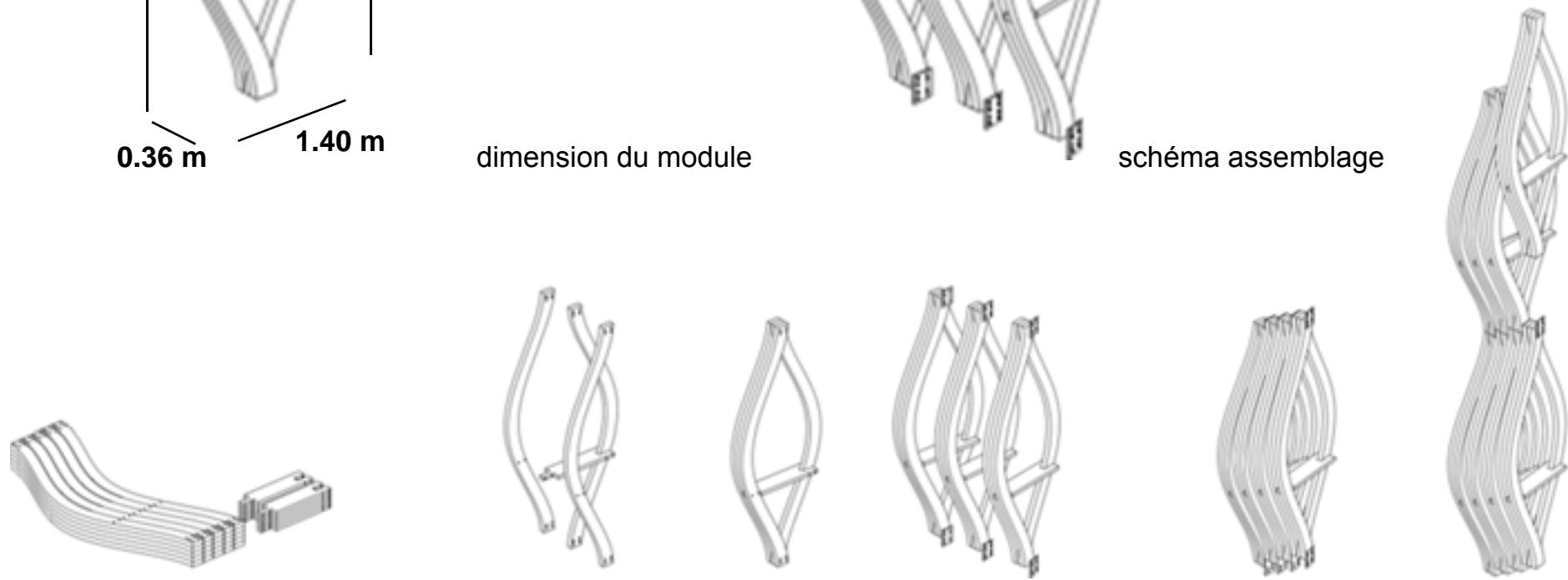
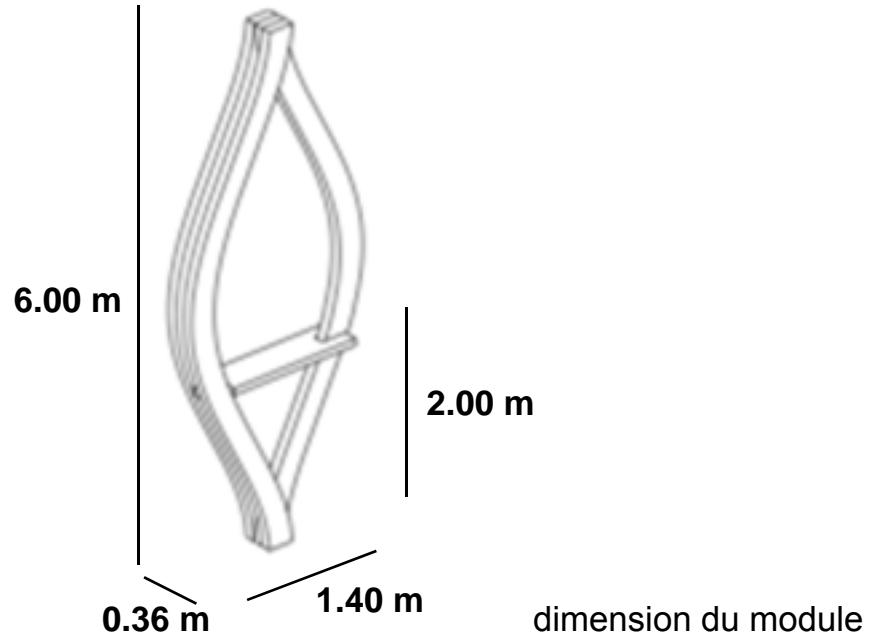


Position de la marche



variation du module

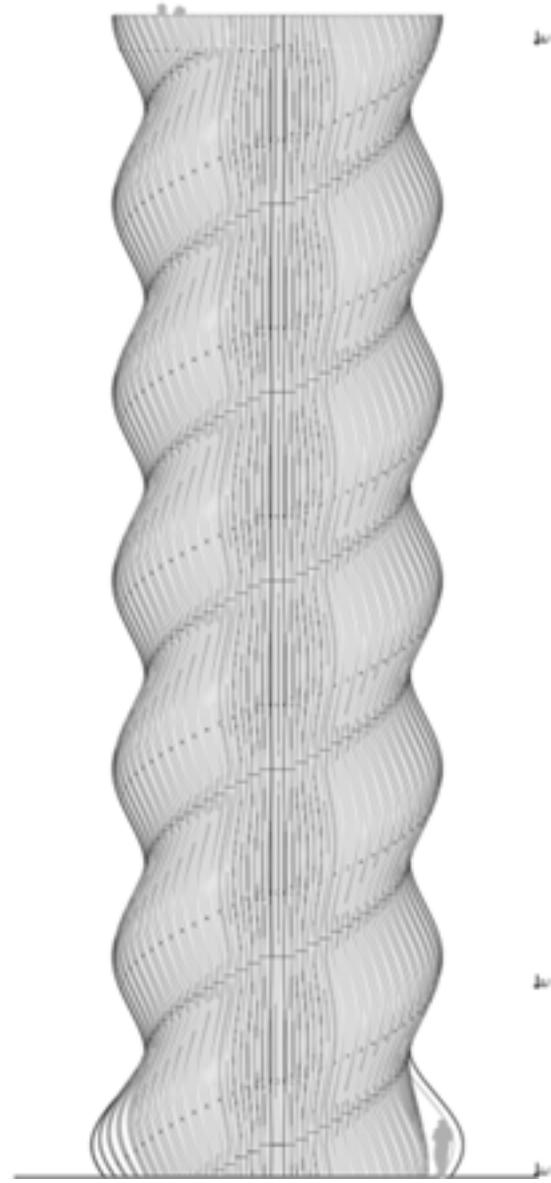
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coupe



élévation

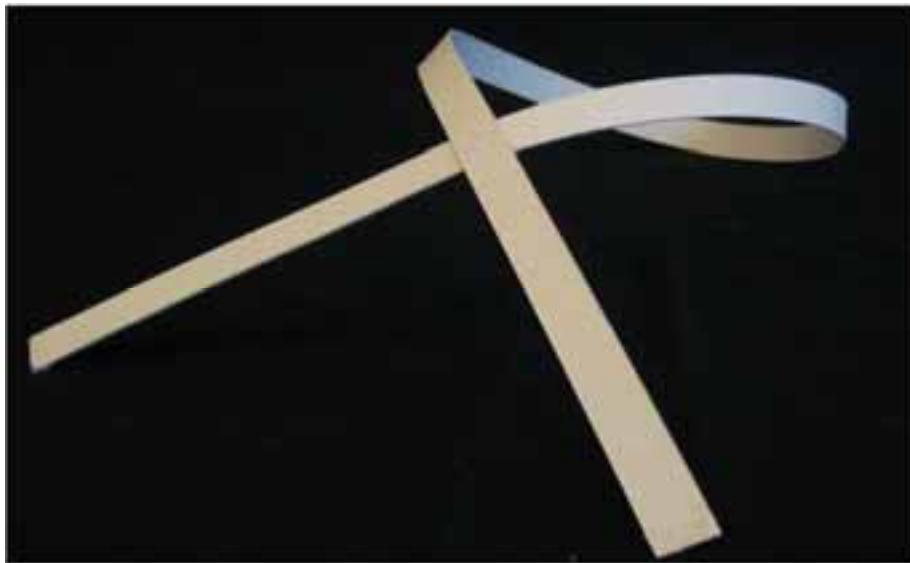
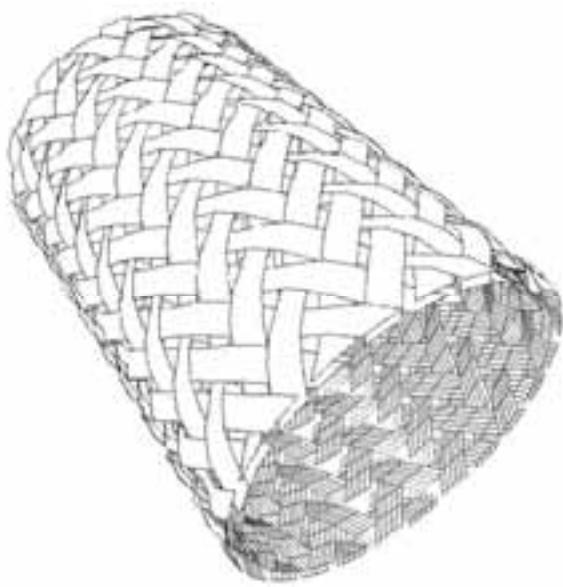
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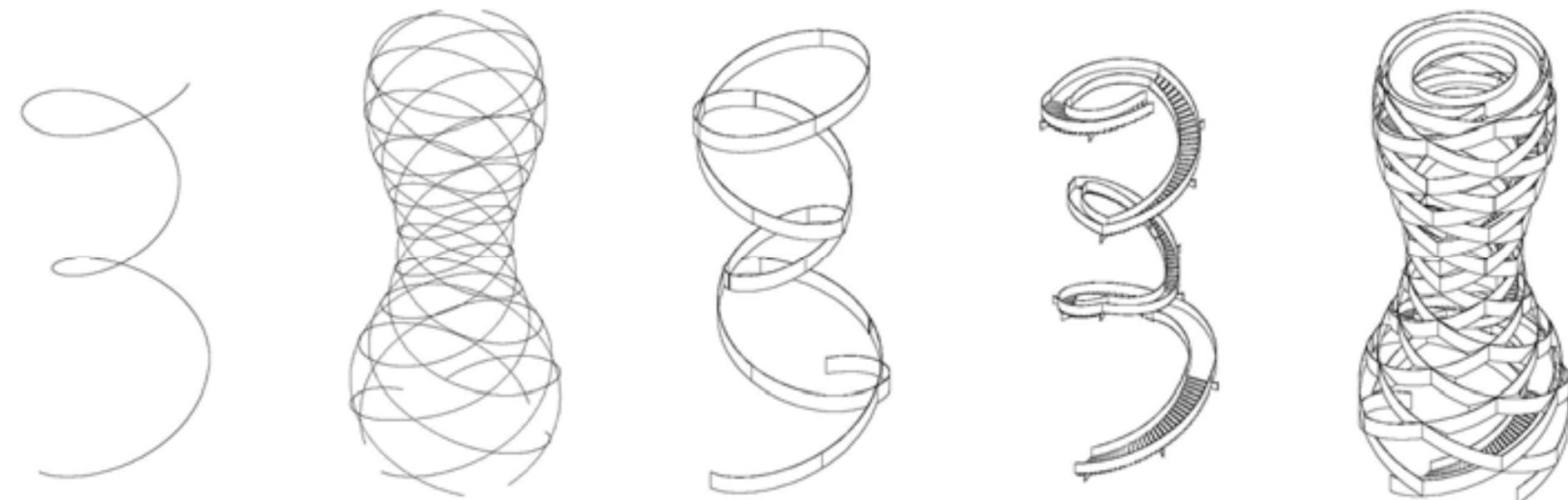
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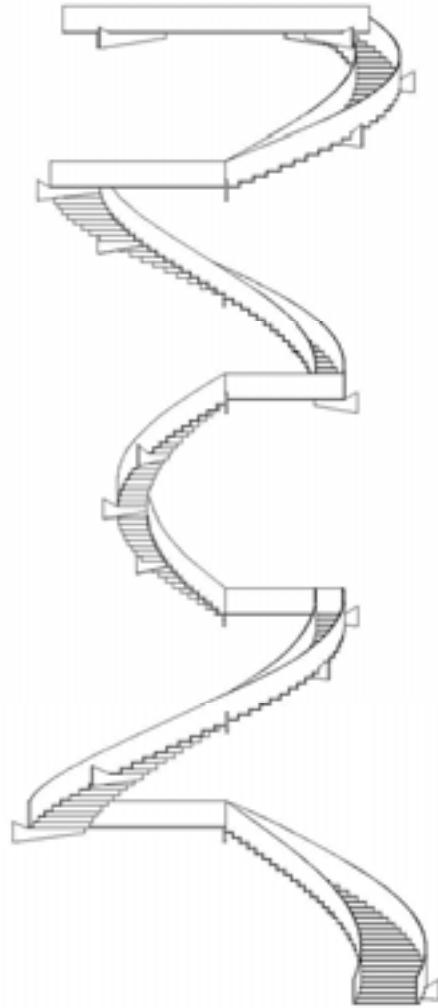
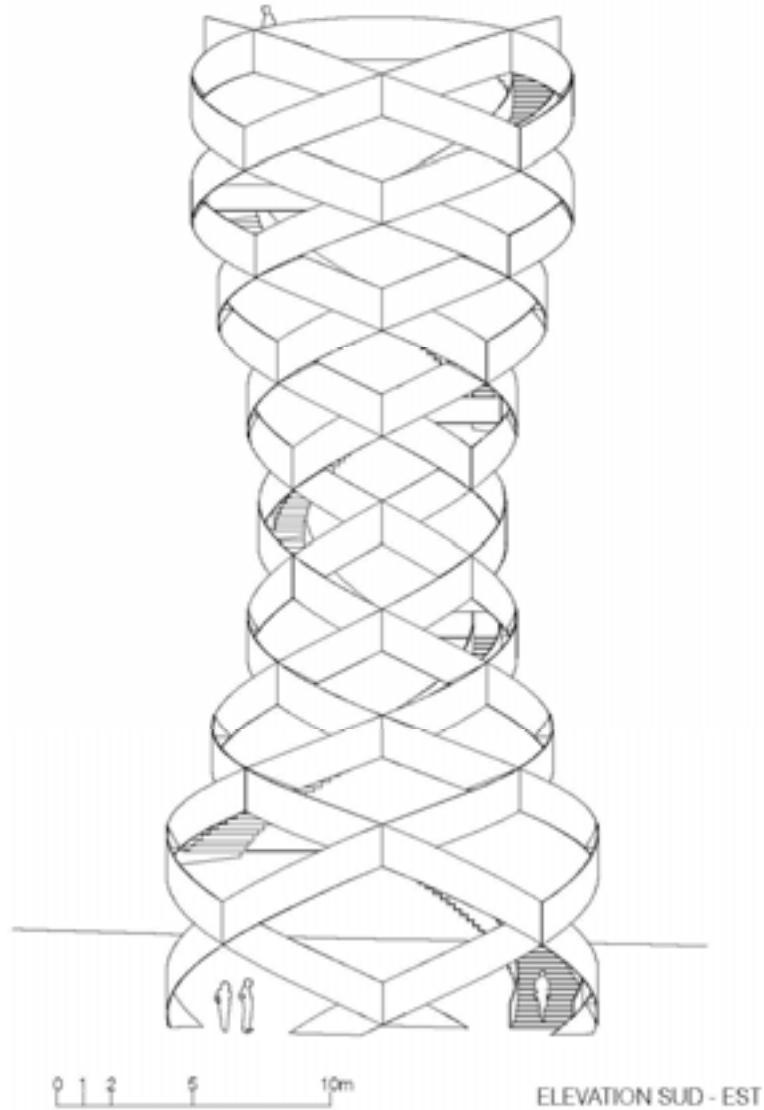
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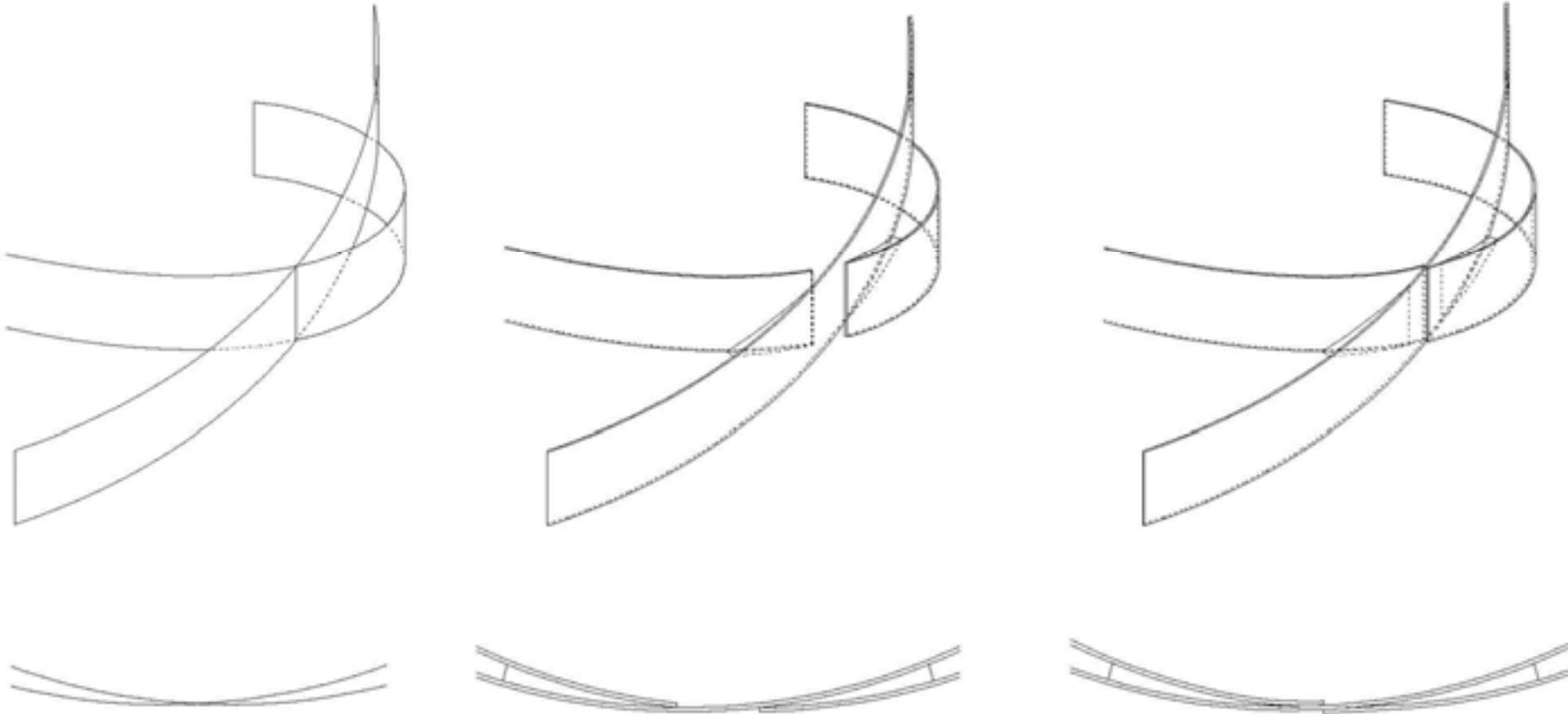
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PRINCIPE D'ASSEMBLAGE

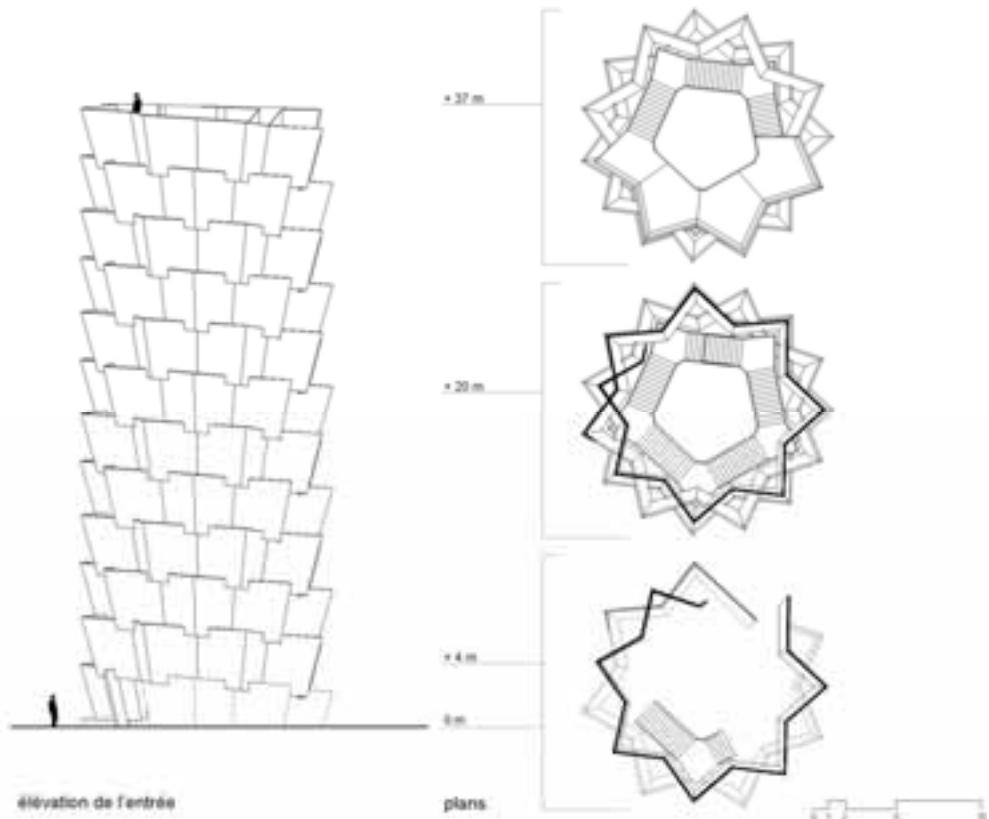
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Student Jonathan Hermann

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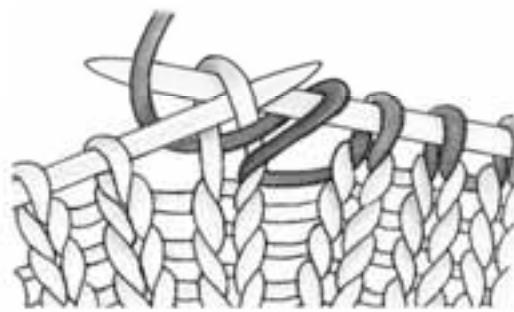
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Student Martin Wyss

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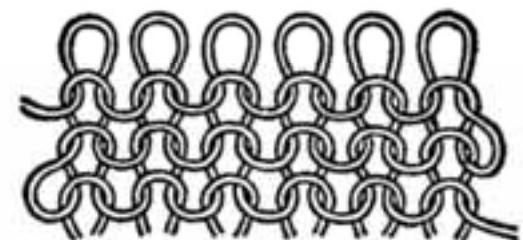
Répétition et intersection des éléments identiques



matière

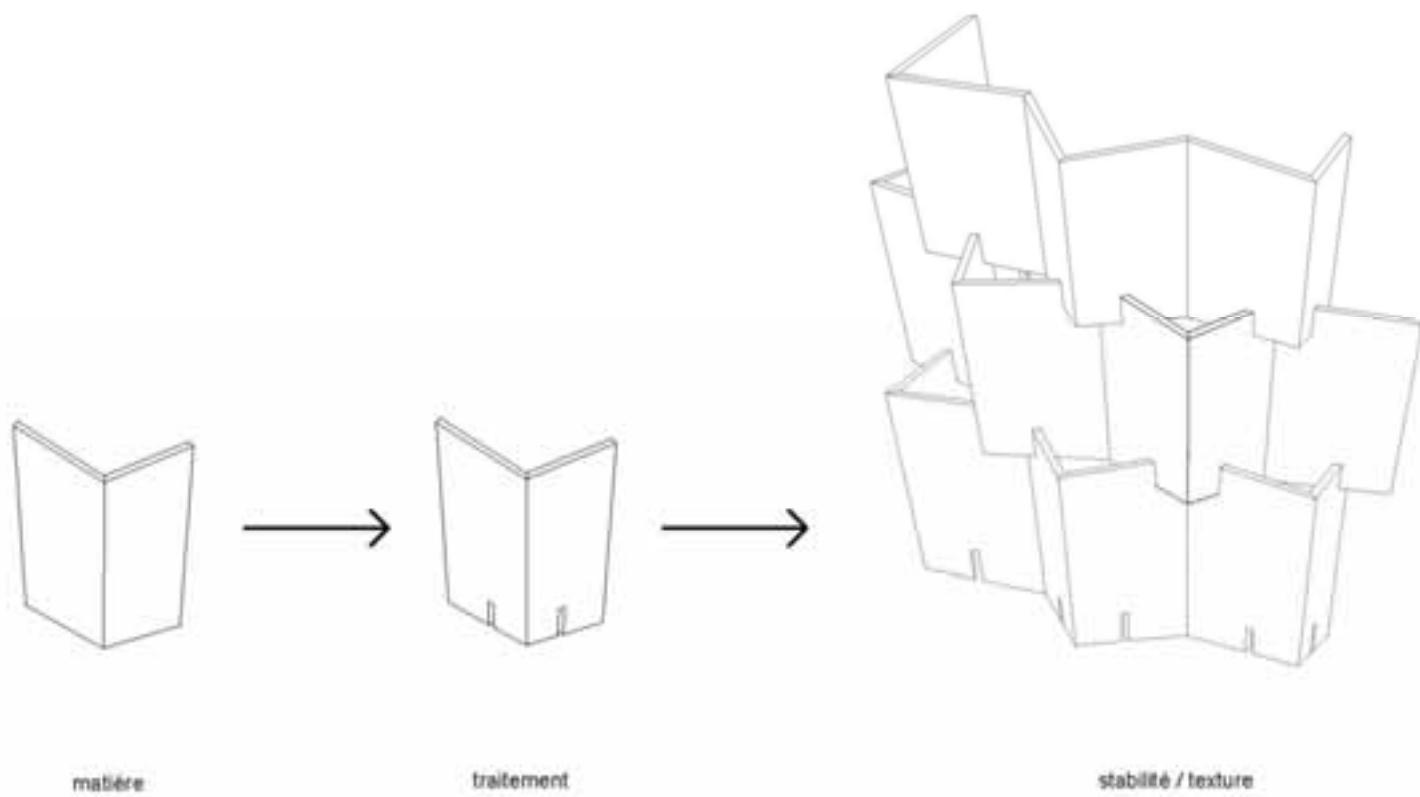


traitement



stabilité / texture

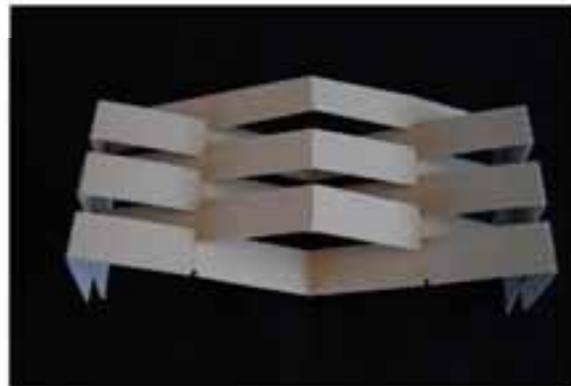
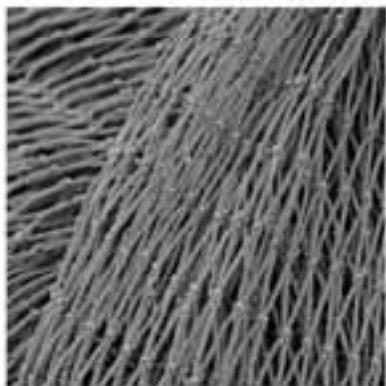
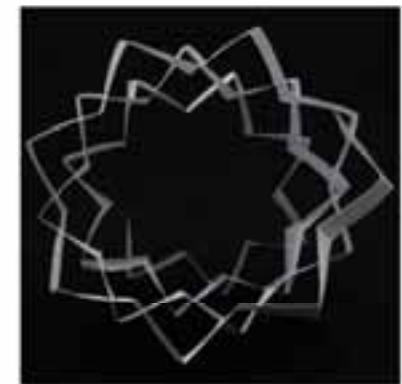
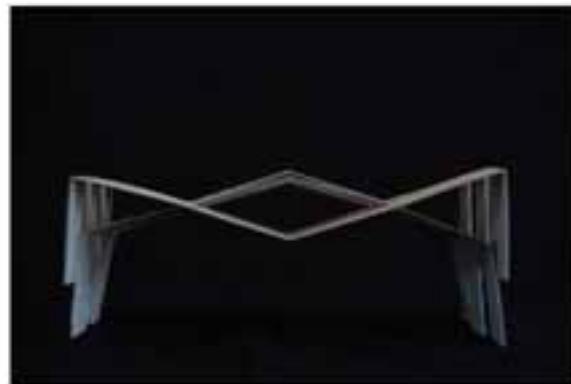
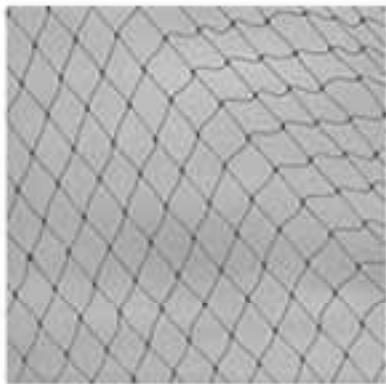
Répétition et intersection des éléments identiques



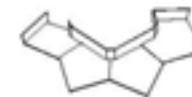
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Perception du même objet



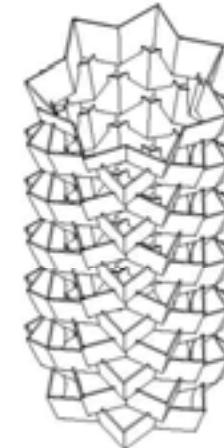
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Student Martin Wyss



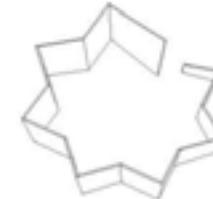
plateforme



escalier



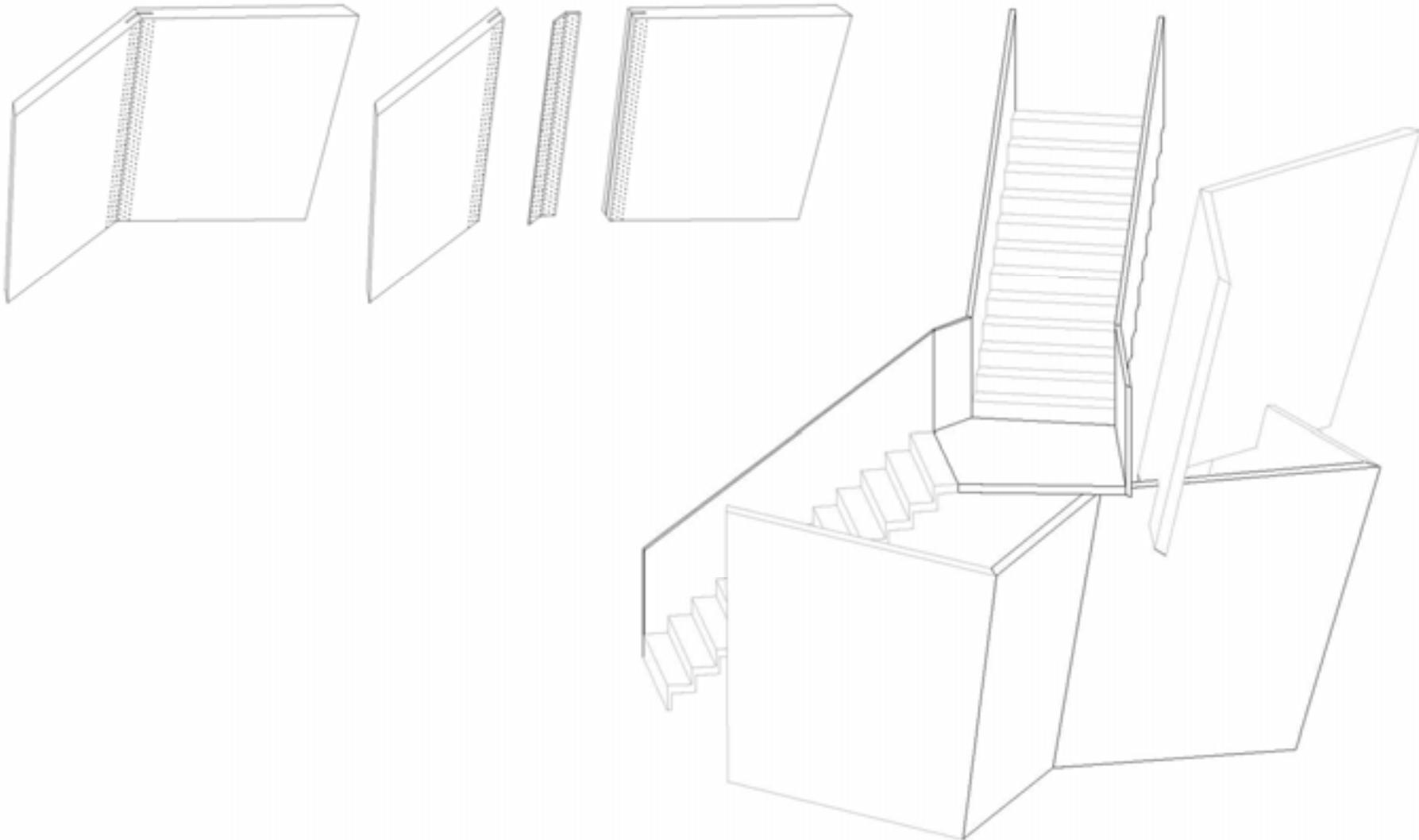
structure



fondation

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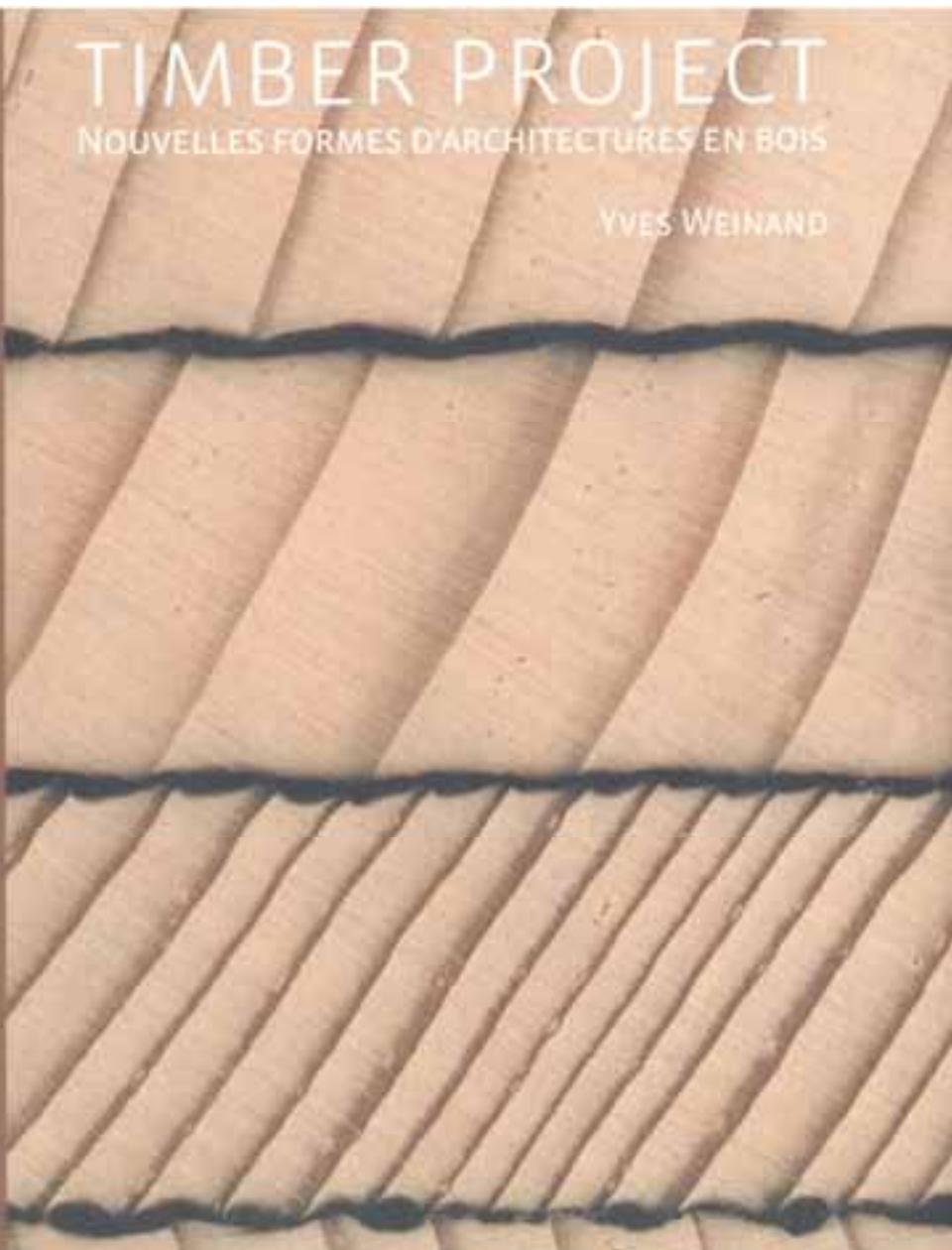
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ARCHITECTURE ALBUMS

TIMBER PROJECT

NOUVELLES FORMES D'ARCHITECTURES EN BOIS

YVES WEINAND



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Laboratory for timber constructions
Direction

Prof. Yves Weinand, ISA architect, EPFL civil engineer,
Associate Professor

Administration

Hildegard Bachmann, secretary
Staff

Ivo Stotz, EPFL architect, Dr.

Gilles Gouaty, DEA EDIIS Lyon (F) computer scientist, Dr.

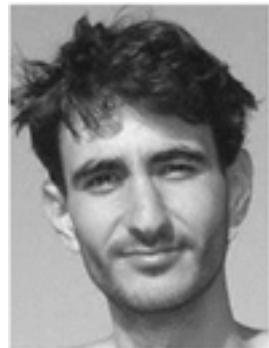
Hani Buri, EPFL architect, scientific collaborator

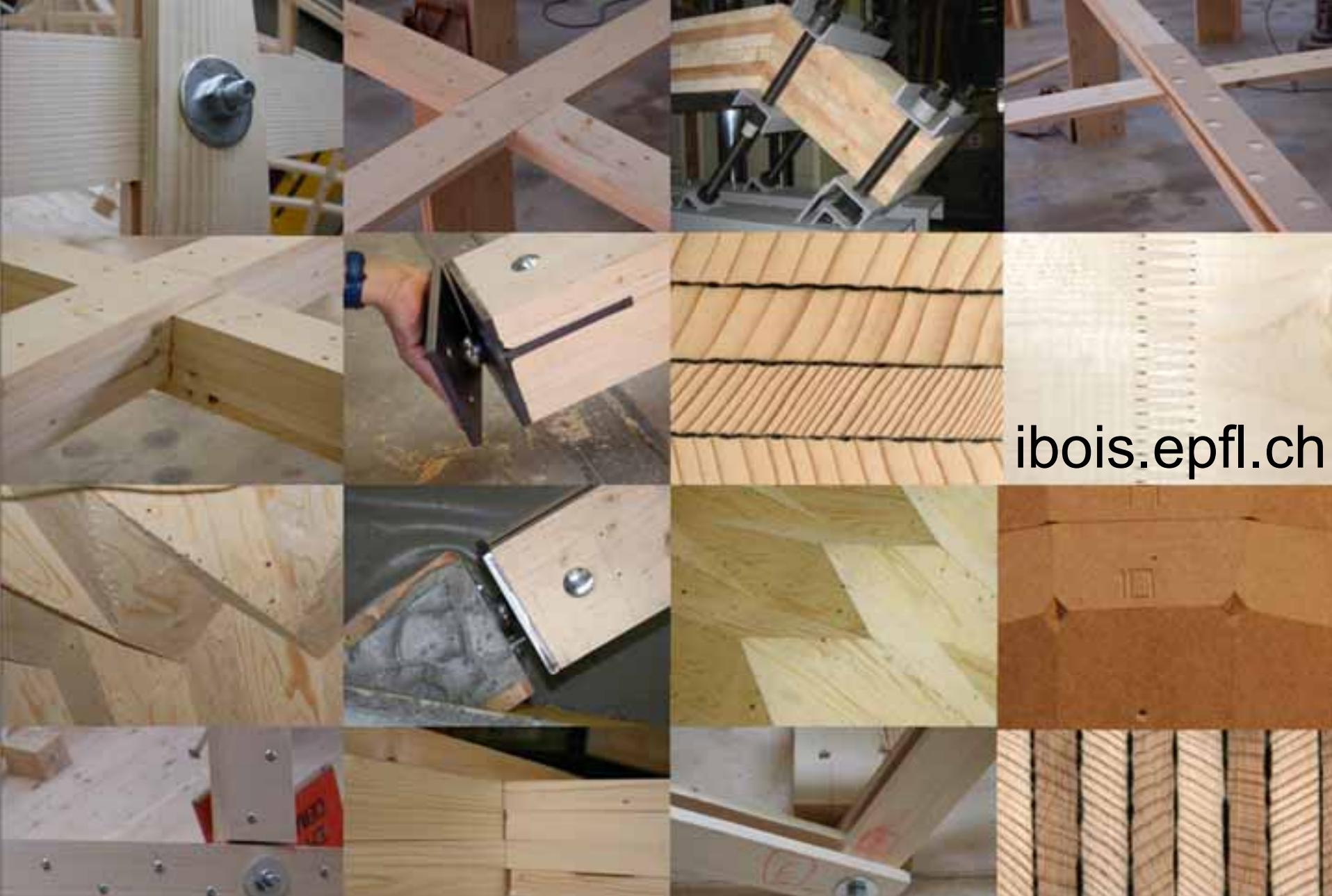
François Demoures, EPFL mathematician, PhD assistant

Markus Hudert, Städelschule Frankfurt (D) architect, PhD
assistant

Johannes Natterer, EPFL SIA civil engineer, Dr., scientific
collaborator

Masoud Sistaninia, Iran University of Science and Technology,
Teheran,
mechanical engineer, PHD assistant





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